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Deicer Source Hindcasting in an Unconfined Roadside Aquifer

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DEICER SOURCE HINDCASTING IN AN UNCONFINED ROADSIDE AQUIFER

A Master's Project Presented by
Ivonne Grajko Hall

Submitted to the Department of Civil and Environmental Engineering of the University
of Massachusetts in partial fulfillment of the requirements for the degree of

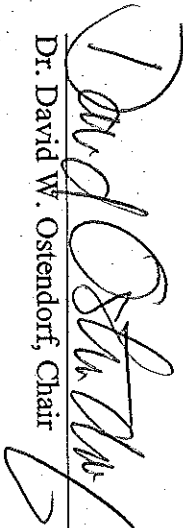
MASTER OF SCIENCE IN ENVIRONMENTAL ENGINEERING

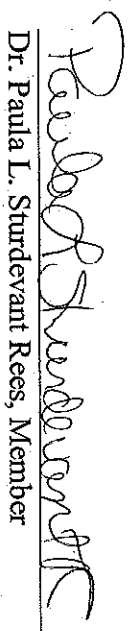
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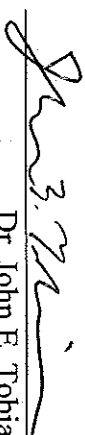
DEICER SOURCE HINDCASTING IN AN UNCONFINED ROADSIDE AQUIFER

A Master's Project Presented by
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ABSTRACT

Deicing materials that include calcium magnesium acetate (CMA), road salt, and premix are applied over a 1.2 mile section of the highway on State Route 25 (SR25) in Plymouth, Massachusetts. This part of the highway was designed to route runoff to an infiltration basin. The main goal of this research was to evaluate when and where deicer contamination infiltrated to the groundwater table at the site, with a focus on the infiltration basin. This project evaluated the steady-state hydraulics of the site, as well as the fate and transport of the deicing materials.

There are many sources of data available for modeling the Plymouth-Carver Aquifer at the site. Monthly groundwater monitoring provided hydraulic head and specific conductivity measurements and ion concentrations in groundwater sampled from wells located in and around the infiltration basin. Groundwater specific conductivity measurements were available from nine permanent conductivity points (PCPs) located in and around the basin. Slug test data collected from one deep well (BO) and one shallow well (BP) were used to confirm the calibration of the permeability of the aquifer material. A rain gauge located in the infiltration basin established the amount of precipitation that fell on the subject site area, and was also compared to data collected by the UMass-Cranberry Station located a few miles west of the basin. Surface water measurements of hydraulic head and specific conductivity collected at five to ten minute intervals at the main exit weir (West Weir) in the infiltration basin were used to characterize the volume and quality of water entering the infiltration basin.

Once the hydraulic model was calibrated, it was first used to recover a constant permeability for the aquifer. A permeability of $1.5 \times 10^{-10} \text{ m}^2$ was found, a value which fell within the range indicated by the slug test data. Next, the transverse and vertical limits of deicer contamination were predicted from the model. The plume was determined by the model to be approximately 20 m wide in the east-west direction, and as deep as 12 m below the water table. This result agreed well with past studies.

The model was then used to hindcast travel times and source locations of deicing constituents in the groundwater. As expected, results confirmed that the infiltration basin is the largest source of deicer contamination at the site, and source isopleths created from

hindcasted data showed deicer infiltration peaking in the winter and in the spring. Monthly average specific conductivities of the groundwater in the basin were hindcasted with the model for a nineteen month period (which included the deicing seasons of 2002 – 2003 and 2003 – 2004) and were compared to what was observed in discharge over the exit weir. The hindcasts for the first deicing season compared well to what was observed over the weir, while the second deicing season was underestimated by the hindcasted results. However, these results may be attributed to the basin being deeply frozen over the course of that winter, thus not allowing the water discharging over the weir to infiltrate the groundwater.

The mass fluxes of each conservative deicer ion were compared to the specific conductivity fluxes as ion flux ratios for an entire year after deicing activities began (November 2002 – November 2003). The ion flux ratios found over the course of a year for CI suggested a decreasing trend, which was also indicated for the water discharging over the weir by a recent study. This showed the high mobility and solubility of CI compared to the other ions. Finally, the mass ratios for each deicer ion was hindcasted for the same year and compared to the composition of the deicers applied. The ratios hindcasted compared favorably to what was recorded.

This steady-state particle hindcasting analysis may be a useful tool in determining relative orders of magnitude of deicer contaminant.

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LIST OF SYMBOLS

Symbol	Dimensions	Description
A_B	l^2	basin area
A_{cell}	l^2	cell area
A_E	l^2	electrode surface area
A_P	l^2	paved area captured
A_{pk}	l^2	peak area
A_x	l^2	area of cell face in x-direction
A_z	l^2	recharge zone area
C	m/l^3	concentration
C^*	m/l^3	adjusted concentration
C_i	m/l^3	ion concentration
C_r	m/l^3	recovered concentration
C_s	m/l^3	concentration of spike solution
C_w	m/l^3	concentration of water sample
D	l	distance
D_m	l^2/t	macrodispersion coefficient
D_{mol}	l^2/t	molecular diffusion coefficient
D_{mx}	l^2/t	macrodispersion coefficient in x direction
D_{my}	l^2/t	macrodispersion coefficient in y direction
D_{mz}	l^2/t	macrodispersion coefficient in z direction
d	l	maximum allowable ponding depth
E	$-$	efficiency of drainage system
F_{dx}	m/l^2t	diffusive solute mass flux in the x direction
F_{mx}	m/l^2t	macrodispersive flux in x direction
f	l/t	soil infiltration rate
G	$t^3-C^2/m-l^2$	conductance
g	l/t^2	gravitational constant
H	l	weir water level

LIST OF SYMBOLS cont.

Symbol	Dimensions	Description
h	l	hydraulic head
IS	mol/l ³	ionic strength
K	l ^{0.5} /t	weir calibration constant
k	l ²	intrinsic permeability
L	l	length of a reach through a cell
Le	l	distance between electrodes
L _R	l	roadway length
M _{azide}	m	mass of azide preservative
M _w	m	mass of water sample
MDL	m/l ³	(concentration) method detection limit
MW _i	m/mol	ion molecular weight
mM _i	mol/l ³	millimolar concentration of the ith ion
m _{d,app}	m	total deicer mass applied
m _{ion, app}	m	mass of conservative ion applied
m _r	m	mass of deicer recovered
Norm RMS	--	Normalized Root Mean Squared
n	--	soil porosity
P _A	l/t	annual average precipitation
Q	l ³ /t	volume flow rate
Q _s	m ⁻¹ /t ³	sublimative heat transfer
Q _H	m ⁻¹ /t ³	sensible heat
Q _R	m ⁻¹ /t ³	total incoming energy
Q _{xi}	l ³ /t	volume flow rate inward, x-direction
q	l/t	specific discharge vector
q _x	l/t	specific discharge in x-direction
q _y	l/t	specific discharge in y-direction
q _z	l/t	specific discharge in z-direction
R	--	recharge
R _i	l	residual of hydraulic head at i location
RMS	--	Root Mean Squared
RF	m ² /l-t ⁴ -C ²	response factor
r	m ⁻¹ /t ³ -C ²	resistance
S _s	l ⁻¹	specific storage
S _y	l ⁻¹	specific yield
S	m ⁻¹ /t ³	stored energy change
s	m/l ³	standard deviation of sample concentration
T _*	t	design ponding time
T _x	--	tortuosity of groundwater in the x direction
t	t	time
t ₁	t	time particle enters cell
t ₂	t	time particle exits cell
t _A	t	time when deicer 1 st applied

LIST OF SYMBOLS cont.

Symbol	Dimensions	Description
t_b	t	time before new deicing season begins
t	t	time interval
U	L/t	apparent groundwater velocity
V	l^3	volume of water infiltrating groundwater
V_s	l^3	volume of spike solution added
V_w	l^3	volume of water sample
V_{xp}	L/t	x-component of particle's linear velocity
V_{xi1}	L/t	x-comp. of average linear velocity inward
V_{yi1}	L/t	y-comp. of average linear velocity inward
V_{zi1}	L/t	z-comp. of average linear velocity inward
V_{x2}	L/t	x-comp. of average linear velocity outward
V_{y2}	L/t	y-comp. of average linear velocity outward
V_{z2}	L/t	z-comp. of average linear velocity outward
$ v $	L/t	magnitude of average linear groundwater
W	1	width of a reach through a cell
W_e	1	effective width
x	1	distance in x direction
x_1	1	initial particle position in x-direction
x	1	x-dimension of cell
x_p	1	x-position of particle
X_{cal}	1	calculated hydraulic head
X_{obs}	1	observed hydraulic head
Y	--	monovalent ion activity coefficient
y	1	distance in y-direction
y	1	y-dimension of cell
z	1	distance in z-direction
z	1	z-dimension of cell
z_B	1	bedrock elevation
z_L	1	limiting streamline elevation
$ z_i $	--	absolute value of the charge of the ith ion
α_x	1	longitudinal dispersivity in x-direction
α_y	1	transverse dispersivity in y-direction
α_z	1	vertical dispersivity in z-direction
β	$C^2 - t^3/m - 1$	average specific conductivity
β_{mo}	$C^2 - t^2/m - 1$	monthly average specific conductivity
γ	l^2	model conductance
δ	--	number of data points
ϵ_A	L/t	ambient recharge rate
ϵ_B	L/t	basin recharge rate
ϵ_M	L/t	monthly recharge rate
ϵ_R	L/t	runoff recharge rate
ζ	1	aquifer thickness
η	--	spike recovery percentage

LIST OF SYMBOLS cont.

Symbol	Dimensions	Description
θ_F	--	irreducible value
θ_u	--	water content in unsaturated zone
κ	$t^3 - C^2/m-l^3$	conductivity
κ^o	$t^3 - C^2/m-l^3$	infinite dilution conductivity
κ_{calc}	$t^3 - C^2/m-l^3$	calculated conductivity
Λ	$l^3 - C^2/C^2 - t^3$	ion mass flux ratio
λ^e, λ_{-1}	$t^3 - C^2/m-l^2$	equivalent conductance of the ith ion
λ_{app}	--	applied ion mass ratio
λ_{hind}	--	hindcasted ion mass ratio
ν	l^2/t	kinematic viscosity
ρ	m/l^3	fluid density
ρ_s	m/l^3	dry soil density
ρ_w	m/l^3	water density
σ_{hind}	$C^2 - t^2/m$	hindcasted monthly conductivity flux
σ_{obs}	$C^2 - t^2/m$	observed monthly specific conductivity flux
σ_{ion}	m/t	hindcasted monthly ion mass flux
v	l/t	flow pore velocity
φ	l/t	hydraulic conductivity
Ω	--	ion charge balance

LIST OF ABBREVIATIONS

Bi-CGSTAB	Bi-Conjugate Gradient Stabilized
BMPs	best management practices
BOD	biochemical oxygen demand
$\text{Ca}_3\text{Mg}_7(\text{C}_2\text{H}_3\text{O}_2)_{20}$	calcium magnesium acetate
Ca^{+2}	calcium ion
CaCl_2	calcium chloride
CBE	Civil and Environmental Engineering
CH_3COO^-	acetate ion
CO_2	carbon dioxide
Cl^-	chloride ion
CHBS	Constant Head Boundaries
CMA	calcium magnesium acetate
DCIS	directly connected impervious surfaces
DIUF	deionized, ultrafiltered
DO	dissolved oxygen
EC	electrical conductivity
EC	Environment Canada
$\text{Fe}(\text{OH})_3$	ferric hydroxide
$\text{Fe}(\text{II})$ or Fe^{2+}	ferrous iron
$\text{Fe}(\text{III})$ or Fe^{3+}	ferric iron
FHA	Federal Highway Administration
GHBS	General Head Boundaries
GPM	gallons per minute
HCl	hydrochloric acid
HCO_3^-	bicarbonate ion
HNO_3	nitric acid
1495	(Massachusetts) Interstate 495
IC	Ion Chromatography
K^+	potassium ion
K_A	potassium acetate
KOH	potassium hydroxide
mM	millimoles
m msl	meters mean sea level
m^3/d	cubic meters per day
MADEP	Massachusetts Department of Environmental Protection
MCP	Massachusetts Contingency Plan
MGD	million gallons per day
MDL	method detection limit
Mg^{+2}	magnesium ion
MgCl_2	magnesium chloride
mg/L	milligrams per liter
MHD	Massachusetts Highway Department
mM	millimoles
msl	mean sea level

LIST OF ABBREVIATIONS cont.

MODFLOW	MODular finite-difference groundwater FLOW model
MODPATH	MODular PATHline model
MSA	methane sulfonic acid
MT3DMS	Modular 3-Dimension Multi-Species Transport model
Na ⁺	sodium ion
NaCl	sodium chloride
NaHCO ₂	sodium formate
NaN ₃	sodium azide
NCDC	National Climatic Data Center
Norm RMS	Normalized Root Mean Squared
NSDWRs	National Secondary Drinking Water Regulations
O ₂	oxygen
PCP	permanent conductivity point
PVC	polyvinyl chloride
QA/QC	quality assurance/quality control
RF	response factor
RMS	Root Mean Squared
SIP	Strongly Implicit Procedure Package
SMCL	Secondary Maximum Contaminant Level
SO ₄ ⁻²	sulfate ion
SOR	Slice-Successive Overrelaxation Package
SR25	(Massachusetts) State Route 25
TCA	tricarboxylic acid
TDS	total dissolved solids
TEI	The Environmental Institute
TRB	Transportation Research Board
UMass	University of Massachusetts
USEPA	United States Environmental Protection Agency
USGS	United States Geological Survey
x ₁	cell face perpendicular to x-direction receiving inflow
y ₁	cell face perpendicular to y-direction receiving inflow
z ₁	cell face perpendicular to z-direction receiving inflow
x ₂	cell face perpendicular to x-direction receiving outflow
y ₂	cell face perpendicular to y-direction receiving outflow
z ₂	cell face perpendicular to z-direction receiving outflow

1 INTRODUCTION

1.1 PROJECT OVERVIEW

Deicing chemicals are applied to roadways to provide safe driving conditions in times of inclement weather during the winter season. The most common road deicer is sodium chloride (NaCl). More commonly known as road salt, NaCl is inexpensive and has been proven to be quick and effective at clearing ice and snow from roadways. Unfortunately, NaCl damages roadways and motor vehicles, and it has been demonstrated to negatively impact the environment. These problems have propagated the development of alternative road deicing materials like calcium magnesium acetate (CMA).

Since the 1990s, the Civil and Environmental Engineering Department at the University of Massachusetts (UMass), in cooperation with the Massachusetts Highway Department (MHD), has studied CMA as an alternative deicer along a 1,950 m (1.2 mile) stretch of State Route 25 (SR25) in Plymouth, Massachusetts. This research site location (known hereafter as “the site”) was chosen due to its proximity directly upgradient of environmentally sensitive cranberry bogs. Runoff from the 1,950 m portion of SR25 that uses CMA discharges to an infiltration basin located adjacent to a rest area off the highway. The runoff ultimately infiltrates into a sandy aquifer.

CMA has been shown to be an effective deicer that minimally impacts roads and automobiles, and causes less harm to the environment (Meyer, 1999). Its contact with environmentally sensitive receptors (e.g., plant life) is limited, since the highly biodegradable nature of CMA ensures that it does not persist. However, the

biodegradation of CMA causes a depletion of dissolved oxygen (DO) in groundwater and surface water, which will eventually lead to a negative impact on aquatic life. In turn, this DO depletion results in anoxic conditions that anaerobically degrade any acetate that is further loaded into the aquifer. The anaerobic degradation of acetate is facilitated by the reduction of ferric iron Fe(III), which coats soil grains, to ferrous iron Fe(II) by iron reducing bacteria. Fe(II) is more mobile and soluble in groundwater, and may precipitate out if later exposed to oxygen.

1.2 OBJECTIVES

This project continues research of the transport of deicing materials at the site.

The main goal of the project was to characterize where and when runoff from the highway infiltrates the groundwater, and use these data to study the fate and transport of deicing materials in the site aquifer. The specific objectives of this project included:

- Collecting and compiling monitoring and analytical data from groundwater and surface water runoff,
- Developing a steady-state three-dimensional numerical model to predict the vertical limit of the contamination area resulting from deicing activities,
- Applying the model to hindcast the travel times and source locations of deicing constituents in groundwater,
- Establishing deicing constituents that entered the groundwater table within the infiltration basin for a nineteen month period that included two deicing seasons by hindcasting monthly isopleths, fluxes, and average specific conductivities, and

- Hindcasting ion mass fluxes, ion flux ratios, and ion mass ratios for a full year after deicing activities to determine the composition of deicer infiltrating the groundwater in the basin.

1.3 RESEARCH APPROACH

To satisfy the objectives of the project, monthly groundwater sampling and monitoring data, frequent monitoring data from permanent conductivity point (PCP) observation locations, and monitoring data logged continuously at a weir located in the infiltration basin were used. Data collection methods are discussed in Chapter 3. These data were used to calibrate the hydraulic model, which was then applied to forecast and hindcast the fate and transport of deicing constituents. Chapter 4 describes the development of the steady-state three-dimensional numerical model, while Chapter 5 presents and discusses results. Chapter 6 gives conclusions about the results found.

2 BACKGROUND

2.1 HYDROLOGY

According to Maidment (2003), the hydrologic cycle is the most important concept in hydrology, and it is illustrated in Figure 2-1 (McGraw-Hill, 2000).

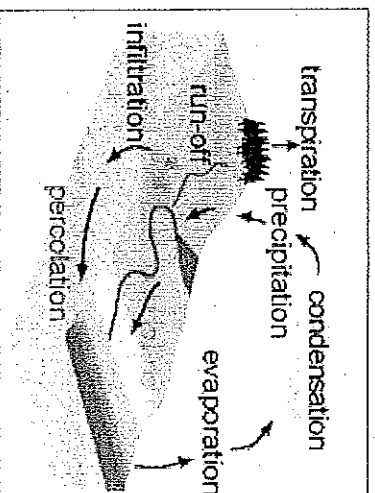


Figure 2-1 Hydrologic Cycle

(McGraw-Hill website, 2000)

Water evaporates from the oceans and land surfaces, circulating in the atmosphere as water vapor, precipitating as rain or snow, running off land surfaces, infiltrating soils and recharging the groundwater table, discharging into streams, and eventually flowing back to the oceans to repeat the cycle. Water is lost along the process cycle via natural mechanisms (e.g., evapotranspiration by trees and other vegetation) and by other means (e.g., pumping of groundwater).

The typical residence time in deeper groundwater is on the order of 10,000 yrs, while in shallower groundwater the residence time is on the order of 100 yrs. Groundwater hydraulic principles are discussed in Chapter 4.

2.1.1 Precipitation

Precipitation is the efflux of water and ice out of the atmosphere as rain and snow, occurring as a mass of air is lifted up through an undisturbed air mass in the troposphere. Precipitation exhibits tremendous variability in time and space (Maidment, 1993). Precipitation can be measured with devices that include rain gauges, disdrometers, dopplar radar, and satellite. Recording rain gauges include the weighting type, the float and siphon type, and the tipping bucket type (Maidment, 1993).

There are two types of hydrologic predictions: event-based and continuous-based. In an event-based prediction, the volume of discharge or runoff is estimated from a single rain event. Conversely, a continuous-based prediction simulates runoff on an uninterrupted basis, including both rain and non-rain events. Spatial estimations of rainfall are often determined from measurement devices like rain gauges. Methods of computing mean areal precipitation include the isohyetal method, the Thiessen polygon method, the station average method, and the inverse-distance squared method.

2.1.2 Snowmelt

Snowmelt is an especially important mechanism for the infiltration of water in northern climates like Massachusetts. Snow accumulates to form a snowpack on a watershed in the winter that causes large discharges in the spring when heavy rain and strong snowmelt coincide. The snowpack conservation of energy balances the efflux of heat from the snowpack with the stored energy change (ΔS) inside the snowpack:

$$Q_s + Q_H - Q_R + \Delta S = 0 \quad (2-1)$$

where Q_s is the sublimative heat transfer, Q_H is the sensible heat, and Q_R is the total incoming energy. As snow melts, water fills the available void spaces until the snowpack moisture reaches its irreducible value θ_f when it is ripe. Once the snowpack becomes ripe, it is ready to discharge snowmelt to the watershed.

2.1.3 Infiltration

Infiltration is the process of water moving into a soil via precipitation, snowmelt, runoff, or irrigation. Infiltration controls surface runoff, groundwater recharge, and the transport of chemicals in surface and subsurface waters.

Infiltration is controlled by the top surface of a soil, which will determine how easily water will be absorbed into the soil. A bare soil leads to the formation of a crust that will impede infiltration (Maidment, 1993). When the soil's ability to absorb water exceeds the discharge rate, all rain and snow will drain into the soil. If the discharge rate exceeds the surface infiltration rate, surface runoff will occur and puddles will form.

Infiltration is also affected by the movement of water through soil. More specifically, it is affected by a soil's ability to transmit water (hydraulic conductivity), and its ability to retain and release water. Smaller soil particles like silts will pack themselves together more closely than larger particles and create smaller void spaces, thus not allowing water to be transmitted as easily. On the other hand, larger soil particles like sands and gravels will act as a more permeable media for water movement. Other factors affecting infiltration include the soil temperature (i.e., if a soil is frozen, it will not allow the infiltration of water).

Infiltration can be measured areally by an analysis of rainfall-runoff data from a watershed, or with a point measurement (Maidment, 1993). Point measurement device types include ponded-water ring or cylinder, sprinkler, tension, and furrow.

2.2 HIGHWAY RUNOFF AND DRAINAGE

2.2.1 Urban Runoff Pollution

Sources of water pollution can be classified as either point sources or nonpoint sources. Point sources refer to the discharge of a contaminant from a discrete location, while nonpoint sources are large areas that cause contamination and are therefore difficult to control (Haestad, 2003). Nonpoint sources of contamination include runoff from agricultural areas and urban areas or highways. Table 2-1 (USEPA, 1993) lists some common constituents found in urban stormwater runoff, as well as their sources and effects.

Some sources of the pollution found in urban runoff include atmospheric deposits, urban animals and birds, and nutrients from fertilizers (Novotny, 2003). However, a significant portion of the pollution in highway runoff is usually caused by automobiles. The residual contamination left by automobiles can include metals, oil, and grease. Deicing chemicals used on pavements to ensure the safe passage of automobiles in the winter also contribute to pollution in highway runoff.

Generally, the first portion of urban runoff flow contains most of the pollution. As a rule of thumb, the first 40% of runoff may contain as much as 60% of the pollution load (Novotny, 2003).

Table 2-1 Urban Runoff Pollutants
(USEPA, 1993)

Constituents	Sources	Effects
Sediments: TSS, turbidity, dissolved solids	Construction sites, urban/agricultural runoff, landfills, septic fields	Habitat changes, stream turbidity, recreation/aesthetic loss, contaminant transport, bank erosion
Nutrients: nitrate, nitrite, ammonia, organic nitrogen, phosphate, total phosphorus	Lawn/agricultural runoff, landfills, septic fields, atmospheric deposition, erosion	Algal blooms, ammonia toxicity, nitrate toxicity
Pathogens: total and fecal coliforms, fecal streptococci, viruses, E.Coli, enterococcus	Urban/agricultural runoff, septic fields, illicit sanitary connections, domestic and wild animals	Ear/intestinal infections, shellfish bed closure, recreational/aesthetic loss
Organic enrichment: BOD, COD, TOC, DO	Urban/agricultural runoff, landfills, septic fields	DO depletion, odors, fish kills
Toxic pollutants: metals, organics	Urban/agricultural runoff, pesticides/herbicides, USTs, hazardous waste sites, landfills, illegal deposits, industrial discharges	Toxicity to humans and aquatic life, bioaccumulation in food chain
Salts: sodium chloride	Urban runoff, snowmelt	Contamination of drinking water, harmful to salt-intolerant plants

Note: TSS = total suspended solids, BOD = biochemical oxygen demand, COD = chemical oxygen demand, TOC = total organic carbon, DO = dissolved oxygen, UST = underground storage tank

2.2.2 Stormwater Management

Urbanization has not only affected the quality of surface water runoff. An acceleration in urban development has also caused an increase in the frequency and magnitude of runoff events and decreased stream base flows (Haestad, 2003). The construction of more paved areas has caused larger volumes of water to runoff as overland flow, and increased the chance of flooding. According to Maidment (1993), stormwater management first received recognition in the early 1970s. Surface runoff in

urban areas has a higher velocity than in nonurban areas because impervious surfaces are smoother, resulting in faster concentrations of flow.

Structural best management practices (BMPs) are used to minimize directly connected impervious surfaces (DCIS) and encourage more local infiltration, which can help reduce pollution (Novotny, 2003). More recently, a multilevel control of stormwater has been practiced. Some of the BMPs used include the installation of porous and modular pavements, grass buffer areas and swales, percolation trenches, and infiltration basins (Maidment, 1993). Swales are typically vegetated depressions with a flat longitudinal slope and mild side slopes. Infiltration basins store stormwater until it infiltrates the bottom and sides (Novotny, 2003). Detention basins, which have an outlet structure, are also commonly used to control runoff (Haestad, 2003).

According to Maidment (1993), infiltration basins act as a retention facility where captured runoff can directly infiltrate into the subsurface. Infiltration basins are typically constructed by building an embankment and impounding water behind it, or excavating a depression with the capacity to capture runoff from a design storm. The basin side slopes should not exceed 4:1 (horizontal: vertical) to reduce erosion. An infiltration basin is only practical if the soils are very permeable to accommodate a tributary drainage area that does not require a large area.

The maximum allowable ponding depth (d)

$$d = f \times T_p \quad (2-2)$$

is a function of the soil infiltration rate (f) and the design ponding time (T_p) (Novotny, 2003). To prevent slime formation, exfiltration time should never exceed 72 hours; if vegetation is planted in the basin, this time should be reduced to 24 to 36 hours. There is

evidence that the organic debris in grass or other vegetation planted in an infiltration basin provide a habitat for insects and worms that help keep the top soil layer aerated, helping it maintain its infiltration capacity.

2.3 HIGHWAY DEICING CHEMICALS

Pavement deicing, or the application of salt and abrasives to control snow and ice, was first practiced in the United States in the 1930s (Chollar, 1989). Chemical deicing is the second most important part of a highway snow- and ice-control program after plowing, and it represents about one-third of winter maintenance budgets (Transportation Research Board TRB, 1991). Sand and gravel are abrasive materials used with deicing chemicals like salt to increase traction on icy roads, but they can clog storm water inlets and sewers (United States Environmental Protection Agency USEPA, 2004). Deicing salts lower the freezing point of water, helping to melt snow and ice accumulated on roadways. They may be applied in liquid or crystalline form, but crystalline forms are slower and longer acting deicing agents (Wegner and Yaggi, 2001). Solid deicing chemicals require moisture from snow or humidity to dissolve it into a brine solution before it can act (Wisconsin Transportation Center, 1996).

The most common road deicer is sodium chloride (NaCl), where mined rock salt has been crushed, screened, and treated with an anti-caking agent (Wisconsin Transportation Center, 1996). Sodium chloride is widely used because it is light (just over one ton per cubic yard) and inexpensive relative to other deicer chemicals. Furthermore, sodium chloride is easy to handle, store, and apply (TRB, 1991). Calcium chloride (CaCl_2), is also a common road deicing agent that is available in pellet, flake, or

liquid form. While calcium chloride requires special handling and is most expensive than sodium chloride, it works more quickly and effectively below 0°C (Chollar, 1989; Wisconsin Transportation Center, 1996). Often, a combination of both sodium and calcium chlorides is used on roadways to maximize their benefits. For example, premix is a mixture of 80% NaCl and 20% CaCl, by weight typically (USGS, 1996).

Other pavement deicers include urea (the nitrogenous component of urine), magnesium chloride ($MgCl_2$), potassium acetate (KA), and sodium formate ($NaHCO_2$). Urea is slower acting than salt and not as effective at lower temperatures, and it enhances the growth of plants and algae because it acts as a fertilizer (Chollar, 1989). Hassan *et al.* (2002) found that urea caused substantially more damage to pavements than potassium acetate and sodium formate.

2.3.1 Chloride-Based Deicing Chemicals

Unfortunately, there are several drawbacks to the use of chloride-based deicing materials. The largest financial disadvantage is that chloride-based compounds are corrosive to concrete and steel, thereby damaging roadways, bridges and motor vehicles (Wisconsin Transportation Center, 1996). Additives are now being used in rock salt and calcium chloride to reduce their corrosive properties. Another approach to solving the problem has been the employment of new construction methods to reduce infrastructure corrosion. These construction methods include the use of cathodic protection for existing bridge decks; and the use of internally sealed concrete, polymer concrete, and epoxy-coated reinforcement bars for new bridge decks (Chollar, 1989).

Another important concern with chloride-based deicing chemicals is their negative impact on the environment. Regulators in the management of nonpoint-source pollution have focused on heavy metals, hydrocarbons, pathogens, and sediment from urban runoff, and nutrients from agricultural runoff. However, the impact of road salt pollution first gained attention in 1980, at which time the Federal Highway Administration (FHWA) named CMA as a possible alternative to salt (TRB, 1991).

Chloride-based deicers have been shown to affect groundwater and soil, leading to negative impacts on plant and aquatic life. Chloride-based salts dissolve readily in water. While the cations in chloride-based deicers (Na^+ , Ca^{+2}) will bond with negatively-charged ions or be taken up in biological processes (Na^+), Cl^- ions are less reactive ions. As a result, chloride-based deicer chemicals are highly soluble and mobile in groundwater, and they are slow to biodegrade. In other words, once these chemicals are introduced into groundwater or surface waters, they spread quickly and persist for a long period of time. This allows the development of widespread contamination plumes, and increases the probability of chloride-based deicers reaching sensitive plant and aquatic life.

Typical salt constituent concentrations in surface water runoff can reach as high as several thousand mg/L (ppm), and sometimes as high in groundwater. Elevated sodium (Na^+) levels create osmotic imbalances in plants that can result in slower water absorption, a loss of cold hardness, and more susceptibility to disease and pests (McFarland and O'Reilly, 1991). Studies at two sites in California indicated that high levels of sodium and chloride were absorbed into plant tissues, although coarser granitic soils retained less salt ions than finer clayey soils (Gidley, 1989). Toxicity data indicated

that approximately ten percent of aquatic species have the potential to be adversely affected by prolonged exposure to chloride concentrations higher than 240 mg/L (EC, 2002). Changes in aquatic species populations occur at even lower levels, with algae shifting in lake populations at chloride concentrations as low as 12 mg/L (EC, 2002).

Road salts enter the environment when snow and ice melt, when sprayed from vehicles, and as windborne powder (EC, 2002). As a preventive measure, road salts should be covered when stored to reduce loss from stockpile runoff and prevent their contamination of nearby streams, aquifers, and estuarine areas (USEPA, 2004). Salt spillage associated with loading operations also has been demonstrated to substantially increase contamination, suggesting that covered deliveries and loadings would mitigate the contamination (Ostendorf *et al.*, 2001). Road salts should be used minimally and reapplied as necessary, to prevent excess salts from being wasted.

The USEPA established a Secondary Maximum Contaminant Level (SMCL) for chloride of 250 mg/L in drinking water supplies (USEPA, 2002). However, National Secondary Drinking Water Regulations (NSDWRs) are only recommended guidelines that states may choose to enforce, and currently Massachusetts does not specify a groundwater standard for chloride (MADEP, 2005).

The negative impacts of chloride-based deicing chemicals has led to the development of more biodegradable deicer chemicals like CMA and KA. However, this study will focus exclusively on CMA as an alternative to chloride-based deicing chemicals.

2.3.2 Calcium Magnesium Acetate (CMA)

The TRB (1991) concluded that while the widespread use of CMA as an alternative to chloride-based deicers is not warranted, its cost-effectiveness on a selective basis (e.g., in environmentally-sensitive areas, on corrosion-prone bridges) should be determined on an individual basis. Vitaliano (1992) concluded that there was not enough evidence to support the fact that the use of CMA could extend the life of old bridges. CMA or $\text{Ca}_3\text{Mg}_7(\text{C}_2\text{H}_3\text{O}_2)_{20}$ acts slower as a deicer than rock salt, and it is more expensive (TRB, 1991). The average cost of road salt is \$30/ton, while the cost of CMA has been estimated to range between \$500 and \$700 per ton (Wegner and Yaggi, 2001).

The Ontario Ministry of Transportation and Communications (Manning and Crowder, 1987) compared the application of CMA and rock salt. The application of CMA differed from that of rock salt: while the salt was spread by dropping it through a dispensing chute in the centerline of the road, the CMA became sticky upon contact with moisture, requiring that it be applied with machinery such as a slowly-rotating spinner. The report stated that the spreading characteristics were similar for both materials (e.g., both salt and CMA bounced until coming to rest), but that moisture bonded CMA to the pavement more strongly than the salt. Once the CMA was immobilized in the pavement, it was observed that additional precipitation was required to flush the CMA from the pavement. Additionally, the TRB (1988) found that less than ten percent of CMA applied in a study appeared in soil water or groundwater, suggesting that a significant portion of applied acetate can become immobilized on a soil surface so that it is not immediately transported through runoff or infiltration. Harris *et al.* (1993) noted that while salt melts into a brine solution, CMA melts to form a milky white solution. Unlike

Manning and Crowder (1987), Harris *et al.* (1993) also stated that the round shape of CMA pellets was a serious drawback, causing it to bounce off the pavement more than the angularly shaped salt particles.

CMA has been demonstrated to have minimal impact on roadways and the environment (Fritzsche, 1992). The TRB (1988) reported that various herbaceous and woody plant species survived root zone CMA concentrations up to 2,500 mg/L (ppm). A study of ten natural lakes in Northern California (Goldman *et al.*, 1989) concluded that eight of the ten lakes showed no significant response in algal biomass with the 0.1 to 10 mg/L (ppm) concentrations of CMA applied. However, some phytotoxic responses have been observed when CMA concentrations exceed 2,500 mg/L (McFarland and O'Reilly, 1991). At the Plymouth site, typical groundwater concentrations of CMA constituents are on the order of 10 and 50 mg/L (ppm), while direct surface water runoff concentrations of CMA can reach up to several thousand mg/L.

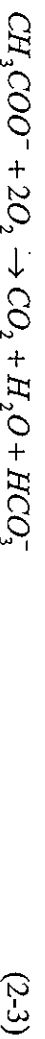
The TRB (1988) indicated that at temperatures of 10 to 20°C, most decomposition of CMA was completed within two weeks; but at 2°C, CMA took up to twice as long to degrade. Horner and Brenner (1992) also found that most decomposition of CMA occurred in two weeks, and that BOD was exerted within ten days. McFarland and O'Reilly (1991) found that the oxidation of CMA was complete within three to six days at temperatures between 10 and 20°C, although less reliably at lower temperatures. These findings may be attributed to the fact that the bacteria that degrade CMA are not as active at lower temperatures. McFarland and O'Reilly (1991) also found that most CMA was biodegraded in soil prior to reaching a receiving water, and if runoff occurred before

biodegradation, only about 10% of the CMA remained after flowing approximately thirty feet.

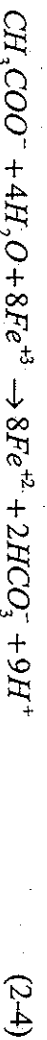
Brenner and Horner (1992) performed laboratory and field experiments to determine the effect of CMA on aquatic and terrestrial ecosystems. The study found that 100 mg/L of CMA completely depleted DO in some receiving waters within two days at 20°C. A level of 10 mg/L of reagent-grade and corned-based CMA caused net DO depletions of approximately 4.5 and 7.0 mg/L, respectively. Brenner and Horner (1992) attributed the extra oxygen demand from the corn-based CMA to the presence of butyrate. As McFarland and O'Reilly (1991) had found earlier, while the rate of DO depletion was shown to be strongly dependent on temperature, a first-order biochemical oxygen demand (BOD) equation did not represent DO depletion well at lower temperatures. Accordingly, Brenner and Horner (1992) modeled the rate of DO depletion with a logistical-type curve that better represented the growth of bacteria.

Brenner and Horner (1992) also recommended that use of CMA be avoided where receiving waters are close to the road and are not large enough to dilute the CMA, or if they support populations sensitive to DO depletions. Another study conducted on a small creek in Oregon showed no measurable increase of BOD or Ca^{+2} and Mg^{+2} concentrations from the application of CMA to a closely paralleling highway (Tanner and Wood, 2000).

Acetate (CH_3COO^-) is mineralized by heterotrophic bacteria via the tricarboxylic acid (TCA) cycle, consuming oxygen (O_2) and forming carbon dioxide (CO_2), bicarbonate (HCO_3^-), and water (Metcalf and Eddy, 2003):



The depletion of DO in groundwater and surface water from the degradation of CMA will eventually lead to a negative impact on aquatic life. Additionally, the DO depletion results in an anoxic condition that anaerobically degrades any acetate that is further loaded into the aquifer. The anaerobic degradation of acetate is facilitated by the reduction of ferric iron Fe(III), which coats soil grains, to ferrous iron Fe(II) by iron reducing bacteria like *Geobacter* and *Shewanella* (Lovley, 1997).



Ferrous iron tends to be more soluble than ferric iron. When reintroduced to aerobic conditions, soluble and suspended bivalent iron may become reoxidized to form insoluble ferric hydroxide, Fe(OH)₃, which precipitates out of solution (Stumm and Lee, 1960). Ferrous iron is also more mobile in groundwater than ferric iron.

2.3.3 Previous UMASS Studies

The Department of Civil and Environmental Engineering at the University of Massachusetts has conducted several years' worth of research on the transport and fate of CMA and other deicers applied at the site. The following includes a brief summary of the research that has been conducted up to date.

Ostendorf *et al.* (1993) indicated that loamy sand cover used on shoulder areas adjacent to SR25 had the ability to reduce oxygen demand by CMA on groundwater for slow snowmelt rates (10⁻⁷ m/sec) at 5°C under aerobic conditions. Aerobic reaction rates of CMA were slower in deeper soils than what was previously observed in the shallower sandy loam (Ostendorf *et al.*, 1995). The application of CMA as a road deicer causes aerobic degradation by microorganisms in the capillary fringe of the subsurface that can

lower oxygen demand in underlying groundwater (Ostendorf *et al.*, 1997; Long, 1996). Column studies performed on intact core sleeves of loamy surficial soils from a shoulder area adjacent to SR25 indicated a rate of acetate degradation between $3.0 \times 10^{-5} \text{ kg/m}^3$ and $3.6 \times 10^{-5} \text{ kg/m}^3$ (Glass, 1999).

It was observed that DO remained depleted in the anoxic zone even after the CMA contamination plume had passed. The reduction of ferric iron (Fe III) to the soluble ferrous iron (Fe II) elevated iron levels in groundwater (Meyer, 1999; Sullivan, 2001).

Fauteux (2002) evaluated the hydraulics of the site aquifer with a two-dimensional analytical model with a streamline analysis, and found a contamination plume about 20 m by 65 m. The basin recharge is much greater than the ambient recharge rate, pushing contamination deeper into the aquifer. Ostendorf *et al.* (2004) determined steady, annual, and monthly recharge rates for the site aquifer.

Ward (2003) observed elevated levels of deicing constituents in pore water extracted from the unsaturated zone in the basin infiltration area nearest to the West Weir. Levels of deicing constituents shown in surface runoff long after the completion of deicing activities also suggested that CMA was becoming immobilized in the highway pavement (Ostendorf *et al.*, 2005a; Ward, 2003). Field data indicated that pavement texture affects deicing agent contamination of highway runoff at storm and seasonal time scales (Ostendorf *et al.*, 2005a). Solid deicing agents can become immobilized in a depression storage layer in the pavement, whose thickness is equal to the average pavement texture. It follows that when the pavement is rough (or the pavement thickness is increased), the probability of deicer persisting in the pavement increases accordingly.

2.4 SPECIFIC CONDUCTIVITY

Electrical conductivity (EC) or conductivity estimates the amount of total dissolved ions in water. *Standard Methods* defines conductivity as a measure of the ability of an aqueous solution to carry an electrical current that depends on the presence of ions, their concentration in water, mobility, valence, and temperature (APHA *et al.*, 1995). Conductivity is affected by geology, because the composition of rock determines the chemistry of the soil in contact with the water. Evaporation of water from the surface of a lake can also concentrate dissolved solids in water remaining, thereby increasing conductivity. Pollutants such as wastewater from sewage treatment plants and septic systems, agricultural runoff, and urban runoff can also contribute to conductivity. In urban runoff, road deicer is an important contributor to electrical conductivity.

The conductance (G) of an aqueous solution is measured between two fixed inert points. The conductance (G) is the reciprocal of resistance (r), and it is directly proportional to the electrode surface area (A_E) and inversely proportional to the distance between the electrodes (L_E) (APHA, 1995):

$$G = \frac{1}{r} = \kappa \left(\frac{A_E}{L_E} \right) \quad (2-5)$$

The conductivity of the aqueous solution (κ) is the proportionality constant in Equation 2-5. The values of conductivity reported are standardized, with A_E equal to 1 cm² and L equal to 1 cm. Specific conductivity additionally standardizes the measurement to a temperature of 25°C.

For naturally occurring waters containing calcium (Ca^{2+}), magnesium (Mg^{2+}), Na^+ , HCO_3^- , sulfate (SO_4^{2-}) and Cl^- ions where the total dissolved solids (TDS) is less than 2,500 mg/L, conductivity may be calculated from measured ionic concentrations

(APHA, 1995). Infinite dilution is assumed so that the contribution to conductivity by each type of ion is cumulative. First, the infinite dilute conductivity κ° is determined:

$$\kappa^\circ = \sum |z_i|(\lambda_{+i}^\circ)(mM_i) + \sum |z_i|(\lambda_{-i}^\circ)(mM_i) \quad (2-6)$$

where $|z_i|$ is the absolute value of the charge of the i th ion, mM_i is the millimolar concentration of the i th ion, and $\lambda_{+i}^\circ, \lambda_{-i}^\circ$ are the equivalent conductance of the i th ion. Next, the ionic strength is calculated with Equation 2-7:

$$IS = \sum z_i^2 \frac{(mM_i)}{2000} \quad (2-7)$$

and the monovalent ion activity coefficient (γ) is found with the Davies equation for $IS \leq 0.5$ M for temperatures between 20 and 30°C:

$$\gamma = 10^{-0.5[IS^{1/2} \times (1 + IS^{1/2}) - 0.3IS]} \quad (2-8)$$

The final calculated conductivity K_{calc} is thus:

$$K_{calc} = \kappa^\circ \gamma^2 \quad (2-9)$$

where K_{calc} is reported in units of $\mu S/cm$.

Granato and Smith (1999) estimated the concentrations of road deicer constituents in highway runoff from a semi-empirical relationship between specific conductance and the ion concentrations, based on samples collected along SR25 in Plymouth, Massachusetts. The adjusted superposition method used accounted for errors at low and high ionic concentrations. At low concentrations, the conductance can be underreported if all the contributing ions are not accounted. At high concentrations, each constituent's contribution to conductance attenuates as the ionic strength increases.

2.5 SITE DESCRIPTION

2.5.1 Site Background

The site is located in Plymouth, Massachusetts, as shown in Figure 2-2. It is located along State Route 25 (SR25), 5.5 km north of the Cape Cod Canal in southeastern Massachusetts. Massachusetts SR25 was completed in August 1987 to extend Interstate 495 (I495) to the Bourne Bridge.

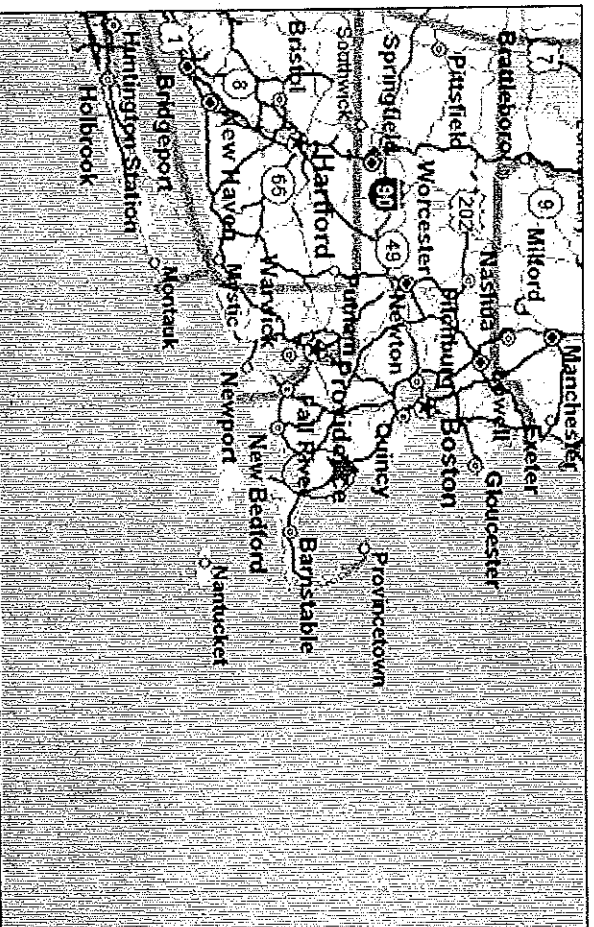


Figure 2-2 Plymouth, Massachusetts
(Mapquest website, 2005)

When the highway opened, the Massachusetts Department of Environmental Protection (MADEP) restricted the use of chloride-based deicing materials on a 1,950 m (1.2 mile) stretch of the roadway to protect sensitive cranberry bogs located directly downgradient. An infiltration basin was also constructed adjacent to this portion of the highway to restrict direct runoff from reaching the cranberry bogs. Since the winter of 1987 – 1988, this stretch of highway has been primarily treated with CMA, except in

emergency situations where the application of a chloride-based deicer (e.g., NaCl, CaCl₂) was required to keep the road clear.

The site extends from the north shoulder of SR25, across the roadway, and through the infiltration basin and rest area south of the highway, as shown on Figure 2-3. Sensitive receptor areas include a replacement wetland area located to the north, a cranberry bog (Mann Bog) to the east, and Weeks Pond to the south.

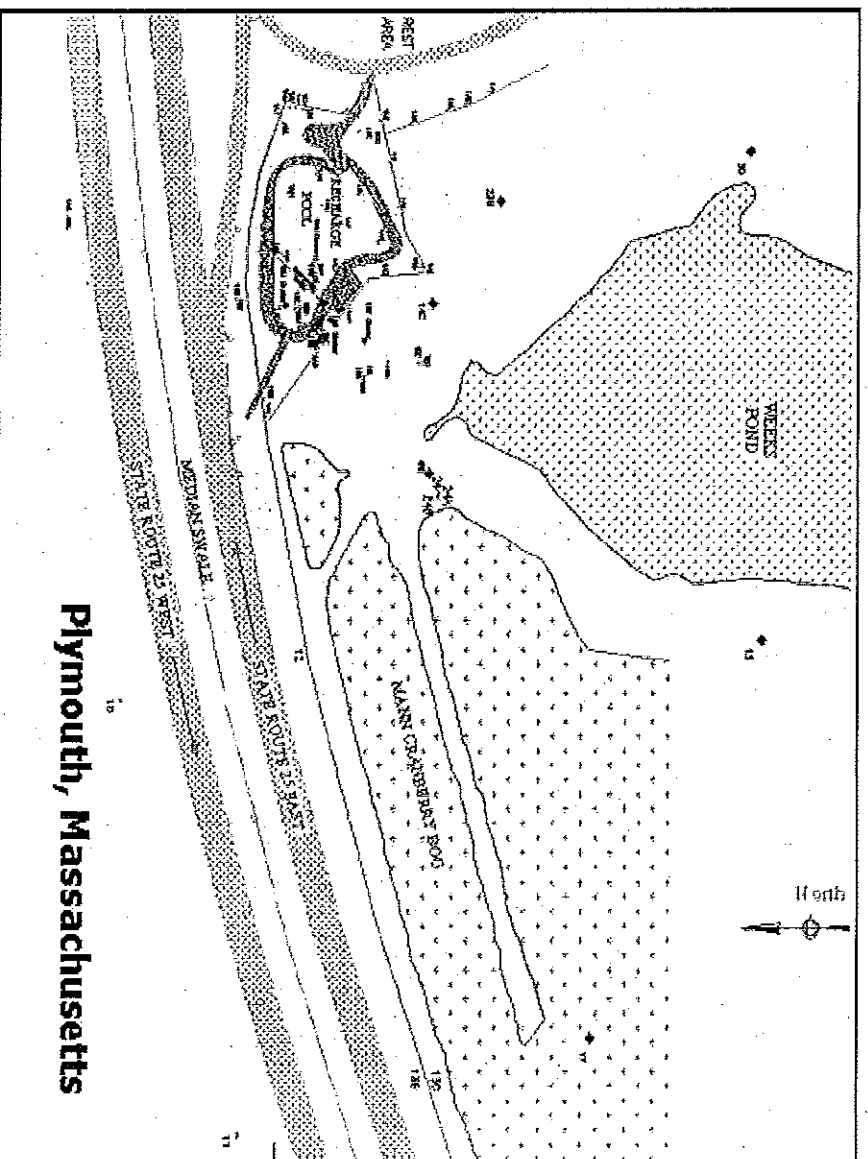


Figure 2-3 Subject Site

SR25 was constructed with six 3.66 m-wide travel lanes, two 1.2 m inner shoulders, two 3.05 m breakdown lanes, and a 30 m-wide grass median swale. The travel lanes, inner road shoulders, and travel lanes were sloped to the south. The drainage systems for the highway were designed to capture runoff into catch basins spaced 90 m apart, located down the center of the grass median swale and along the paved surface edges. The catch basins were designed to discharge captured runoff to one of two exit 90° V-notch weirs (West and East Weirs) located in the infiltration basin. Runoff from the rest area parking lot and access roads are collected in a separate drainage system that does not empty into the basin.

2.5.2 Aquifer Properties

The Plymouth-Carver aquifer that underlies the Plymouth research site is part of the Wareham Outwash Plain, which slopes to the south or southwest. Figure 2-4 shows a map of the Plymouth-Carver aquifer. The site is located in the southeastern corner of the Plymouth-Carver aquifer. The aquifer consists primarily of a fine to coarse saturated grained glacial sand and gravel, with increasing silt near the bedrock interface. The outwash plain is bounded by glacial till and bedrock hills to the west, by the Cape Cod canal and Buzzards Bay to the south, and by Cape Cod Bay to the north and east (USGS, 1996).

Bedrock is highly fractured throughout the research site, and it is predominately granitic in composition (USGS, 1996). Regional depth to bedrock ranges from approximately 100 ft above msl in the southwestern corner of the aquifer, to about 200 ft below msl along the eastern coast (Hansen and Lapham, 1992). Drilling near the

Hansen and Lapham (1992) used a porosity of 0.28 when modeling the Plymouth-Carver aquifer material, and reported a mean specific yield, S_y , of 0.16. Specific yield (S_y) is the decrease in the volume of water stored in a vertical column that extends across the thickness of an aquifer of unit cross-sectional area, per unit decline in head; it is always less than the soil porosity because some water will remain held in pore spaces by capillary forces (Fitts, 2002). Permeability of the aquifer material at the research site was listed between 1.5×10^{-10} and $2.5 \times 10^{-11} \text{ m}^2$.

Meyer (1999) indicated a porosity (n) of 0.33 and a calibrated permeability of $9.9 \times 10^{-11} \text{ m}^2$ for the site aquifer material. Ostendorf *et al.* (2004) stated that the porosity ranged from 0.25 and 0.35 for the site aquifer material. Slug testing revealed that the permeability of the aquifer material ranged between $7.2 \times 10^{-11} \text{ m}^2$ and $2.3 \times 10^{-10} \text{ m}^2$ (Ostendorf *et al.*, 2005b).

According to Meyer (1999), native sand fill of the Carver coarse sand series (Mesic, uncoated Typic Quartzismment) was used to build the foundation beneath the highway road bed. Fill areas sloping away from the road bed were covered by a 0.20 m layer of loamy sand fill that was grayish brown with loose texture, which was planted with grass to reduce soil erosion. The fill layer was less than 2 m within the site area, and it was assumed not to interfere with ambient groundwater flow. The fill was uniform with a mean grain size diameter of 1.0 mm, and dry soil density ρ_s of $2,650 \text{ kg/m}^3$.

2.5.3 Aquifer Hydrology

The Plymouth-Carver aquifer is recharged mostly by precipitation, and to a lesser extent, from infiltration of runoff and recharge from kettle ponds (Hansen and Lapham, 1992). Fitts (2002) suggested that for the Cape Cod area, groundwater recharge could be as much as 50% of precipitation. The average annual precipitation for the region was estimated to be 1.47 m/yr (NCDC, 1991). According to Ostendorf *et al.* (2004), the ambient recharge rate ($\epsilon\lambda$) for the site was 2.14×10^{-8} m/s (675 mm/yr), or 47% of that typical average annual precipitation rate. Hansen and Lapham (1992) estimated the rate of groundwater recharge to coarse-grained deposit to range from 26 to 28 in/yr, or 660 to 710 mm/yr. Total annual recharge to the Plymouth-Carver aquifer was estimated to average 120 MGD, or approximately $450,000 \text{ m}^3/\text{d}$ (USGS, 1996).

Monthly rain and snowfall records from August 2003 through July 2004 were gathered from rain gauges located in and around the infiltration basin, and are summarized in Table 2-2. Appendix A contains precipitation records for this period of time.

Groundwater in the aquifer is discharged by drainage to surface water bodies, pumping for bog irrigation, evapotranspiration, and evaporation from the water table (USGS, 1996). Average groundwater discharge to rivers and streams is about $139 \text{ ft}^3/\text{sec}$ or $4 \text{ m}^3/\text{sec}$ (Hansen and Lapham, 1992).

The water table is relatively flat compared to land surface topography, and water table altitudes fluctuate within a range of about 1.5 to 2 ft, or 0.46 to 0.60 m (USGS, 1996). Groundwater generally flows to the south (Meyer, 1999; Sullivan, 2001).

Table 2-2 Monthly Precipitation Recorded, August 2003 – July 2004

Date	Accumulated Precipitation			
	Basin rain gauge inches	m	Cranberry Station inches	m
Aug-03	2.57	0.78	2.82	0.86
Sep-03	1.93	0.59	2.37	0.72
Oct-03	4.79	1.46	5.23	1.59
Nov-03	2.17	0.66	2.94	0.90
Dec-03	5.89	1.80	5.99	1.83
Jan-04	1.63	0.50	1.80	0.55
Feb-04	2.59	0.79	2.41	0.73
Mar-04	2.46	0.75	2.21	0.67
Apr-04	4.95	1.51	5.54	1.69
May-04	2.26	0.69	2.80	0.85
Jun-04	1.81 *	0.55	1.65	0.50
Jul-04	2.26	0.69	2.73	0.83

*Note: In June 2004, the basin rain gauge had a gap in data received, and data from the Cranberry Station for that time period supplemented the basin gauge data.

2.5.4 Groundwater Quality

The chemicals of interest in this project were dissolved Na^+ , Cl^- , Ca^{+2} , and Mg^{+2} . These conservative ions are found in naturally in groundwater and on soil coatings, and in the road deicers (NaCl , CaCl_2 , CMA) applied to highway SR25. Ambient ion concentrations were determined by averaging concentrations reported from August 2003 through July 2004 at monitoring wells located upgradient of the site that were determined to be clean upon review (UB101, UB102, UB203 – UB205, UC101, UC102, UC203, UC204). These ion data are in Appendix B. The ambient concentrations were comparable to the ambient values determined by Meyer (1999), as is demonstrated in

Table 2-3. Ambient concentrations did not appear to vary seasonally. The ambient level of specific conductivity was 86 $\mu\text{S}/\text{cm}$, which was slightly higher than the value of 59 $\mu\text{S}/\text{cm}$ found by Meyer (1999) for wells located in the basin area. Perhaps the specific conductivity has become slightly elevated in some of the upgradient wells (located adjacent to the highway) due to shoulder runoff from the highway.

Table 2-3 Ambient Ion Concentrations

Ion	mg/L	
	Mean Concentration August 2003 – July 2004	(Meyer, 1999) August 1997 – September 1998
Ca^{+2}	1.0	1.4
Cl^-	12.9	10.3
Mg^{+2}	1.0	1.5
Na^+	9.6	6.7

3 MATERIALS AND METHODS

There were many sources of data available for modeling the aquifer at the Plymouth site. The following section describes the field and laboratory methods used to gather data from November 2002 through November 2004. Hydraulic head data from August 2003 through July 2004 was used to calibrate the numerical model. Specific conductivity data from November 2002 through November 2004 and ion data from November 2002 through September 2004 was used in a hindcast analysis.

3.1 GROUNDWATER AND SURFACE WATER SAMPLING PROCEDURES

Groundwater samples were collected monthly from monitoring wells at the site. The samples were screened in the field for pH and specific conductance and later analyzed in the laboratory for major cations and anions. These wells were also monitored for groundwater table elevations and DO. In addition, surface water samples were collected from the exit weir located in the western part of the infiltration basin (West Weir); the preparation of the surface water samples was the same as that of the groundwater samples. The water samples used for this project were collected from ninety-one wells located in the general basin area, from November 2002 through September 2004. Figure 3-1 is a map showing the locations of the groundwater sampling wells and the West Weir. In addition, water level measurements recorded at twenty wells and seven surface water locations near the Mann cranberry bog, between August 2003 and July 2004, were used to calibrate the model.

3.1.1 Full Purge Groundwater Sampling from Observation Wells

Groundwater samples were collected in accordance with ASTM D 4448-85a (1996) procedures as part of a larger full-scale site characterization project. Sampling began by unlocking and opening the wells, removing the PVC caps, and measuring the depth to the water table with weighted measuring tape (ASTM, 1996). The depth to water measurements were recorded on a field sheet like that in Figure 3-2.

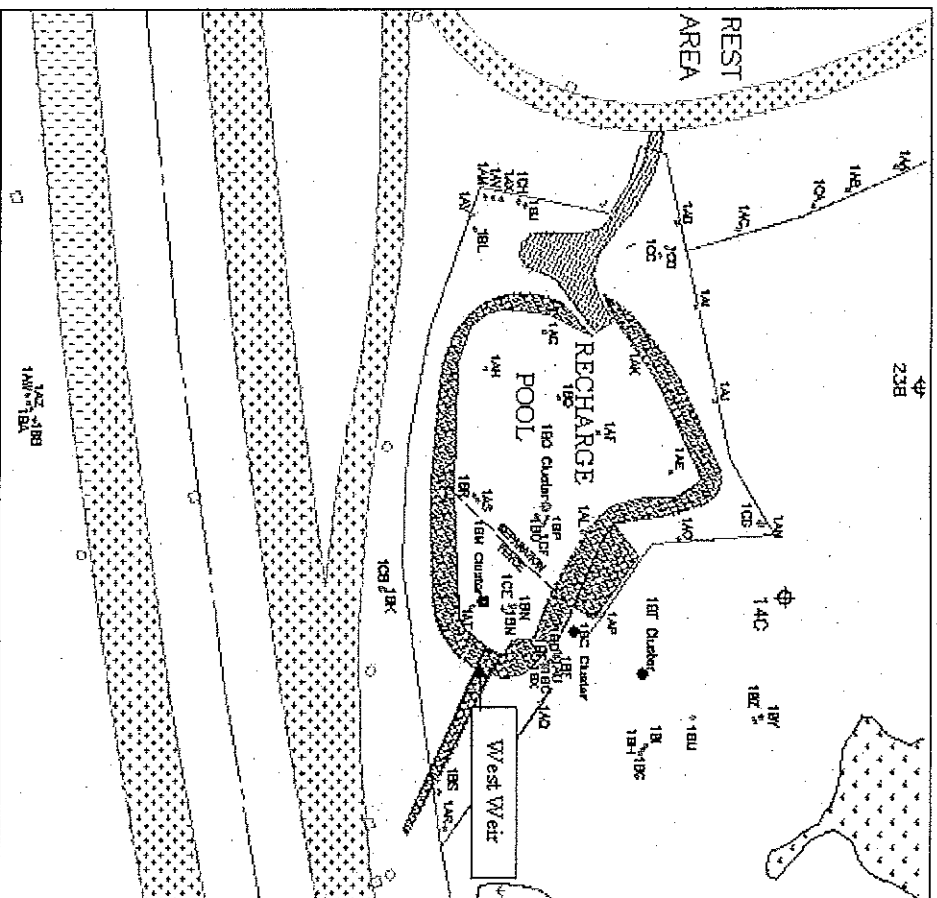


Figure 3-1 Groundwater and Surface Water Sampling Locations

Plymouth Groundwater Quality Sampling						Date: _____					
Well ID	PV (gal)	Depth to Bottom of Screen (ft)	WL from TOR	DO (mg/L)	Temp. (C)	Well ID	PV (gal)	Depth to Bottom of Screen (ft)	WL from TOR	DO (mg/L)	Temp. (C)
AA	2.5	15.63				BMF	7	29.81			
AB	3	13.8				BMG	8	32.73			
AC	3	13.08				BMH	8.5	35.54			
AD	3	11.69				BN	12.5	26.44			
AE	5	11.92				BO	37	76.73			
AF	5	11.86				BOa	3	14.59			
AG	5	11.63				BOb	4	17.6			
AH	5	11.89				BOc	4.5	20.42			

Figure 3-2 Water Level Field Sheet

A one-way check valve was attached to the end of a length of polypropylene tubing. The tubing varied in length from approximately 5 to 15 ft (1.5 to 4.6 m). The tubing was connected to a four-stroke gasoline-powered surface pump (Honda Model WX10) with a CamLoc™ coupling. A 0.625-inch (1.6 cm) diameter garden hose was attached to the exit port of the pump. The hose emptied into a five-gallon bucket that was used to measure the volume of water purged from the well.

Three well volumes were purged from all wells except for the cluster wells, where 1.5 well volumes were purged. Purging the wells in this manner ensured that the samples collected were representative of fresh groundwater. Each foot (or 0.3 m) of 2-inch (5 cm) PVC well casing contains 0.16 gallons (0.6 L) of water. Water samples were collected into 400 mL plastic cups (Cole Palmer; Vernon Hills, IL). The polypropylene tube was drained before sampling a new well.

A portion of the water sample was split into vials for analysis of cations and anions as described in Section 3.2. That sample was assigned a unique number. The rest of the sample was measured for pH, temperature, and specific conductance that was recorded on a field sheet like that illustrated in Figure 3-3.

Plymouth Groundwater Quality Sampling					Date:				
Well ID	Vial ID	Cond. (µS/cm)	Temp. (C)	pH	Well ID	Vial ID	Cond. (µS/cm)	Temp. (C)	pH
AA									
AB					BMF				
AC					BM ₂				
AD					BMT				
AE					BN				
AF					BO				
AG					BO ₂				
					BO ₃				

Figure 3-3 Water Quality Field Sheet

The pH was measured with an Accumet AP-61 portable pH meter (Fisher Scientific), and the specific conductance (standardized to a temperature of 25°C) and temperature were measured with YSI 30 meter (YSI, Yellow Springs, OH). All sample vials were placed in a cooler to be transported back to the University of Massachusetts (UMass). After the well was sampled, DO was also measured before replacing the cap and locking the well.

3.1.2 Water Sample Field Preparation

Water samples to be analyzed for cations were completely extracted in the field. The samples were withdrawn with a 10 cc syringe and were filtered using a 0.45-micron in-line filter (Millipore Corporation; Bedford, MA) into numbered, 1-mL polypropylene autosample vials (National Scientific; Lawrenceville, GA). The vials were pretared with 5 µL of 12.5% nitric acid (HNO₃).

In the field, water samples to be analyzed for anions were placed into clean, numbered 20-mL vials which were pretared with 2 mL of 0.5% sodium azide (NaN₃). Sodium azide was used as a preservative to prevent the aerobic degradation of acetate

during sample collection, transport, and storage. The vial was capped with a screw-on top lined with a Teflon/silicon septum.

3.2 LABORATORY PROCEDURES

Sample vials containing groundwater and surface water samples were stored in refrigerators at a temperature of 4°C during the analysis phase. The UMass Environmental Institute-Civil and Environmental Engineering (TEI-CEE) Cooperative Environmental Analysis Laboratory analyzed the cation and anion samples.

3.2.1 Laboratory Groundwater Sample Preparation

The anion samples required further preparation in the laboratory before analysis. The anion vials were weighed on a scale (Sartorius Corporation; Edgewood, NY) to an accuracy of 2 decimal places (0.01 g) before the samples were extracted again. The samples were withdrawn with a 3 cc syringe and were filtered using a 0.45-micron in-line filter (Millipore Corporation; Bedford, MA) into numbered, 2-mL glass autosample vials (National Scientific; Lawrenceville, GA).

3.2.2 Sodium, Magnesium, and Calcium Detection by Ion Chromatography

Filtered water samples were analyzed for cations that included Na^+ , Mg^{2+} , and Ca^{2+} using a Dionex DX-600 Ion Chromatography (IC) System (Dionex Corporation; Sunnyvale, CA)¹. The system included: a GP-50 gradient pump, a CD-25 conductivity detector, an EG-40 Eluent Generator, a CS12-A cation exchange column, a CSRS-ULTRA cation suppressor, and an AS50 autosampler. Dionex Peaknet Software recorded the data.

Degassed, deionized, ultrafiltered (DIUF) water and 18 mM methane sulfonic acid (MSA) were used as eluents. A cation analysis method program that was developed by Dionex detected the cations of interest. The program used a run time that ranged from 21 to 28 minutes (depending on instrument performance and the age of the column) with the 18 mM MSA eluent.

Once every thirty days, dilutions of known standard solutions were performed and run on the IC. The dilution concentrations chosen represented the concentrations that were expected to be observed. The peak area response was calibrated to the known concentration, giving elution times for each cation species and a peak area for each dilution. Calibration was also performed any time the operating parameters on the instrument changed or if the QA/QC was reported out of an acceptable range (see Section 3.6.2). The peak area for each dilution was plotted against the known concentration to develop a linear regression calibration curve. A typical cation chromatograph is on Figure 3-4, and a typical magnesium calibration curve is on Figure 3-5.

¹ Potassium was also analyzed in the cation samples, but potassium concentrations were not evaluated in this project.

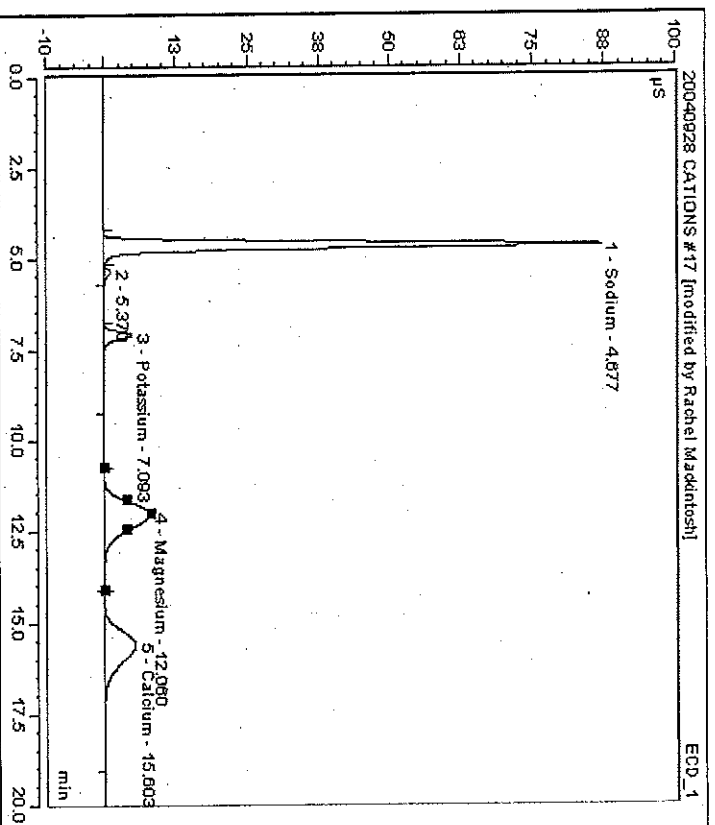


Figure 3-4 Typical Cation Chromatograph

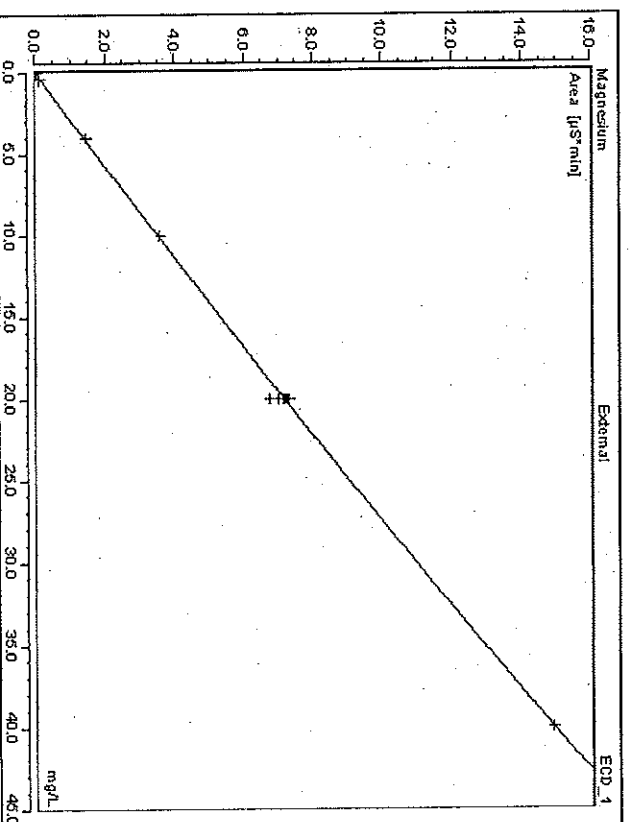


Figure 3-5 Typical Magnesium Calibration Curve

Groundwater anion concentrations were calculated based on the calibration curve and the elution times found for each cation. The concentration (C) was found as shown in Equation 3-1:

$$C = A_{pk} \times RF \quad (3-1)$$

where A_{pk} was the peak area and RF was the response factor for the ion.

3.2.3 Chloride Detection by Ion Chromatography

Filtered water samples were analyzed for anions that included Cl⁻ using a Dionex DX-500 IC System (Dionex Corporation; Sunnyvale, CA)². The system included: a GP-50 gradient pump, a CD-25 conductivity detector, an AG-15 guard column, an Ion Pac AS1-15 analytical column, an ASRS-ULTRA II anion suppressor set in recycle mode, an AS550 autosampler, and an EG eluent generator. Dionex Peaknet Software recorded the data.

Degassed DIUF water and 36 mM potassium hydroxide (KOH) were used as eluents. An anion analysis method program that was developed by Dionex detected the anions of interest.

As with the cations, dilutions of known standard solutions were performed and run on the IC once every thirty days. The dilution concentrations chosen represented the concentrations that were expected to be observed. The peak area response was calibrated to the known concentration, giving elution times for each anion species and a peak area for each dilution. Calibration was also performed any time the operating parameters on the instrument changed or if the QA/QC was reported out of an acceptable range (see

² Acetate was also analyzed in the anion samples, but acetate concentrations were not evaluated in this project.

Section 3.6.2). A typical anion chromatograph is on Figure 3-6, and a typical chloride calibration curve is shown on Figure 3-7.

Groundwater anion concentrations were calculated based on the calibration curve and the elution times found for each anion. The adjusted concentration (C^*) found was corrected to account for dilution and pretaring, as shown in Equation 3-2:

$$C^* = A_{pk} \times RF \left[\frac{M_{azide} + M_w}{M_w} \right] \quad (3-2)$$

where M_{azide} was the mass of the azide preservative, and M_w was the mass of the water sample.

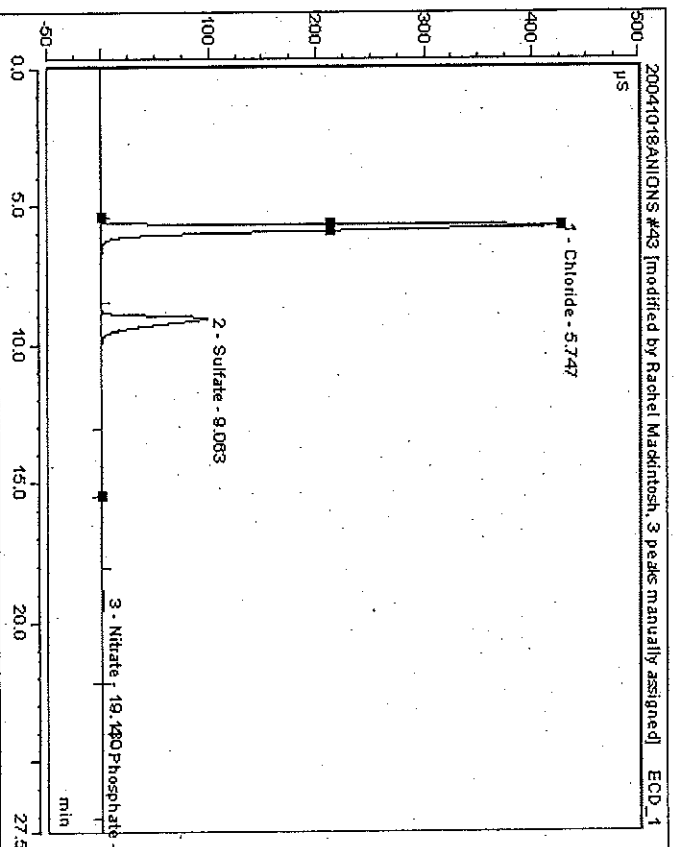


Figure 3-6 Typical Anion Chromatograph

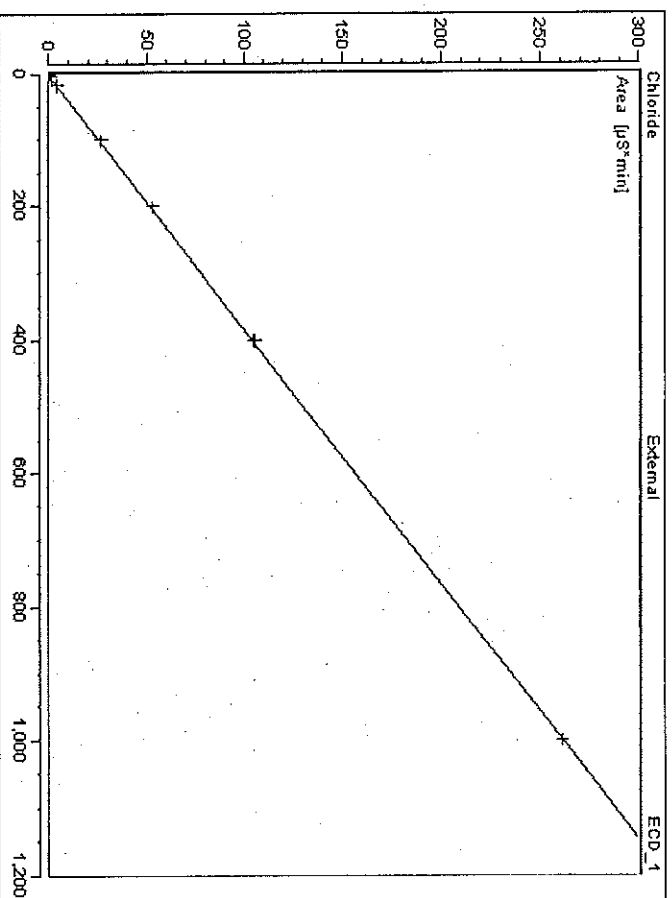


Figure 3-7 Typical Chloride Calibration Curve

3.3 PERMANENT CONDUCTIVITY POINT MEASUREMENTS

Electrical conductivity was measured at nine permanent conductivity point (PCP) locations in and around the infiltration basin, on an approximate biweekly basis. This study used PCP data from November 2002 to November 2004, which are located in Appendix C. Figure 3-8 is a map showing the PCP locations.

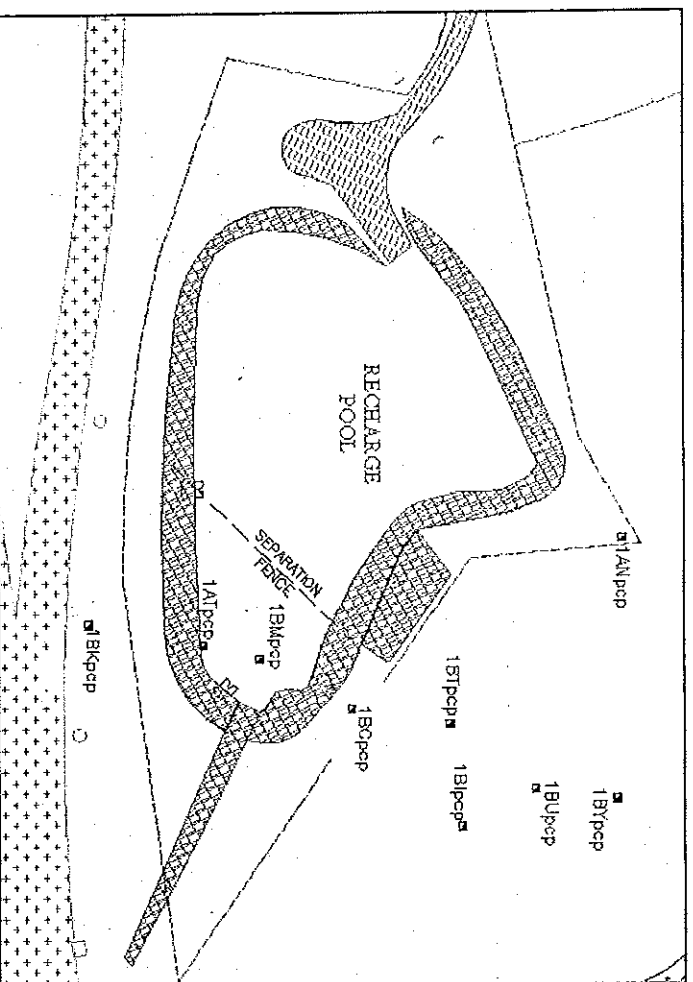


Figure 3-8 Permanent Conductivity Point Locations

The PCP system was a prototype groundwater electrical conductivity detection system developed by the UMass Geotechnical Group. The PCP system acts as a long conductivity meter permanently installed in the aquifer, and was designed to avoid the process of physically collecting a groundwater sample to measure conductivity (Kelley, 2003).

According to Kelley (2003), the PCP conductivity cell consisted of two brass screws serving as the electrodes with an electrical wire attached between the electrode. The cell was mounted to a rigid 1 inch (2.5 cm) polyvinyl (PVC) pipe. The PCP electrodes were also encased in a 2-inch (5 cm) diameter, 5-inch (12 cm) long PVC groundwater well screen with cut 5 cm (2-inch) diameter PVC well cap on the top and bottom of the screen. The parts of the lead wires from the PCP conductivity cells that stuck out of the ground were attached to a terminal block in a wooden housing unit.

A YSI Model 33 S-C-T meter (YSI, Yellow Springs, OH) was used to measure the conductivity in the field. The meter was modified with alligator clips so that the clips could be attached to the lead wires of the pcg conductivity cell to make a measurement (Kelley, 2003). The field measurements were noted on a sheet like that shown on Figure 3-9.

Number	1AT	IBM	IBC	IBT	temperature	IBU	IBI	IBY	1AN	IBK
				thermometer temp						
				surface temp						
1										
2										

Figure 3-9 PCP Field Sheet

The field measurements were converted to electrical conductivity values with conversion factors obtained through a calibration procedure. Two series of calibrations were performed on the PCP conductivity cells, both of which were performed by filling a large chamber with native sand and tap water where pore fluid was passed via a continuous flow isolated fluid system (Kelley, 2003). The electrical conductivity was increased by adding salt, and was measured simultaneously with a hand-held meter and the PCP unit. The two sets of conductivity data obtained with each device were correlated to result in conversion factors used to calculate electrical conductivity from the field data. In addition, all conductivity was standardized to a temperature of 25°C to give the specific conductivity.

3.4 WEIR MONITORING MEASUREMENTS

Runoff flow from the highway drainage systems was monitored at five to ten minute intervals using a 90° V-notch weir setup at the drainage outfall known as the West Weir³. This project used weir data recorded from November 2002 to May 2004, which are summarized in Appendix N. A picture of the West Weir is on Figure 3-10.

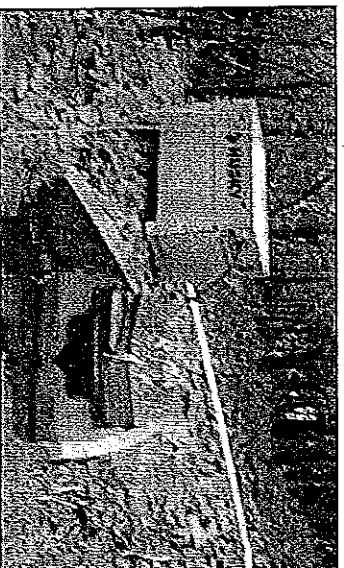


Figure 3-10 West Weir

Data recorded at the West Weir included the water level, specific conductance, and pH of the water flowing through the weir. The drainage system empties into the weir through 3-ft (0.9 m) diameter pipes. The weir was constructed by the UMass metal shop, and is approximately 4 ft (1.2 m) wide and 2.25 ft (0.7 m) tall. The point of the V-notch was approximately 6 inches (15.2 cm) from the base, opening to a maximum width of 3 ft (1 m) and a maximum height of 1.75 ft (0.5 m).

The West Weir was equipped with a model 4230 Bubble Flow Meter (ISCO; Lincoln, NE) that was primarily housed in a waterproof case, with secondary containment

³ The East Weir saw virtually no flow during the period of record, so that only the West Weir monitoring data was evaluated.

provided in a stainless steel housing unit located adjacent to the weir. The logger was equipped with plastic tubes connecting the data logger to a location inside the weir below the water surface.

The mechanism that the flow meter used to measure the water level in the weir employed air bubbles, where an air compressor forces out a metered amount of air through a plastic tube, and the pressure needed to force the air bubbles out was recorded (Ward, 2003). The pressure was converted to a water level once the meter was calibrated for the depth of the tube in the weir. The conversion of the recorded water level or head (H) in the V-notch weir to a flow rate (Q) was performed with Equation 3-3 (Grant and Dawson, 1997):

$$Q = KH^{2.5} \quad (3-3)$$

where K was a constant that depends on the angle of the V-notch and the measurement units. For a flow rate in GPM and a head in feet, the constant K was 1122.

Specific conductance and pH were measured with a YSI 600R multi-parameter water quality sonde (YSI, Yellow Springs, OH), and recorded with the flow meter. The flow, specific conductance, and pH data were downloaded via a cellular phone hookup at the site to a modem located at UMass. The required electricity is supplied by two car batteries stored in the protective housing unit.

3.5 RAIN GAUGE

A Model 674L Logging Rain Gauge (ISCO; Lincoln, NE) was installed near the East Weir on top of a protective housing unit to record precipitation at the site as shown on Figure 3-11. This project used rain gauge precipitation data measured from August

2003 to July 2004 at this gauge, as well as a gauge located at the UMass-Cranberry Station located a few miles west of the site.

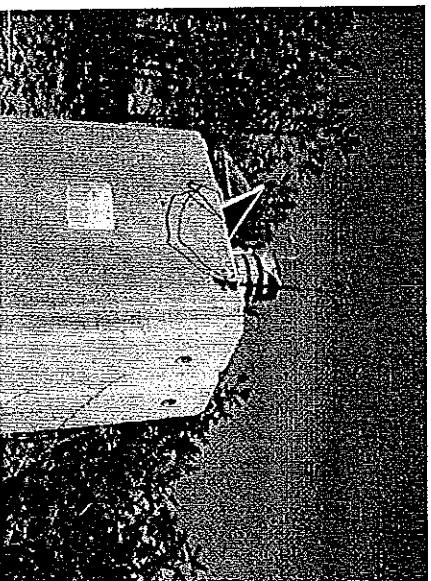


Figure 3-11 Rain Gauge Unit

The rain gauge was a 33-cm tall cylinder with a diameter of 20 cm that was constructed of stainless steel, aluminum, and plastic parts; screens protected all openings (ISCO, 1993). The rain gauge had an accuracy of $\pm 1\%$ of the bucket volume for precipitation rates up to 560 mm/hr.

The rain gauge used a tipping bucket with a capacity of 760 mm/hr and a sensitivity of 0.01 inches (0.25 mm). The gauge was equipped with heating pads to melt frozen precipitation. The data collected by this gauge was compared to the data obtained by the UMass-Cranberry Station located a few miles west of the site.

sample. These techniques were performed to verify the precision of the instrument. The acceptable percent difference between replicate injections and standard solutions was $\pm 10\%$. If the samples exceeded this difference, the samples were analyzed again.

3.6.2.2 Water Blanks

Water blanks were analyzed at least twice when starting up the instrument, and three times at the beginning of each sample run. Water blanks were also analyzed periodically throughout sample runs. The water blank samples used degassed DIUF water, and the water blanks analyzed for cations were also treated with 0.125% HNO_3 to lower the pH below 2.

3.6.2.3 Continuing Calibration Check Standard

A standard solution with a lot number different from those used to create the calibration curve was also analyzed to verify the accuracy of the calibration curve.

3.6.2.4 Method Detection Limits

The MDL is the lowest concentration that can be reliably detected by an analytical instrument for each ion. *Standard Methods* 1030E defined the MDL as:

$$MDL = 3.14 \times s$$

(3-5)

where s was the standard deviation from the sample mean of seven replicate injection samples of a standard solution with a known concentration.

To determine the MDL for each ion, seven replicate injections were alternated between the known standard solution and a water blank. The water blank replicate

injection data was used to determine the level of "noise" for a particular ion. The concentration chosen to be replicated was required to be significantly higher than the level of noise observed for a particular ion.

The MDIs were recalculated every time the ion column was cleaned. The ion columns were cleaned with a mixture that included oxalic acid, acetonitrile, and hydrochloric acid (HCl).

3.6.2.5 Laboratory Spikes

Laboratory spikes were also performed in a manner similar to the field spike procedure indicated in Section 3.6.1.2, where samples were dosed or "spiked" with a known volume of ion standard solution. The recovered ion concentration was compared to the known ion concentration of the standard solution. If the spike recovery for a particular ion did not fall within an acceptable range of 85% to 115%, the ion concentrations for that month were excluded for the project.

3.6.2.6 Ion Charge Balance Analysis

An ion charge balance (Ω) was found to test the neutrality of all water samples, according to Standard Method 1030F (APHA *et al.*, 1995):

$$\Omega = \frac{|z_+| - |z_-|}{|z_+| + |z_-|} \times 100\% \quad (3-6)$$

The charge balances were determined as the sum of ion concentrations (C_i) divided by the ion molecular weight (MW_i):

$$\Omega = \sum \frac{C_i}{MW_i} \times 100\% \quad (3-7)$$

An acceptable range of net charge was $\pm 10\%$ for this project. Any data that did not meet this standard were excluded. Charge balances are indicated with ion data used in Appendix B.

3.6.2.7 Electrical Conductivity Balance

The theoretical electrical balance was determined for each sample in accordance with *Standard Methods* 2510A (APHA *et al.*, 1995), as specified in Section 2.4, with analyzed ion concentrations. The theoretical conductivities were compared to field values, and are listed in Appendix B with corresponding ion data.

4 MODEL DEVELOPMENT

4.1 GOVERNING EQUATIONS

A mathematical model can describe three-dimensional groundwater hydraulics and contaminant fate and transport. Groundwater models are commonly applied to water supply studies and contaminant remediation systems. The steps involved in mathematically modeling groundwater flow include reviewing all existing data, developing a simple conceptual model, and simulating the conceptual model with a mathematical model (Fitts, 2002; Ahlfeld, 2003). The process of modeling is iterative.

The hydraulics of groundwater can be defined by two governing equations. For an incompressible fluid like water, the conservation of mass in a porous media is defined by:

$$\frac{\partial \rho q_x}{\partial x} + \frac{\partial \rho q_y}{\partial y} + \frac{\partial \rho q_z}{\partial z} - \rho R + \frac{\partial \rho n}{\partial t} = 0 \quad (4-1)$$

where q_x , q_y , and q_z are the components of the specific discharge; R is the recharge; ρ is the density of the fluid flowing through the media (e.g., water); x , y , and z are the distances in each respective direction; and t is time. If flow is steady-state, the last term on the left-hand side of equation 4-1 may be excluded. Darcy's law describes the specific discharge through a porous media. It is defined as follows if the permeability is isotropic (Fitts, 2002):

$$q = -\frac{\rho_w g k}{\nu} \left(\frac{\partial h}{\partial x} + \frac{\partial h}{\partial y} + \frac{\partial h}{\partial z} \right) \quad (4-2)$$

where g is the gravitational constant, ν is the dynamic or kinematic viscosity of the fluid (water), and h is hydraulic head.

When it is reasonable to assume that groundwater flow is two-dimensional in the vertical plane, a streamline analysis can be made in a vertical cross-section in the x , z plane, which is one unit thick in the y -direction. Streamlines are imaginary lines that trace the advective flow paths traveled by water molecules. Laplace's equation for steady hydraulic head in two dimensions governs the head (Fitts, 2002):

$$\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial z^2} = 0 \quad (4-3)$$

In a steady, homogeneous, isotropic (i.e. permeability is constant) aquifer, streamlines are perpendicular to lines of constant head. A flow net is a graphical representation for estimating the distribution of hydraulic heads, discharges, and streamlines in steady two-dimensional groundwater flow (Fitts, 2002). Solutions of the Laplace equation include harmonic functions and conjugate, perpendicular harmonic functions. These corresponding harmonic functions are known as stream functions (Fitts, 2002). A limiting streamline separates contaminated basin recharge water and ambient groundwater.

The transport of solute contaminants in groundwater is primarily governed by advection. However, groundwater contaminants mix and disperse due to both molecular diffusion, and mechanical dispersion caused by differences in velocities (Fitts, 2002). Molecular diffusion is governed by Fick's first law, which for the x -direction is shown as

$$F_{dx} = -nT_x^* D_{mol} \frac{\partial C}{\partial x} \quad (4-4)$$

where F_{dx} is the diffusive solute mass flux in the x-direction, T_x^* is the tortuosity of groundwater in the x direction, and D_{mol} is the molecular diffusion coefficient.

According to Fitts (2002), mechanical dispersion has not been shown to behave according to any similar fundamental law, since it depends on too many complex processes and factors. Mechanical dispersion is usually much larger in the direction of groundwater flow than it is transverse to flow. Mechanical dispersion depends on spatial and transient variations in velocities caused by heterogeneity of the soil medium and transient flow phenomena. An example of transient flow phenomena is recharge from urban runoff.

In light of these complexities, molecular diffusion and mechanical dispersion are often known collectively as macrodispersion, where the macrodispersive flux in the x-direction (F_{mx}) are modeled by a form of Fick's law,

$$F_{mx} = -nD_{mx} \frac{\partial C}{\partial x} \quad (4-5)$$

where D_{mx} is the macrodispersion coefficient in the x direction. It is defined as

$$D_{mx} = \alpha_x |\bar{v}| + T_x^* D_{mol} \quad (4-6)$$

where α_x is the dispersivity in the x-direction, and $|\bar{v}|$ is the magnitude of the average linear groundwater flow pore velocity (Fitts, 2002). Pore velocity (v) is defined as

$$v = \frac{U}{n} \quad (4-7)$$

where U is the apparent or superficial velocity. Macrodispersion coefficients and dispersivities are fitting parameters, and are not representative of any real physical properties. Furthermore, the magnitude of dispersivity found will depend on the scale of

the experiment used to measure it. Typical values for laboratory tests range from millimeters to centimeters, but dispersivity values can be as high as tens of meters in a field scale model. A curved coordinate system is often aligned with the flow direction for transport models, where α_x and D_{mx} refer to the longitudinal direction. Meanwhile, α_y , D_{my} , α_z , and D_{mz} apply to two orthogonal directions transverse to the longitudinal groundwater flow direction.

Contaminant transport can be represented with the three-dimensional advection-dispersion governing equation,

$$\nabla \cdot D_m \nabla C - \nabla \cdot (CU) = n \frac{\partial C}{\partial t} \quad (4-8)$$

Hydrologists often simplified the complicated expressions described into elegant analytical models. However, beginning in the 1950s, reservoir engineers and applied mathematicians experimented with numerical techniques to solve flow equations algebraically (Bredenhoeft and Hall, 1995). By the 1970s, digital computers facilitated the use of cumbersome numerical solutions to simultaneously solve the expressions for flow and later contamination, thereby allowing for a more accurate representation of aquifers.

A steady-state numerical model of the research site was created to simulate groundwater flow and contaminant transport in the site aquifer. MODFLOW is a three-dimensional, block-centered modular finite-difference groundwater flow model code developed by the United States Geological Survey, or USGS (Waterloo, 2003). A version of the original model, MODFLOW-2000, was selected to simulate groundwater flow. MODPATH was used to simulate the advective transport of deicer particles and generate streamlines that were plotted as contours. Visual MODFLOW 3.1.0 is a

software package that was used as a graphical interface to support the numeric engines that run the numerical model.

The finite-difference method solves algebraic equations based on the governing equations 4-1 and 4-2. Figure 4-1 (Pollack, 1989) gives a finite-difference cell defining the x-y-z and i-j-k coordinate systems.

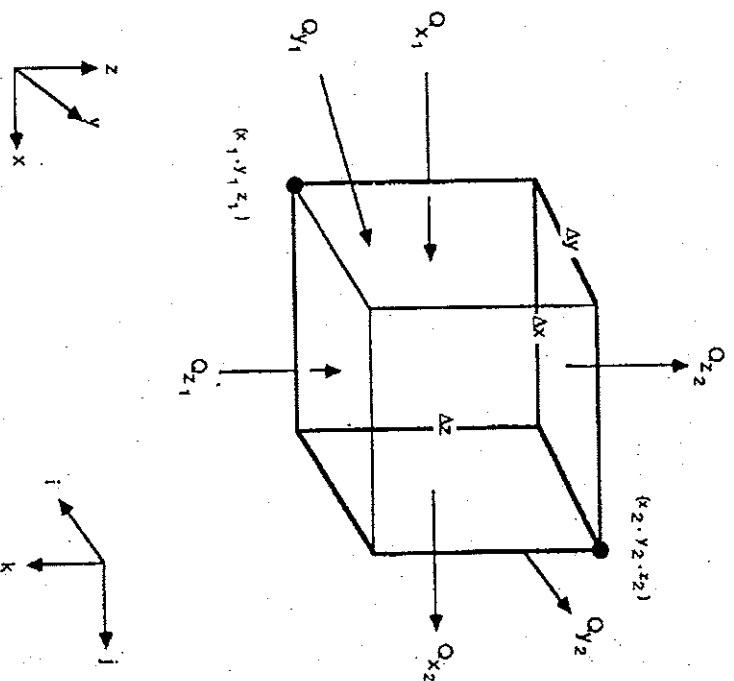


Figure 4-1 Finite Difference Cell
(Pollack, 1989)

Equation 4-9 gives a mass balance equation (Pollack, 1989) that can be written for the cell in Figure 4-1:

$$n \left\{ \frac{(v_{x_2} - v_{x_1})}{\Delta x} + \frac{(v_{y_2} - v_{y_1})}{\Delta y} + \frac{(v_{z_2} - v_{z_1})}{\Delta z} \right\} = \frac{Q}{\Delta x \Delta y \Delta z} \quad (4-9)$$

where $x_1, x_2, y_1, y_2, z_1, z_2$ are the cell faces perpendicular to the respective direction (e.g., the x_1 face is perpendicular to the x-direction); and $\Delta x, \Delta y$, and Δz are the dimensions of the cell. The left side of equation 4-9 is the net volume rate of outflow per unit volume. The average linear velocity components inward (v_{x1}, v_{y1}, v_{z1}) and outward (v_{x2}, v_{y2}, v_{z2}) are found by dividing the volume flow rate inward in the x-direction (Q_{x1}) by the cross-sectional area of the face and the porosity, as demonstrated for the x_1 face in the following equation:

$$v_{x_1} = \frac{Q_{x_1}}{n \Delta y \Delta z} \quad (4-10)$$

Darcy's law is substituted for each flow term in equation 4-9, the hydraulic heads are simultaneously solved for the node centered in each cell, and the intercell flow rates are thus determined.

Visual MODFLOW uses a built-in data interpolation, gridding, and contouring component to import and interpolate field data. Interpolation methods supported by Visual MODFLOW include Inverse Distance Squared method, the Natural Neighborhood method, and Kriging (Waterloo, 2003). The Inverse Distance Squared interpolation method, where a weighting factor is applied to data depending on its distance from the grid cell that is inversely proportional to the distance squared, was used for this model. Several solvers are available with Visual MODFLOW to solve the numerical flow equations, including the Slice-Successive Overrelaxation Package (SOR), the Strongly Implicit Procedure Package (SIP), and the WHS solver. The WHS solver was chosen for this model, which uses a Bi-Conjugate Gradient Stabilized (Bi-CGSTAB) acceleration

routine with Stone incomplete decomposition for preconditioning of the flow partial differential equations (Waterloo, 2003).

A particle tracking post-processing package was developed to compute three-dimensional streamlines based on output from steady-state simulations obtained with a finite difference groundwater flow model like MODFLOW (Pollack, 1989). MODPATH calculates the streamlines and MODPATH-PLOT presents the streamlines graphically, both of which are FORTRAN programs. Since MODFLOW uses a block-centered approach that assumes properties within a cell are homogeneous, MODPATH uses a semi-analytical particle tracking scheme. This tracking scheme assumes each directional velocity component varies linearly within a grid cell in its own coordinate direction, allowing streamlines to be traced and travel times between points along a streamline to be computed (Pollack, 1989; Waterloo, 2003). The position of the particle for each coordinate direction was derived by Pollack (1989) for each coordinate direction. The derivation is briefly summarized here for the x-direction, and it is analogous for the y and z-directions. The direct integration of the rate of change in a particle's x-component of velocity (vx_p)

$$\left(\frac{dv_x}{dt}\right)_p = \left(\frac{dv_x}{dx}\right)vx_p \quad (4-11)$$

where x_p is the x-position of the particle, and the relation

$$\frac{dv_x}{dx} = A_x \quad (4-12)$$

where A_x is the area of the x-cell face, eventually results in this expression for the exit x-position of a particle:

$$x_p(t_2) = x_1 + \left(\frac{1}{A_x}\right) \{v_{x_p}(t_1) \exp(A_x \Delta t) - v_{x_1}\} \quad (4-13)$$

where t_1 is the time when the particle enters the cell, t_2 is the time the particle leaves the cell, Δt is the time the particle remains in the cell, and x_1 is the initial x-position of the cell. These relationships are illustrated on Figure 4-2 (Pollack, 1989).

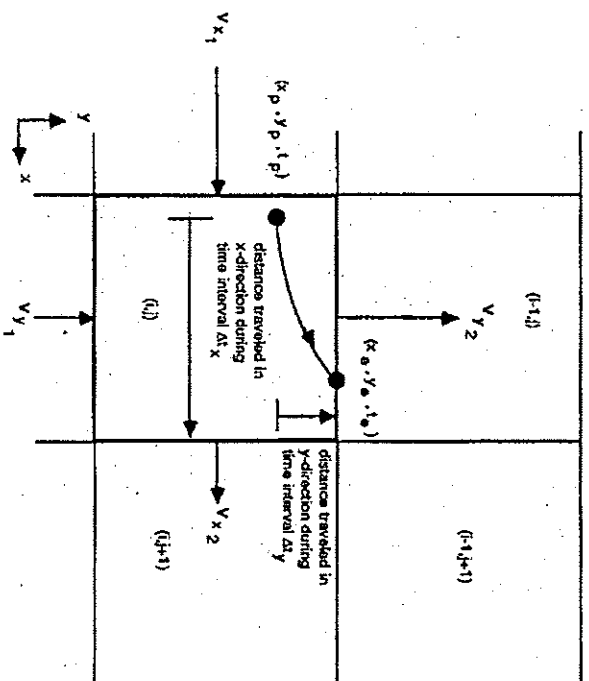


Figure 4-2 Schematic of the Particle Exit Point and Travel Time in a Two-Dimensional Cell (Pollack, 1989)

4.2 CONCEPTUAL MODEL

In reality, the subject site aquifer is a complex, heterogeneous system that can never be fully characterized, even with the wealth of data available for the subject site. Certain assumptions were made about the site aquifer to build a model that would be simple to use but would represent the important properties of the aquifer.

Review of monthly hydraulic head values over the past several years at the site revealed that head values do not fluctuate significantly over the course of a year. Steady-state flow conditions have been assumed at the subject site for past studies (Ostendorf *et al.*, 2004). Therefore, steady-state flow conditions were established to simplify the model.

The conceptual model assumed a homogenous isotropic aquifer, where the permeability was constant across the entire area and depth of the domain, in all directions. Previous modeling of the site aquifer (including Sullivan, 2001; Fauteux, 2002; Ward, 2003) also established a homogeneous, unconfined aquifer when modeling the site. The aquifer was considered to be unconfined with groundwater recharge resulting from ambient precipitation, infiltration from highway runoff, and infiltration from highway runoff effectively routed to the infiltration basin. The model steady ambient recharge rate was found by applying results obtained from measuring tritogenic helium and tritium concentrations in groundwater collected in the infiltration basin area (Meyer, 1999), and it is indicated in Section 2.5.3.

Figure 4-3 (Pollack, 1989) presents a conceptualization of the model domain, which can be considered a control volume that is part of the larger regional aquifer. The

top face of the model control volume is the ground surface. Recharge flux is applied to top unconfined layer to be infiltrated to the groundwater table.

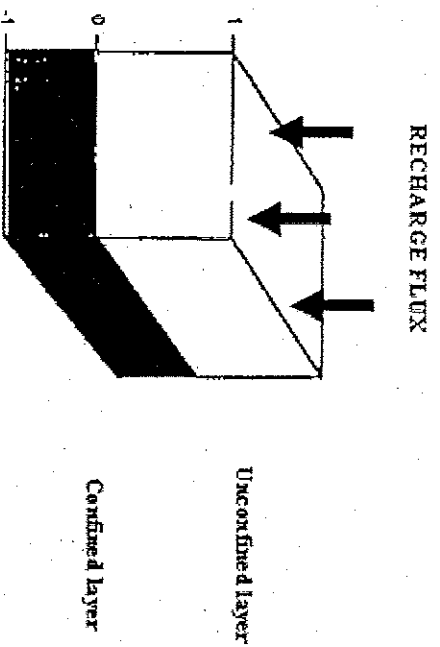


Figure 4-3 Model Domain Conceptualization
(Pollack, 1989)

Flow into the infiltration basin is caused by runoff routed from approximately 28,260 m² of pavement from SR25 eastbound and westbound lanes and a portion of the median area. Table 4-1 lists the drainage scheme for the paved highway areas designated in Figure 4-4.

Pavement areas on this section of SR25 were sloped to the south so that catch basins located in the adjacent southern shoulders or median areas collect the runoff. Paved areas E, F, B, C, and a small part of 4 (a median area) were designed so that their runoff was routed to the West Weir in the infiltration basin. An additional 9373 m² of

pavement not included in the model domain was also designed to route runoff to the West Weir. This drainage system (I) was demonstrated to be 68% efficient (Ostendorf *et al.*, 2005a).

Table 4-1 Highway Drainage Scheme

Scheme	Description	Drainage Eff (%)	Designation	Type	Station		Pavement		Captured Area
					start	end	length m	eff width* m	m ²
I	Drains to basins south then to W. Weir	68	E	WB lane	556.5	559	75	15.24	1143
			F	WB lane	559	565	180	15.24	2743.2
			B	EB lane	559	565	180	15.24	2743.2
			C	EB lane	565	575	300	15.24	4572
			4	median	565	575	300	12.38	3714
II	Drains to basins in median then to W. Weir	21	G	WB lane	565	575	300	15.24	4572
III	Drains to E. Weir	0	D	WB lane	555	556.5	45	15.24	685.8
			A	EB lane	556.5	559	75	15.24	1143
			H	EB lane	555	556.5	45	15.24	685.8
I†	Not in model domain but drains to W. Weir	68	w of G	WB lane	578	587	270	15.24	4114.8
			w of C	EB lane	575	583.5	255	15.24	3886.2
			w of 4	median	575	578	90	15.24	1371.6
Paved area received by West Weir =									28860

*effective paved road width = 3 x 3.66m travel lanes + 3.04 m breakdown lane + 1.22 m inner paved shoulder

†Pavement not included in model domain only to keep domain smaller.

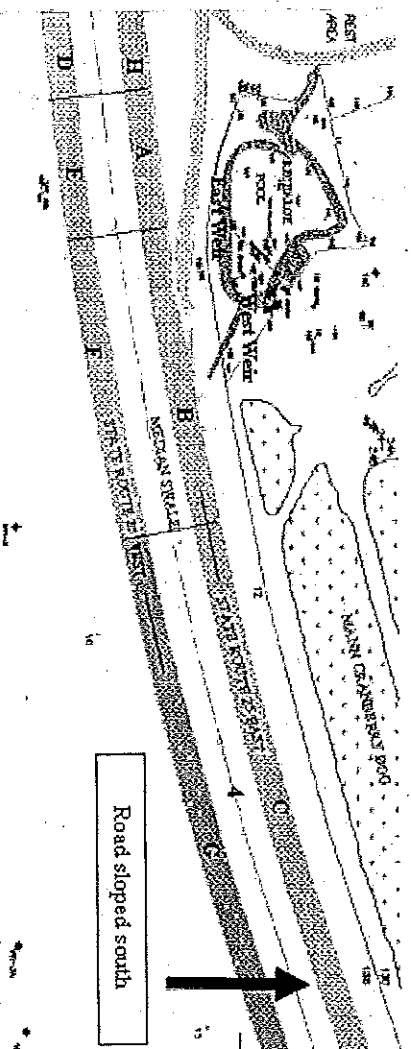


Figure 4-4 Highway Drainage Scheme

The paved area captured (A_p) was defined as:

$$A_p = L_R \times W_e \quad (4-14)$$

where L_R is the roadway length and W_e is the effective width of the paved area. Drainage system II was designed to route runoff from area G (part of the westbound lane) to catch basins located in median area 4. Drainage system II was indicated to be 21% efficient (Ostendorf *et al.*, 2005a). In drainage scheme III, runoff from paved areas A, D, and H was designed to ultimately discharge to the East Weir in the infiltration basin. However, a review of flow data collected at the East Weir shows System III to be virtually inefficient.

In addition, all groundwater was considered mobile within the soil pores, so that the total and effective porosities were equivalent (Fitts, 2002). Since the water table is shallow and the soil grains are relatively coarse in the site aquifer, the specific yield (S_y) was approximated to be the porosity value and was applied across the entire thickness of the aquifer (Fitts, 2002). For further simplification, the boundary between the bedrock surface was considered to be at a constant elevation.

Advective transport of the deicing materials in groundwater was considered to be the dominant mode of contaminant travel. Dispersion and diffusion were thought to be much less significant than advection, and were ignored in this model with the utilization of particle tracking to simulate deicer contamination. According to Pollack (1989), advection models can not be used to find solute concentrations in groundwater because they ignore mixing by dispersion, but they can be a valuable tool for comparing relative magnitudes of solute. The deicing contaminant was assumed to act conservatively based

on modeling results demonstrated by Meyer (1999) for the site, so that adsorption and degradation were not considered.

4.3 HYDRAULIC MODEL DEVELOPMENT

A digital map image of the research site was imported into the MODFLOW model. The model domain included the infiltration basin and monitoring wells located upgradient and downgradient of the basin, covering an approximate area 900 m long in the x-direction by 700 m long in the y-direction. The digital map was placed into the MODFLOW model at an angle of 68° to align the flow of groundwater with the x-direction; therefore, excluding areas not chosen to be part of the model, the approximate domain area was $468,000 \text{ m}^2$. The domain was discretized into a rectangular finite-difference grid with 43 rows in the x-direction and 67 columns in the y-direction. Most grid cells were 20 m by 20 m, but the grid was refined to 10 m by 20 m cells in the highway area and 5 m by 5 m in the infiltration basin area. Cell sizes were varied in this manner to provide better resolution in the regions of interest in the model, the highway and basin areas. Please refer to the plan view of the model domain shown in Figure 4-5.

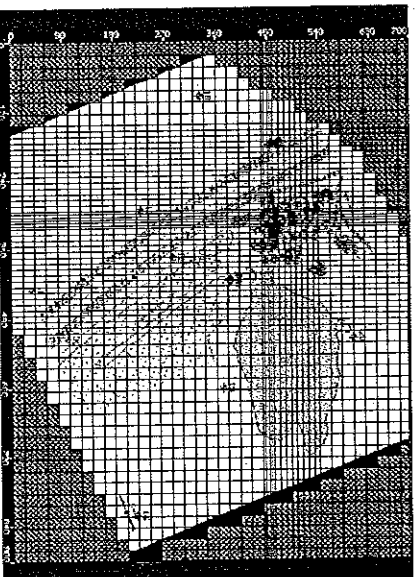


Figure 4-5 Plan View of Model Domain

The maximum aquifer thickness was 40 m, divided into four layers spaced at 10-m intervals. Figure 4-6 shows a cross-section of the vertical layering in the model. Ground surface elevations were imported into MODFLOW, so that the uppermost layer 1 varied in thickness due to the topography, while layers 2 through 4 were constant in thickness (10 m each). Ground surface elevations are in Appendix E. As a result, the total thickness of the aquifer ranged from 32 to 37 m thick. Layer 1 was considered to be unconfined, while the other layers were confined.

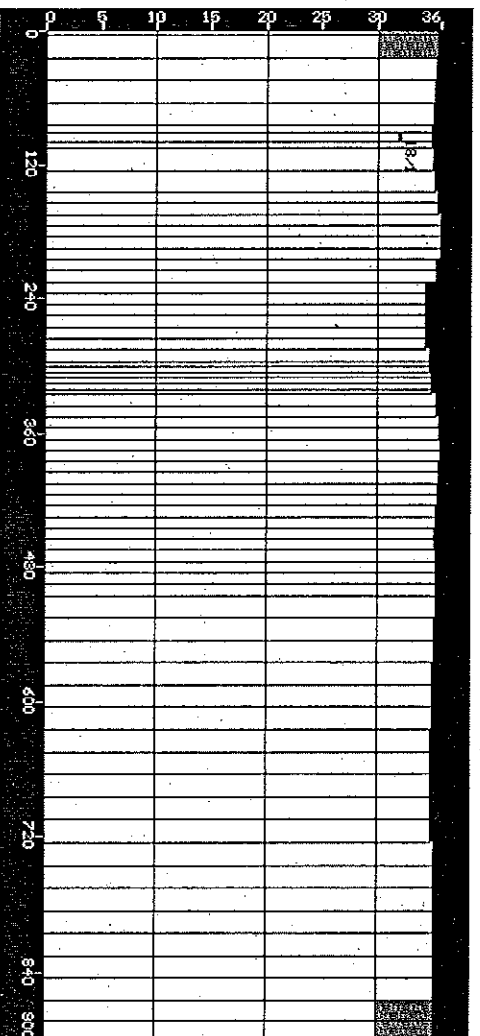


Figure 4-6 Cross-Sectional View of Model Domain

Subsurface investigations at the research site indicated that bedrock can be found at an elevation of 24.9 m below msl (Meyer, 1999). This model assumed the bedrock interface elevation to be constant across the entire domain, and it is set as the datum line ($z = 0$).

4.3.1 Initial Hydraulic Parameters

Table 4-2 lists the initial parameter values used to calibrate the hydraulic model.

Table 4-2 Initial Model Parameters	
Parameter	Value
Specific storage	S_s zero
Specific yield	S_y 0.3
Effective porosity	n 0.3
Bedrock elevation	z_B -24.9 m msl
Aquifer thickness	ζ 32 - 37 m
Layer 1	2 - 7 m
Layer 2	10 m
Layer 3	10 m
Layer 4	10 m
Kinematic viscosity	ν 1.3×10^{-6} m ² /s
Permeability	k 1×10^{-10} m ²

For this steady-state groundwater model, the specific storage term S_s was assumed to be zero. The porosity n was assumed to be 0.3 for the model. Hansen and Lapham (1992) used a porosity of 0.28 when modeling the Plymouth-Carver aquifer. According to Ostendorf *et al.* (2004), the porosity at this specific site within the regional aquifer can range from 0.25 to 0.35; Meyer (1999) used a value of 0.3 when numerically modeling the site aquifer. Since the water table is shallow and the soil grains are relatively coarse at the research site, the specific yield value S_y was approximated to be the porosity value of 0.3. The permeability k was assumed to be a constant value, and the calibration of the permeability is discussed in Section 5.1.3.

4.3.2 Boundary Conditions

The bottom of the aquifer was considered to be the interface between bedrock and the aquifer, and was treated as a no-flow or impermeable boundary.

$$\frac{\partial h}{\partial x} = 0 \quad (\text{at } z_B) \quad (4-15)$$

Water should flow in and out of the vertical sides or plane edges of the cube on Figure 4-3 in the direction of groundwater flow because these sides are in contact with the regional aquifer. Since MODFLOW assumes no-flow boundaries at each vertical side of the model domain, it was necessary to calibrate the outer boundary conditions by comparing calculated hydraulic heads to observed measurements. Hydraulic head values were generated by importing measured field data from August 2003 through July 2004 at monitoring well locations located within the domain. The hydraulic head measurements used to calibrate this model are located in Appendix F.

Figure 4-7 includes hydraulic head contours (in m msl) based on an average of the August 2003 – July 2004 data⁴. Calibration of the specified constant hydraulic head boundary conditions was based on these contours, and is discussed in Section 5.1.1. Hydraulic head values were assigned to the model in terms of the bedrock elevation (24.9 m below msl) acting as the datum line. In other words, a hydraulic head value of 32 m in the model actually represents a head of 7.1 m above msl. Specified head boundaries are indicated on Figure 4-8.

⁴ If irrigation pumping was occurring at a well located just outside the basin area at the Mann Cranberry Bog while hydraulic head measurements were taken, these data were not used in the average.

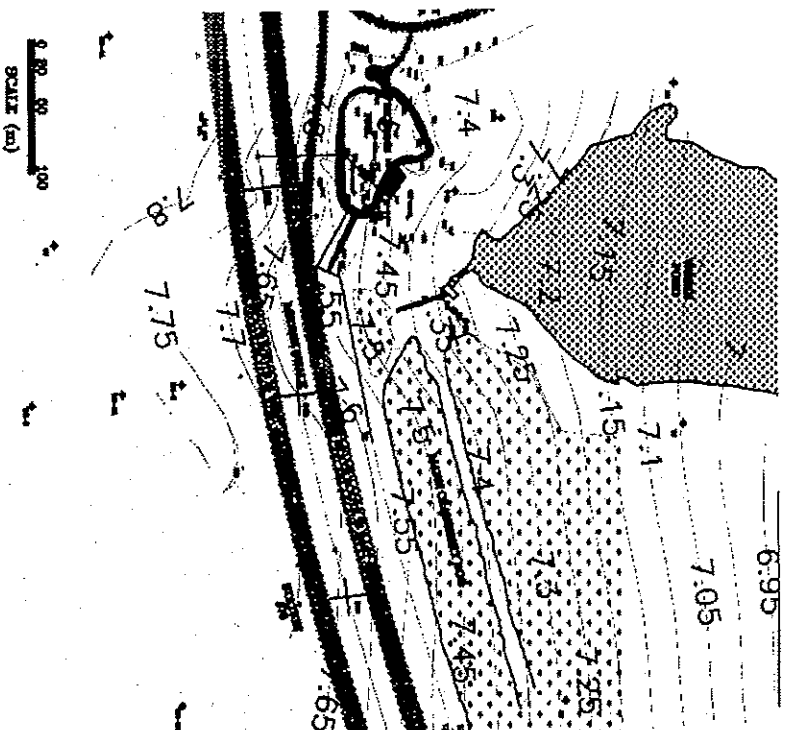


Figure 4-7 Average Hydraulic Head Contours (in m msl) based on August 2003 – July 2004 data

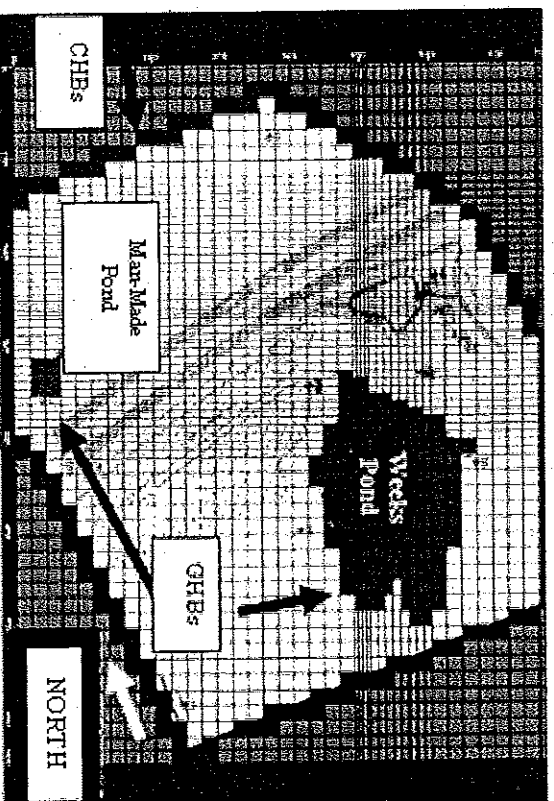


Figure 4-8 Specified Boundary Conditions

The Constant Head Boundary (CHB) condition in Visual MODFLOW sets the head value in a selected grid cell independent of the surrounding cells, acting as an infinite source or sink of water (Waterloo, 2003). Initial CHBs were applied to the edges of the model domain as follows to represent the contours observed in Figure 4-4: a CHB of 32.8 m (7.9 m above msl) was applied along the northern edge of the domain; a CHB of 32.75 m (7.85 m above msl) was applied at the northeastern corner; and a CHB of 31.7 m (6.8 m above msl) was applied at the southwestern corner.

General Head Boundaries (GHB) were used to simulate two surficial water bodies (Weeks Pond and the Man-Made Pond) within the model domain. The CHB condition was not used to simulate the water bodies because it resulted in an unrealistic representation of the streamlines emanating from the infiltration basin (i.e., it curved the streamlines up toward Weeks Pond because the CHB condition provided an infinite source of water to the system). Instead, the GHB condition provided flow into or out of a cell that was proportional to the difference between the head in the cell and the reference head assigned to the external source, and did not act as infinite water source (Waterloo, 2003). The GHB condition requires that boundary head and conductance values be added as input. The boundary head for each water body was specified as the average of hydraulic heads measured from August 2003 through July 2004. For Weeks Pond, the boundary head was 32.2 m, and for the Man-Made Pond, the boundary head was 32.7 m. Conductance (γ) is calculated by MODFLOW as

$$\gamma = \frac{(LxW)x\phi}{D} \quad (4-16)$$

where L is the length of a reach through a cell, W is the width of the cell, ϕ is the vertical hydraulic conductivity of the aquifer material separating the external source/sink from the model grid, and D is the distance from an external source or sink (e.g., a water body just outside the domain) to the model grid. However, a calibrated value can also be used to set the conductance. Since the water bodies of interest exist within the domain, the conductance was calibrated to a value of 1 m^2 . Figure 4-9 (Waterloo, 2003) illustrates a schematic of the GHB condition.

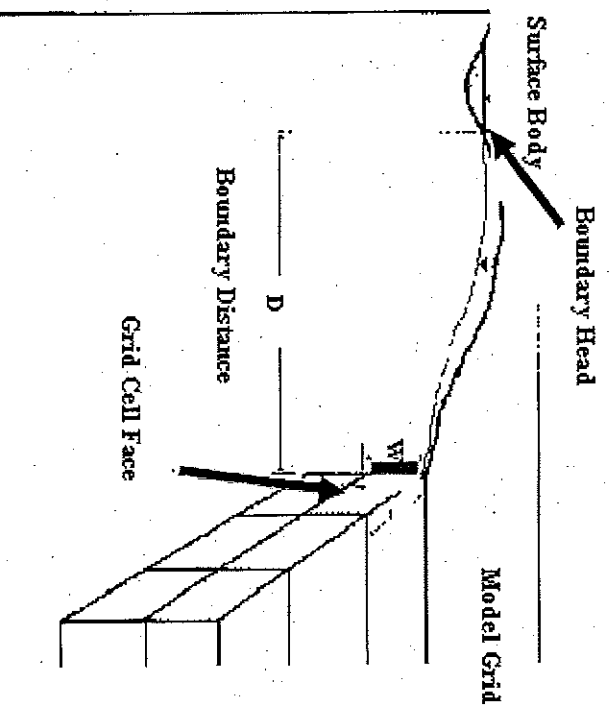


Figure 4-9 General Head Boundary Schematic
(Waterloo, 2003)

Table 4-3 lists the initial boundary conditions used to calibrate the hydraulic model. The final calibrated values of the CHBs are presented in Section 5.1.1.

Table 4-3 Initial Specified Boundary Conditions

Parameter	Model Value	Actual Value
Constant Head Boundaries		
Northern Limit	32.8 m	7.9 m
Northeastern Corner	32.75 m	7.9 m
Southwestern Corner	31.7 m	6.8 m
General Head Boundaries		
Weeks Pond	32.2 m	7.3 m
Man-Made Pond	32.7 m	7.8 m

4.3.3 Recharge Zones

Recharge flux was assigned to the top face of all cells. Recharge zones were used to characterize areas with different recharge rates within the model domain, as shown in Table 4-4. Please note that the recharge zone areas chosen in the model are not the same size as the actual recharge areas. The model recharge rates on these areas were based on the model recharge zone area (A_z) so as to better represent the actual recharge on these areas. The model recharge parameter transformation process was as follows:

According to data collected from a rain gauge station in the basin and from the nearby UMass Cranberry Station (see Chapter 3), the subject site received 35 inches (897 mm) of precipitation between August 2003 through July 2004. This period of record was a little drier than usual; an annual average precipitation of 1.5 m/yr (approximately 4.6×10^{-8} m/s) has been noted for the site (Meyer, 1999). Ostendorf *et al.* (2004) found a steady-state recharge rate ϵ_s of 2.18×10^{-8} m/s for the site.

Table 4-4 Recharge Zones

Recharge Zones	No.	Location Description	Model area	Recharge Rates
Ambient	1	areas excluding 2 - 16	401950 m ²	422 mm/yr
Highway Pavement	2	eastbound, westbound lanes	23400 m ²	zero
Effective Basin	3	west of fence, east of West Weir	250 m ²	62902 mm/yr
Median	4	between stations 565 - 575	7800 m ²	617 mm/yr
North Shoulder	5	between stations 559 - 565	2200 m ²	422 mm/yr
Rest Area Pavement	6	exit ramp, parking lot	10400 m ²	zero
South Shoulder	7	between stations 559 - 565	1200 m ²	730 mm/yr
Median	8	between stations 559 - 565	4600 m ²	502 mm/yr
North Shoulder	9	between stations 565 - 575	4200 m ²	422 mm/yr
South Shoulder	10	between stations 565 - 575	4400 m ²	562 mm/yr
North Shoulder	11	between stations 555 - 556.5	600 m ²	422 mm/yr
South Shoulder	12	between stations 556.5 - 559	1000 m ²	903 mm/yr
Median	13	between stations 556.5 - 559	2400 m ²	486 mm/yr
Median	14	between stations 555 - 556.5	1800 m ²	582 mm/yr
North Shoulder	15	between stations 556.5 - 559	1200 m ²	422 mm/yr
South Shoulder	16	between stations 555 - 556.5	600 m ²	903 mm/yr
SUM			468000 m ²	

Using the typical annual average precipitation value of 4.6×10^{-8} m/s and the

steady recharge rate found, an R of 47% resulted. ϵ_A was based on R:

$$\epsilon_A = RP_A \quad (4-17)$$

where P_A was the annualized precipitation rate. The basin recharge rate ϵ_B was the infiltration rate of highway runoff successfully discharged to the basin area.

Unlike ambient recharge, all basin discharge was considered to be infiltrated to the water table. ϵ_B was determined by:

$$\epsilon_B = \epsilon_A + \sum (E \times P_A \times \frac{A_P}{A_Z}) \quad (4-18)$$

where E is the efficiency of the drainage system, and A_P is the paved area captured. Highway runoff not effectively captured by the drainage system was assumed to infiltrate the southern adjacent areas, at the ambient R of 47%. The runoff recharge rate ϵ_R was

$$\epsilon_R = \epsilon_A + \sum \{(1-E) \times P_A \times \frac{A_P}{A_Z}\} \quad (4-19)$$

The ambient recharge area (Zone 1) comprised the entire domain excluding paved zero recharge areas (Zones 2 and 6), the effective infiltration basin recharge area (Zone 3), runoff recharge areas (Zones 4, 7, 8, 10, 12, 13, 14, and 16), and northern shoulder areas (Zones 5, 9, 11, and 15). The northern shoulder areas were considered to receive only ambient recharge and no highway runoff. The paved zero recharge zones were represented by Zones 2 and 6. Zone 2 included any paved surfaces such as the parking lot of the rest area located near the infiltration basin, and the east and westbound lanes of the Route 25. Zone 6 comprised the rest area off-ramp from the highway, and the portion of the parking lot area included within the model domain. Runoff recharge zones 4, 8, 13, and 14 were grassy median areas (since the paved areas in the medians were small in relation to the grassy areas, the entire medians were treated as pervious surfaces); and runoff zones 7, 10, 12, and 16 comprised the grassy southern shoulder area.

Zone 3 was designated as the effective infiltration basin area. The effective basin area initially selected was a square region 20 m by 20 m with an area of 400 m², but the final calibrated size of the effective infiltration basin was 250 m². Past field observations

have noted an E-shaped puddle during storm events (Ward, 2003). The method used to select the effective basin recharge area and recharge rate for Zone 3 is discussed in Section 5.1.2.

Figure 4-10 indicates the recharge zones used in the model, and Figure 4-10a details the effective basin recharge area. Figure 4-11 shows how the captured pavement areas in Table 4-1 were related to the recharge zones assigned in the model.

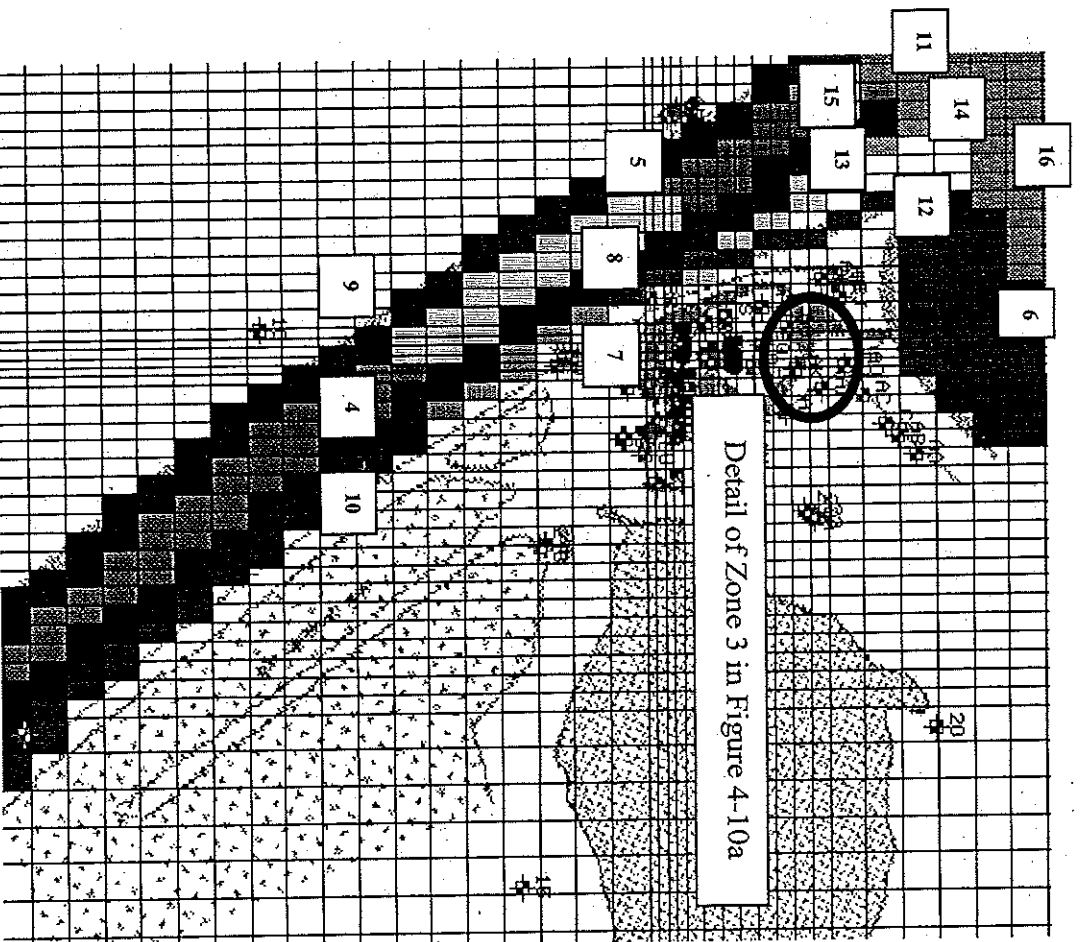


Figure 4-10 Recharge Zones

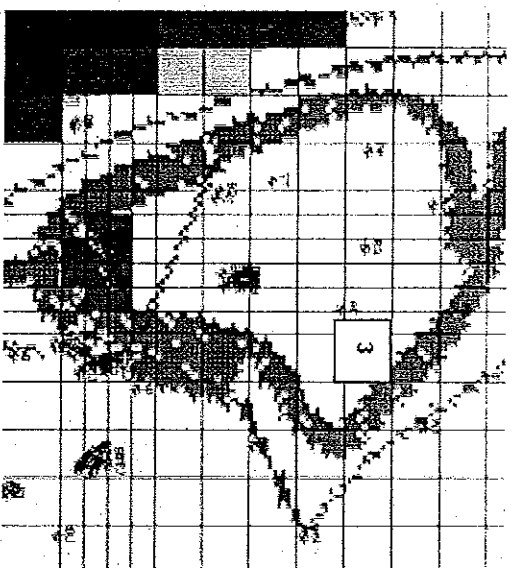


Figure 4-10a Basin Recharge Zone

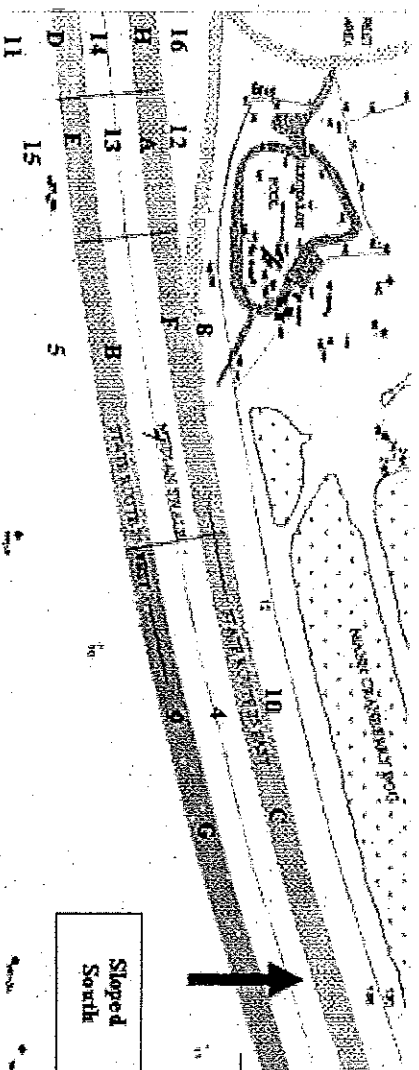


Figure 4-11 Captured Pavement Areas with Model Recharge Zones

4.4 CONTAMINANT MODEL DEVELOPMENT

Particles created by MODPATH were used to simulate deicer particles. This method also only considered advection, and ignored dispersion. Figure 4-12 shows a particle and the resulting streamline that traced the path the particle traveled in groundwater.

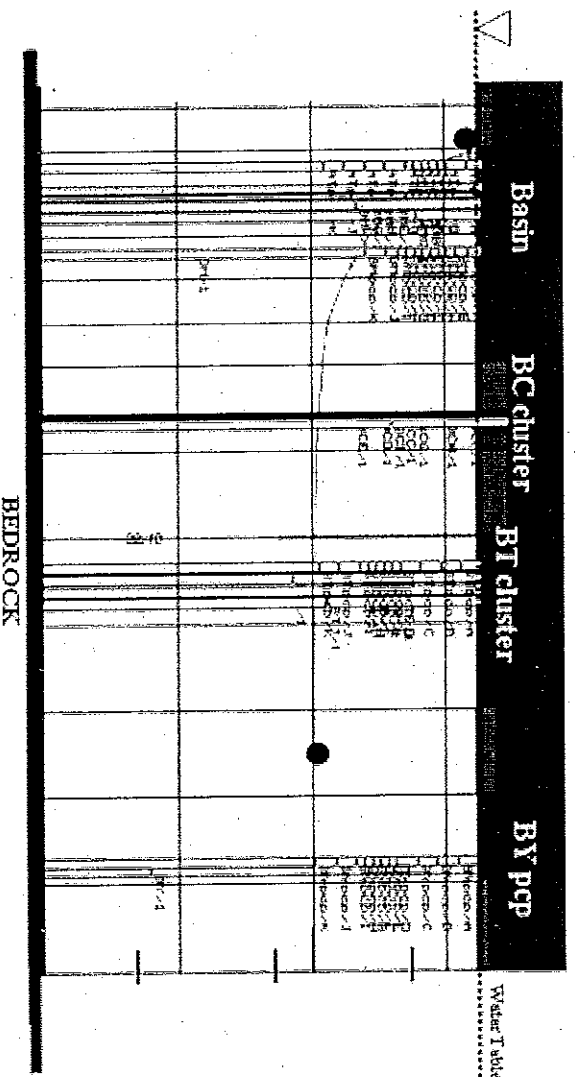


Figure 4-12 Streamline

A circle of particles was placed surrounding the effective infiltration area (Zone 3) and the particles were tracked forward by MODPATH to roughly characterize which wells were within the general path of the deicer plume. To determine the vertical extent of contamination, particles were assigned to the most upgradient edge of the effective infiltration area and released forward in time to simulate the vertical limiting streamline.

Particles were assigned to the midpoint of each observation well and tracked backward to determine which wells receive water from within the model domain. The origin locations of particles that entered the groundwater within the model domain were noted with their respective travel times.

5 RESULTS AND DISCUSSION

5.1 HYDRAULIC MODEL CALIBRATION

5.1.1 Hydraulic Head Boundary Condition Calibration

Boundary conditions along the edges of the model domain were calibrated by comparing the annual averages of observed hydraulic head measurements from August 2003 through July 2004 with heads predicted by the model. Initial head boundaries were chosen based on annually averaged heads observed in wells located at the edges of the model domain (Wells 11, 13C, 16, 18, 20). The predicted hydraulic head data was fit to the observed heads by varying these boundary conditions to minimize the error, in this case the Normalized Root Mean Squared (Norm RMS). Norm RMS was expressed as a percentage, and was defined as:

$$NormRMS = \frac{RMS}{(X_{obs})_{max} - (X_{obs})_{min}} \quad (5-1a)$$

where X_{obs} is the observed hydraulic head, and RMS is:

$$RMS = \sqrt{\frac{1}{\delta} \sum_{i=1}^n R_i^2} \quad (5-1b)$$

where δ was the number of data points, and the residual value R_i for each observation location is the difference between the calculated and observed hydraulic head.

$$R_i = X_{cal} - X_{obs} \quad (5-1c)$$

Figure 5-1 plots the annually averaged observed hydraulic heads versus the heads predicted by the steady-state model. The hydraulic model was considered to be calibrated when the Norm RMS reached a value less than 5%, and the 95% confidence intervals were centered with the data points. Monitoring well ST showed the largest hydraulic head residual of 0.225 m. Otherwise, the calibrated hydraulic model yielded a

Norm RMS of 4.9%, indicating a good agreement between observed and predicted hydraulic head values.

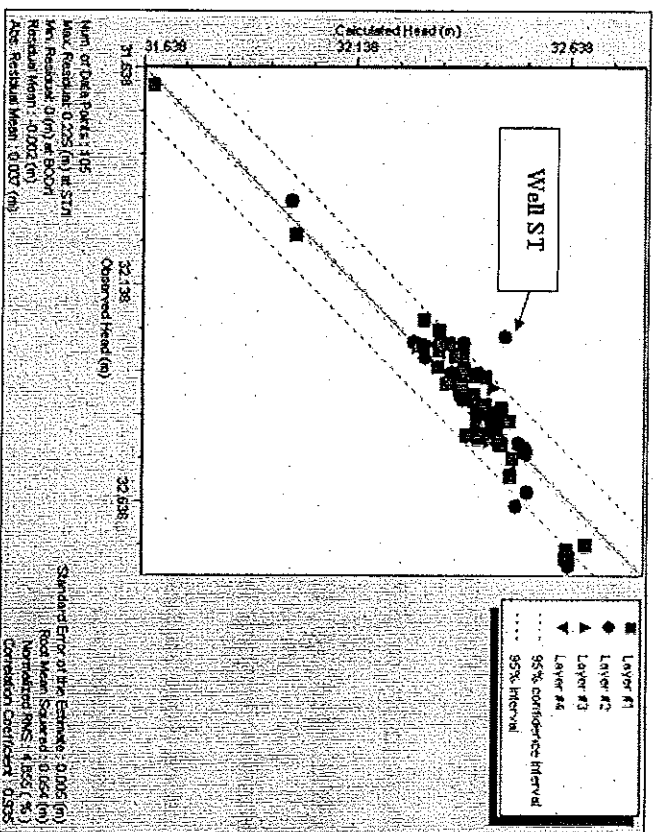


Figure 5-1 Observed vs. Predicted Hydraulic Heads

Figure 5-2 compares the frequency of residuals resulting from the hydraulic head calibration to a normal distribution curve. Fifty-two wells indicated hydraulic head residuals of up to ± 0.02 m, while the normal distribution curve predicted that about half of that number of wells should see residuals up to ± 0.02 m. The largest residual reported was approximately 0.23 m at one well (ST). Given the level of precision that can be achieved for measuring water levels in the field (0.01 m), the residuals reported for the calibration were fairly reasonable.

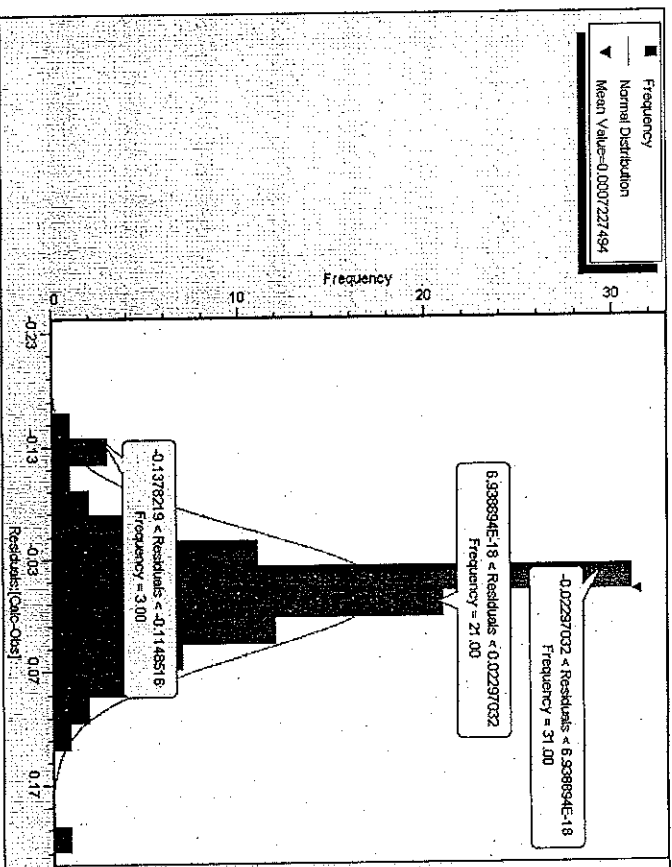


Figure 5-2 Hydraulic Head Calibration Residuals Histogram

Figure 5-3 represents the calibrated hydraulic head boundary conditions at the limits of the model domain.

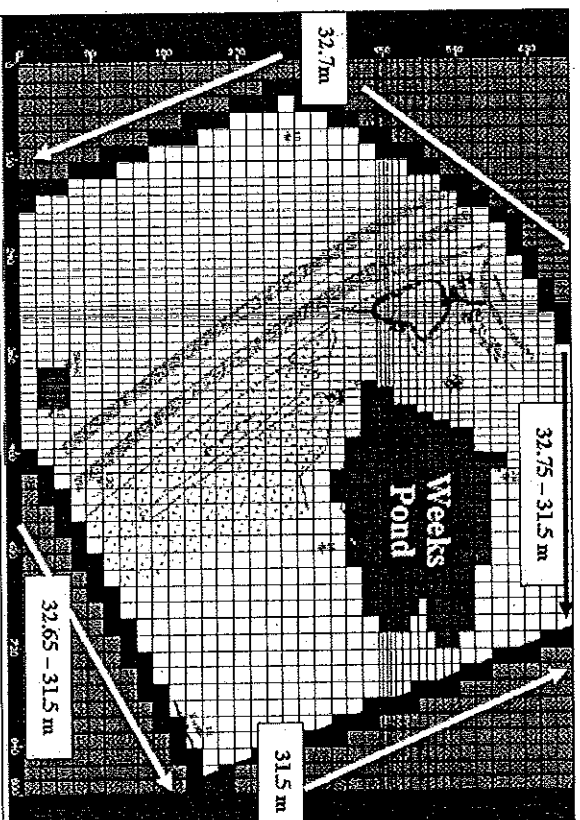


Figure 5-3 Hydraulic Head Boundary Conditions

5.1.2 Infiltration Basin Area and Rate Calibration

The effective area of the infiltration basin, or the puddle area resulting from stormwater discharging to the basin via the West Weir⁵ that eventually infiltrates the groundwater table, constantly changes depending on several factors. These variables include the size of a storm, the volume of stormwater that is captured by the storm drains, and whether the ground is frozen. However, an average effective basin infiltration area was calibrated by comparing the limiting streamline to that demonstrated by past studies.

An effective infiltration basin area A_b of 250 m² was indicated by this calibration method. The area roughly follows the geometry of the basin directly in front of the West Weir. The infiltration area has a maximum width of 20 m north to south, and 15 m east to west. This area includes most of the area before the separation fence. The infiltration basin area is depicted on Figure 5-4.

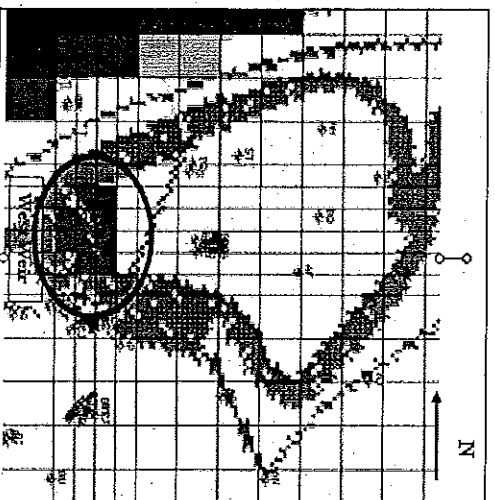


Figure 5-4 Effective Infiltration Basin Area

⁵ Any stormwater discharge delivered by the East Weir to the infiltration basin was considered insignificant.

A_b was used to determine ε_b . The basin infiltration rate and the infiltration area were related as follows:

$$\varepsilon_b = \frac{EA_p P_A}{A_b} \quad (5-2)$$

It was assumed that the water entering the basin via the West Weir was completely infiltrated to the groundwater table. The annual average precipitation falling on the highway pavement discharges to the basin over a significantly smaller area, therefore resulting in a much higher infiltration rate than the ambient recharge rate.

Ostendorf *et al.* (2005a) concluded that the drainage system along the majority of the paved area captured (24,288 m²) was 68% efficient in delivering runoff to the infiltration basin, while the remaining paved area (4,572 m²) was 21% efficient in capturing runoff. This resulted in an ε_b of 1.99×10^{-6} m/s.

5.1.3 Permeability Calibration

To calibrate a single permeability k for the model, a range of values was chosen based on slug test data measured in 2003. A one-parameter Fibonacci search was performed for a range of k values, where the minimum value was the k found at the shallow well (BP) and the maximum value was twice the permeability indicated at the deep well (BO). The results of the Fibonacci search are shown on Figure 5-5. An optimum k of 1.5×10^{-10} m² was found for the steady-state hydraulic model. This result falls roughly in the middle of the range observed with the field slug testing.

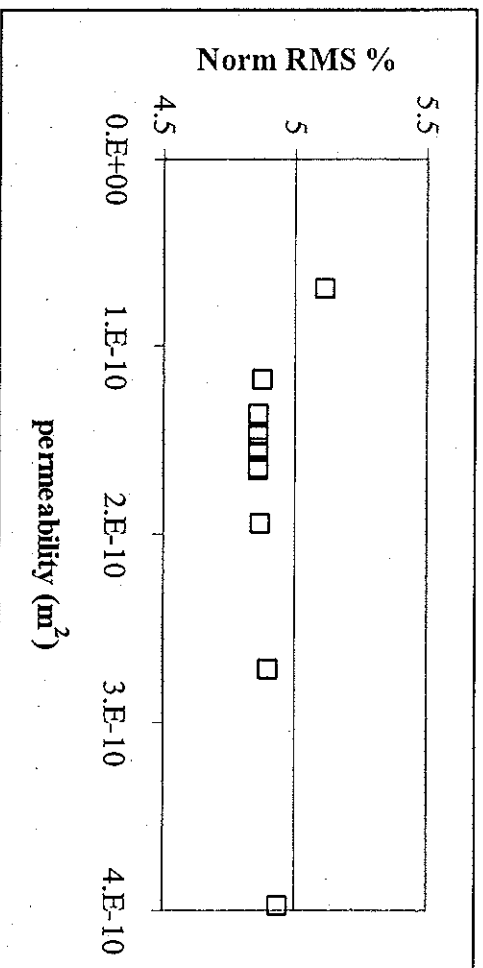


Figure 5-5 Calibration of Permeability

5.1.4 Hydraulic Model Parameters

Table 5-1 lists the final steady-state hydraulic model parameters. ϵ_A on the remaining unpaved areas in the model domain was 1.34×10^{-8} m/s, two orders of magnitude less than the ϵ_B . However, since approximately the same volume of water falling on A_p (approximately $30,000 m^2$) must be infiltrated over an A_B ($250 m^2$) two orders of magnitude smaller, this recharge rate was reasonable.

Table 5-1 Steady-State Hydraulic Model Parameters

Parameter	Value	
Paved Highway Area Discharging to Basin	A_p	28,860 m ²
Effective porosity	n	0.3
Bedrock elevation	z_B	-24.9 m msl
Aquifer thickness	ζ	32 - 37 m
Kinematic viscosity	ν	1.3×10^{-6} m ² /s
Annual average precipitation	P	0.90 m/yr
Ambient steady recharge	ε_A	1.34×10^{-8} m/s
Effective basin area	A_B	250 m ²
Basin recharge	ε_B	1.99×10^{-6} m/s
Flow over basin area	Q	5×10^{-4} m ³ /s
Permeability	k	1.5×10^{-10} m ²
Limiting streamline elevation	z_L	-4.8 m msl

5.2 STREAMLINE ANALYSIS

5.2.1 Forward Particle Tracking

5.2.1.1 Horizontal Extent of Deicer Plume

A circle of particles was assigned around the effective infiltration basin and modeled forward in time to predict how far the deicer will travel in groundwater. Figures 5-6a and 5-6b give a plan view showing the possible paths the deicer could travel.

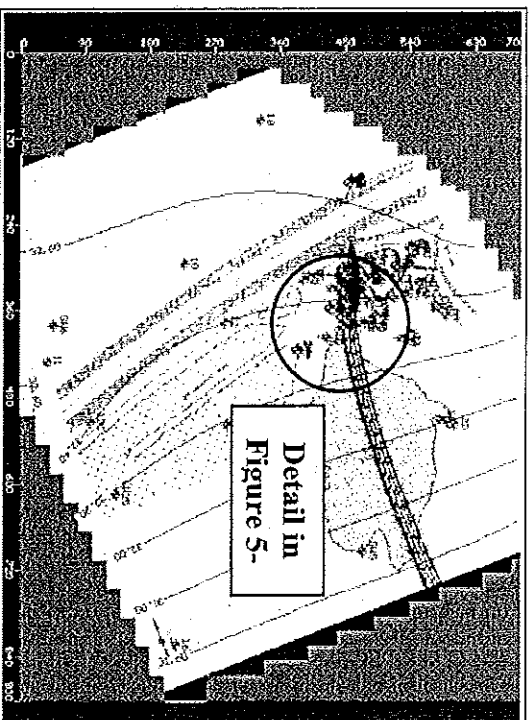


Figure 5-6a Plan View of Streamlines Predicted

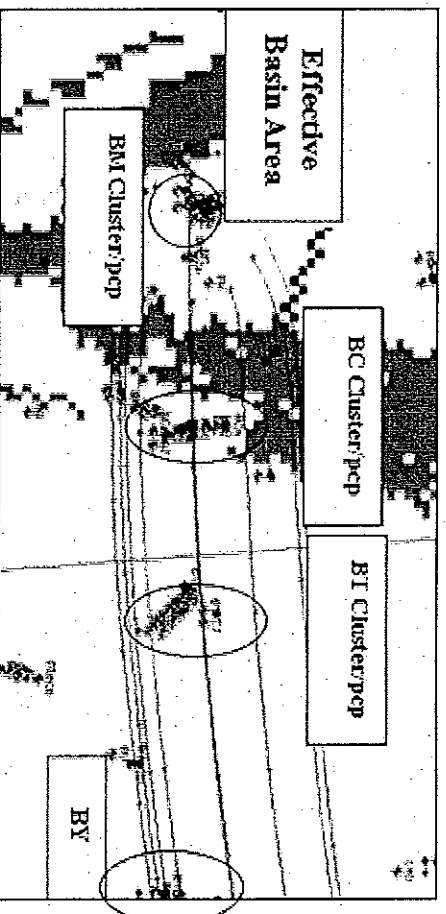


Figure 5-6b Detailed Plan View of Streamlines Predicted

Longitudinally, the deicer traveled to the downgradient limit of the model domain, and its extent could not be determined. Transversely, the model predicted that the deicer plume was approximately 20 m wide (east to west) traveling in a southerly direction, and was defined by the width (east to west) of the effective infiltration basin area. This result was expected, since groundwater generally flows in a southerly direction.

5.2.1.2 Vertical Extent of Deicer Plume

The vertical limit of the deicer contamination plume was determined by modeling the limiting streamline. Particles were assigned to the most upgradient edge of the effective infiltration basin, and modeled forward in time to determine the floor of deicer contamination.

Figure 5-7 illustrates the limiting streamline path along the centerline of the contamination plume.

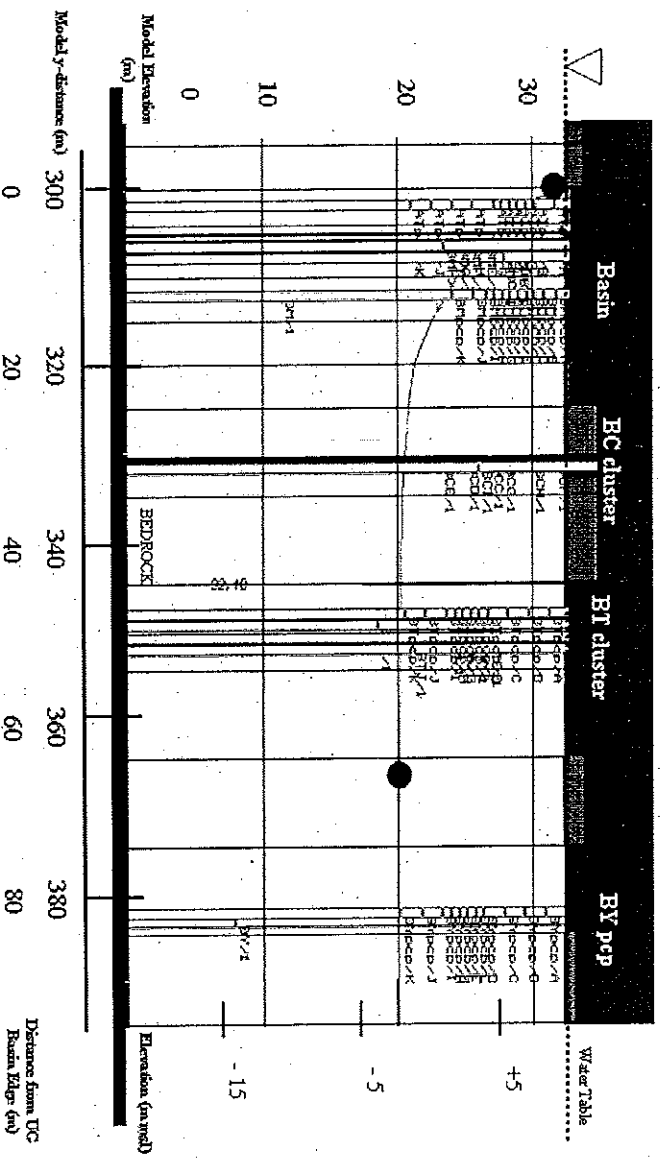


Figure 5-7 Limiting Streamline

Table 5-2 lists the elevations of the limiting streamline at three locations along the centerline of the contaminant plume: well clusters BM, BC, and BT.

Table 5-2		Limiting Streamline Elevation	
Cluster / pcp	Distance from Upgradient Basin Edge (m)	Elevation (m msl)	Depth Below Water Table (m)
BM	6	1.4	6.2
BC	30	-4.3	11.8
BT	49	-4.8	12.3

Well cluster BM is approximately 6 m away from the upgradient edge of the infiltration basin, and is located within the basin area in front of the West Weir. Well cluster BC is located just outside the infiltration basin, approximately 30 m away from the upgradient edge of the basin. Well cluster BT is approximately 49 m away from the upgradient basin edge. The bottom of the plume pushed down as the plume migrates away from the infiltration basin, but it appeared to plateau around the BC cluster. The maximum limiting streamline depth found was approximately 4.8 m below msl. Fauteux (2002) found a maximum limiting streamline depth of 4 m below msl.

5.2.2 Reverse Particle Tracking

Once the hydraulic model was calibrated and the contamination plume was roughly defined, a particle was placed at the midpoint of each observation well screen, and modeled backward. This reverse particle tracking analysis was performed to determine where the water observed in each monitoring well originates at the water table, and the travel time of a typical water molecule. If that water was contaminated with

deicer, the travel time of a water molecule was assumed to approximate the travel time of deicer.

If the particle modeled did reach the groundwater table within the domain, its source location and travel time were recorded. The travel times of particles entering the groundwater table within the model domain are listed in Table 5-3 for sampling well observations, and in Table 5-4 for permanent conductivity point (PCP) observations.

Table 5-3 Sampling Wells Receiving Water from the Infiltration Basin Area

Well	Travel time days	Sampling depth m msl	Well	Travel time days	Sampling depth m msl
AO	50	8.19	BMb	9	3.90
AP	30	8.04	BMc	11	2.96
AT	2	7.34	BMd	10	2.14
BCa	20	5.97	BMe	17	1.47
BCb	20	3.56	BN	10	1.78
BCc	20	1.99	BTa	65	5.40
BCd	40	0.17	BTb	65	4.44
BCE	40	-1.63	BTc	65	3.57
BCf	15	6.81	BTd	65	2.75
BCg	25	2.93	BTe	65	1.75
BCh	17	5.04	BTf	68	0.73
BCi	30	1.09	BTg	70	-0.10
BCj	42	-0.24	BTb	70	-0.96
BD	20	5.60	BTj	90	-3.73
BE	35	-0.52	BTk	50	7.27
BMa	7	4.76	BZ	120	6.67

*Note: Travel times based on a porosity of 0.3.

Table 5-4 Permanent Conductivity Points Locations Receiving Water from the Infiltration Basin Area

Well	Travel time days	Sampling depth m msl	Well	Travel time days	Sampling depth m msl
ATpcp	3	6.83	BTpcp	50	6.51
	5	5.30		50	4.99
	6	4.69		60	3.47
BCpcp	25	7.12		70	1.94
	25	5.60		70	1.33
	30	4.08		70	0.72
	40	2.55		70	0.11
	40	1.03		70	-0.50
	40	0.42		70	-1.11
	40	-0.19		75	-2.63
	50	-0.80		80	-4.15
	50	-1.41	BUpcp	110	6.04
	50	-2.02		110	4.51
BMpcp	1	6.90		110	2.99
	3	5.99		110	1.47
	5	5.38		110	0.86
	6	4.77		110	0.25
	8	4.16		110	-0.36
	9	3.55		110	-0.97
	11	2.94	BYpcp	120	-1.58
	13	2.33		120	5.83
	15	1.72		120	4.31
	18	0.81		120	2.79
	25	-0.72		130	1.26
				130	0.65
				130	0.04
				130	-0.57
				130	-1.18
				140	-1.79
				150	-3.31

*Note: Travel times based on a porosity of 0.3.

The data show that particles originating in the infiltration basin area reached the BM cluster within 1 to 4 days. Particles arrive at the BC cluster within 15 to 50 days, at the BT cluster within 50 to 80 days, and at the BY pcg location within 4 to 5 months.

Table 5-5 provides the travel times of particles that were not hindcasted to enter the water table from the infiltration basin area.

Table 5-5 Observation Locations Receiving Water from Other Source Areas in the Model Domain

Well	Travel time days	Origin Location	Sampling depth m msl
AG	130	south shoulder of EB lane	7.34
AH	90		7.38
AF	120		7.31
AN	210		8.01
AS	80		7.43
AC	190	shoulder area N of ramp for rest area	8.24
AD	150		8.10
AI	200		8.14
Bjpcp	420	by back fence area, b/tw wells BK/BS	5.96
AJ	11	crest of basin, comes down slope	8.04
CB	240		8.63
AQ	330	N of WB lane, near 4 UG wells across rd	8.17
BG	30		7.61
AA	160		8.38
CA	160	rest area	6.14
AB	35		8.03

*Note: Travel times based on a porosity of 0.3.

The date that a specific conductivity or ion concentration was hindcasted to occur in the groundwater was found by subtracting the travel time from the observation date when the well was measured or sampled. Calculations of the "origination date" for each specific conductivity or ion concentration observed are included in Appendix G.

If the particle modeled hit the edge of the model domain before reaching the groundwater table, it was assumed that the particle originated in the subsurface outside of the domain. Water not originating in the domain was demonstrated to hit either the eastern or northeastern domain boundary. This result was expected, since these are the most upgradient locations in the model. Monitoring wells predicted to receive water from a source outside of the model domain are listed in Table 5-6.

Table 5-6 Wells Receiving Water from Outside the Model Domain

Observation	Hit model boundary	Sampling depth m msl	Observation	Hit model boundary	Sampling depth m msl
Well	E BC NE BC		Well	E BC NE BC	
BF	X	-6.49	BTi	X	-6.34
BH	X	-12.96	BU	X	-0.02
BI	X	0.75	BUpcp	X X	-3.11 -4.63
Blpcp	X	4.44	BX	X	-22.99
	X	2.92	BY	X	-16.95
	X	1.39	BYpcp	X	-4.83
	X	0.78	CD	X	5.14
	X	0.17	ST	X	2.64
Blpcp	X	-0.44			
	X	-1.05			
	X	-1.66			
	X	-3.18			
	X	-4.70			

Table 5-6 cont.

Wells Receiving Water from Outside the Model Domain

Observation Well	Hit model boundary E BC NE BC	Sampling depth m msl	Observation Well	Hit model boundary E BC NE BC	Sampling depth m msl
AK	X	7.39	BJ	X	4.33
ANpcep	X	7.90	BK	X	-18.89
		6.38			6.91
		4.85			5.39
		3.33			4.78
		2.72			4.17
		2.11			3.56
		1.50			2.95
		0.89			2.34
		0.28			0.82
		-1.24			-0.71
ATpcep	X	-2.77	BKpcep	X	-2.23
		4.08			-3.76
		3.47			4.44
		2.87			0.40
		2.26			-0.48
		0.73			-1.44
		-0.79			-13.34
		-2.32			4.93
		-3.84			4.02
		-18.73			3.05
AU	X		BOc	X	
AV	X	4.38	BOD	X	2.17
AW	X	-16.87	BOe	X	1.26
AX	X	-0.48	BOf	X	0.31
AY	X	4.49	BOg	X	-0.59
AZ	X	0.44	BOh	X	-1.49
BA	X	6.63	BP	X	1.91
BB	X	-5.59	BQ	X	-13.41
BC	X	-12.59	BR	X	-13.26
BCpcep	X	-3.54	BS	X	-11.58

5.2.3 Observed Specific Conductivity

Average specific conductivity profiles based on observed values recorded between August 2003 through July 2004 were plotted for locations along the supposed centerline of the deicer plume at varying distances from the upgradient basin edge. The specific conductivity for this period of record are in Appendices B and C. Figures 5-8a through c compare the average specific conductivity profiles to the limiting streamline predicted by the model for: the BM well cluster region, the BC cluster region, and the BT cluster region respectively. The wells assigned to each cluster region are listed in Table 5-7.

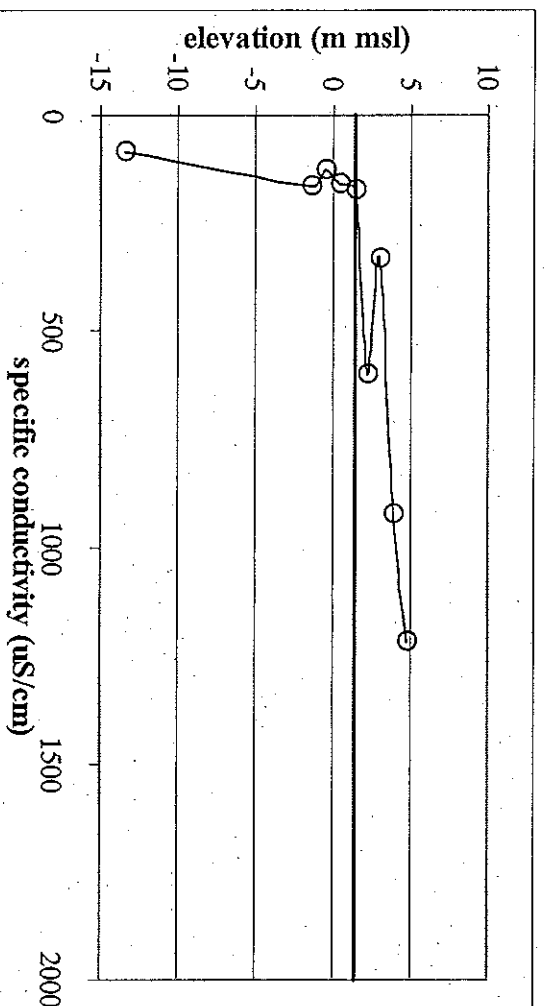


Figure 5-8a BM Cluster Average Observed Specific Conductivity Profile

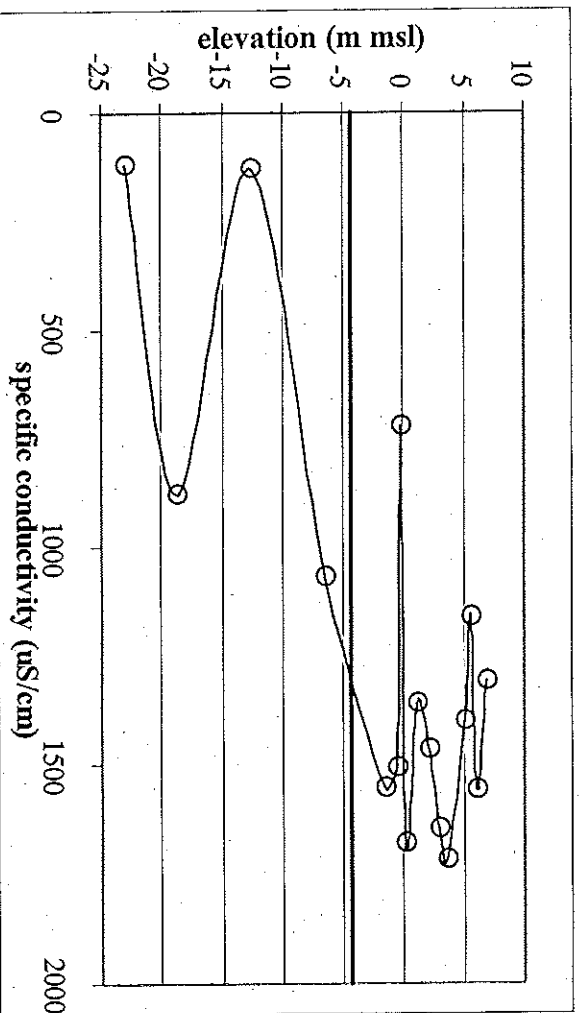


Figure 5-8b BC Cluster Average Observed Specific Conductivity Profile

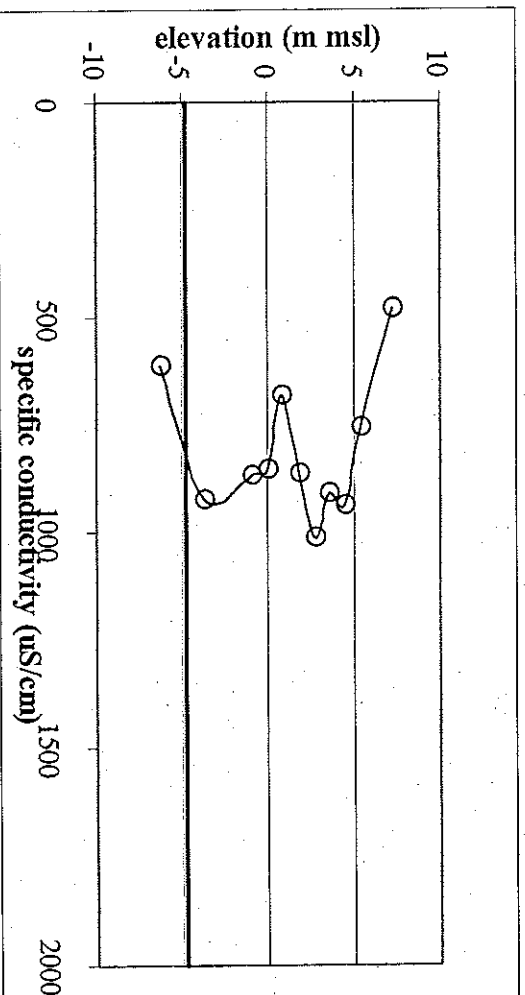


Figure 5-8c BT Cluster Average Observed Specific Conductivity Profile

Table 5-7 Wells Assigned to each Cluster Region

Cluster Region	Wells	Elevation (m msl)	Specific Conductivity (uS/cm)	Cluster Region	Wells	Elevation (m msl)	Specific Conductivity (uS/cm)
BC	BCf	6.8	1309	BT	BTk	7.3	480
	BCa	6.0	1558		BTa	5.4	759
	BD	5.6	1164		BTb	4.4	939
	BCb	5.0	1401		BTc	3.6	911
	BCb	3.6	1719		BTd	2.7	1015
	BCg	2.9	1646		BTe	1.7	864
	BCE	2.0	1467		BTf	0.7	682
	BCi	1.1	1361		BTg	-0.1	854
	BCd	0.2	1681		BTh	-1.0	867
	BCj	-0.2	721		BTj	-3.7	923
	BE	-0.5	1508		BTi	-6.3	613
	BCE	-1.6	1553				
	BF	-6.5	1068				
BM	BC	-12.6	129				
	AU	-18.7	880				
	BX	-23.0	119				
	BMa	4.8	1221				
	BMb	3.9	923				
	BMc	3.0	333				
	BMd	2.1	603				
	BMe	1.5	175				
	BMf	0.4	159				
	BMs	-0.5	127				
	BMh	-1.4	162				
	BM	-13.4	83				

The profile for the BM cluster (Figure 5-8a) shows that the limiting streamline was predicted for an elevation where specific conductivity suddenly declined with depth. In Figure 5-8b, the specific conductivity profile for the BC cluster shows that average specific conductivities were typically about 1,500 $\mu\text{S}/\text{cm}$ down to an elevation of about 2 m below msl. Below this elevation, the specific conductivity appears to change behavior, oscillating with increased depth. The limiting streamline predicted was between these two zones. The profile for the BT cluster in Figure 5-8c does not indicate a noticeable

difference in specific conductivity with depth, typically remaining at about 700 $\mu\text{s}/\text{cm}$, which is a slightly elevated value.

5.3 CONTAMINANT FATE AND TRANSPORT

To evaluate the fate and transport of deicing materials through the Plymouth aquifer, a backward particle tracking analysis was used with wells, where water was determined to originate in the infiltration basin, to hindcast levels of deicer entering the groundwater table in the effective basin area. The hindcasted data presented in this section represents model results, and not observed results.

A nineteen month period between November 2002 and May 2004 was evaluated with the hindcasting analysis. During this time period, deicer was applied on SR25 from November 2002 to April 2003, and again from December 2003 to March 2004. Figure 5-9 shows the observed monthly average specific conductivities in the water that discharged over the West Weir during this time period, along with times when deicer was applied. Weir data recorded for this time period are summarized in Appendix N.

Since several deicing materials (including CMA, rock salt, premix) were used on the highway area at the subject site, specific conductivity was used as a surrogate measurement of all deicing materials in the groundwater. The specific conductivity or ion concentration observed for each particle was assumed to be conserved and assigned to that particle as it traveled through the groundwater.

Calcium and magnesium levels were generally as high as 10 and 50 mg/L during the deicing seasons, and were at ambient levels (below 10 mg/L) by the autumn.

5.3.2 Specific Conductivity Fluxes

Monthly vertical fluxes of specific conductivity were found by the model hindcast data at the infiltration basin. The monthly vertical specific conductivity flux σ_{hind} was determined as follows:

$$\sigma_{hind} = \sum (\beta \times A_{cell} \times \varepsilon_M) \quad (5-3)$$

where β was the average specific conductivity assigned to an area A_{cell} , and ε_M was the monthly recharge rate at that area. For the basin, a basin recharge rate of 1.99×10^{-6} m/s translated to an ε_M of 5.33 m/mo. The effective basin area was split up into a grid with 5 m by 5 m cells, and the specific conductivity values hindcasted to a particular cell for that month were averaged and assigned to that 25 m² area. Calculations of the hindcasted fluxes are in Appendix M. The hindcasted specific conductivity fluxes for November 2002 to May 2004 are shown on Figure 5-10.

The observed monthly specific conductivity vertical flux σ_{obs} in the basin area was determined as:

$$\sigma_{obs} = \sum (\beta \times Q \times \Delta t) \quad (5-4)$$

A summary of observed data recorded at the West Weir are in Appendix N.

The observed vertical specific conductivity fluxes from November 2002 to May 2004 are shown on Figure 5-11.

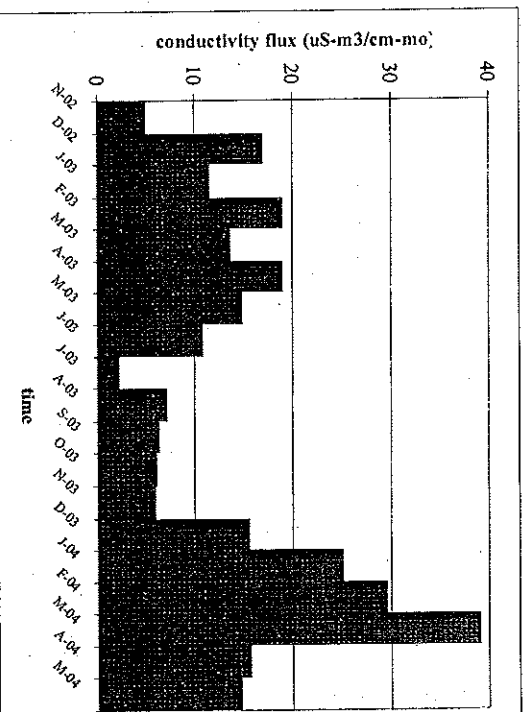


Figure 5-10 Hindcasted Specific Conductivity Flux

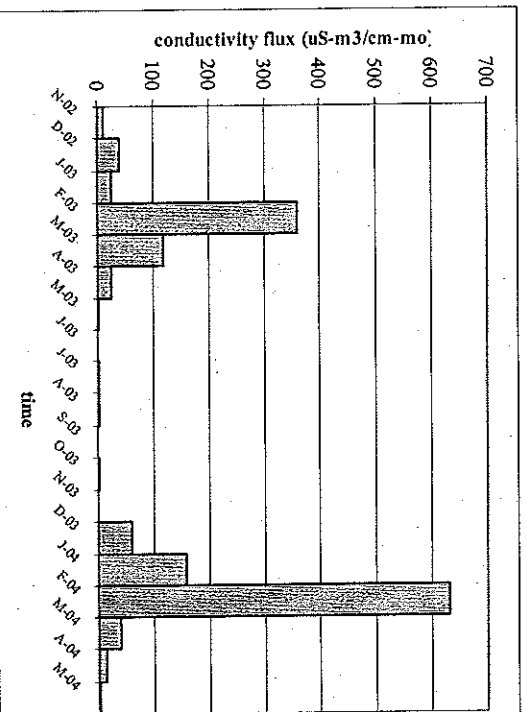


Figure 5-11 Observed Specific Conductivity Flux

The hindcasted and observed specific conductivity fluxes in the basin are compared in Table 5-8. The observed fluxes are higher than those hindcasted for the winter, and lower than those hindcasted for the summer months. The steady-state hydraulics of the model would account for these results. However, the hindcasted results

capture the fact that more deicer was discharged to the basin during the second deicing season than the first.

Table 5-8 Basin Specific Conductivity Fluxes

Month	Specific conductivity flux ($\times 10^5$ uS-m ³ /cm-mo)	
	Observed	Hindcasted
Nov-02	11.8	5.0
Dec-02	39.9	17.0
Jan-03	25.9	11.6
Feb-03	358.7	19.0
Mar-03	119.0	13.7
Apr-03	26.6	19.0
May-03	2.2	14.9
Jun-03	0.1	10.9
Jul-03	1.2	2.2
Aug-03	2.0	7.2
Sep-03	0.0	6.4
Oct-03	1.2	6.1
Nov-03	0.5	6.0
Dec-03	60.9	15.6
Jan-04	158.8	25.1
Feb-04	632.1	29.6
Mar-04	40.8	39.2
Apr-04	13.9	15.7
May-04	3.3	14.8

The monthly average monthly specific conductivity β_{mo} was determined by dividing the flux by the volume of water V infiltrating the groundwater:

$$\beta_{mo} = \frac{\Sigma(\beta \times Q \times \Delta t)}{V} \quad (5-5)$$

The observed and hindcasted average specific conductivities in the basin are listed in Table 5-9, and shown on Figure 5-12. The values compared relatively well for the winter of 2002 up through the end of 2003. However, in January and March 2004, the

model hindcast significantly underestimated the average specific conductivity, and underestimated in the following spring months.

Table 5-9 Average Basin Specific Conductivity

Month	Average specific conductivity (uS/cm)	
	Observed	Hindcasted
Nov-02	546.2	387.3
Dec-02	1744.7	1272.2
Jan-03	3556.9	868.3
Feb-03	909.8	1578.2
Mar-03	582.8	1024.8
Apr-03	1974.8	1470.6
May-03	1278.5	1117.0
Jun-03	239.2	844.4
Jul-03	543.1	165.6
Aug-03	297.1	543.5
Sep-03	--	494.2
Oct-03	106.4	459.5
Nov-03	101.6	461.5
Dec-03	3336.4	1169.1
Jan-04	43618.5	1885.6
Feb-04	2917.8	2372.6
Mar-04	8280.3	2941.8
Apr-04	864.6	1218.1
May-04	576.9	1106.9

*Note: No flow was observed over the West Weir in September 2003.

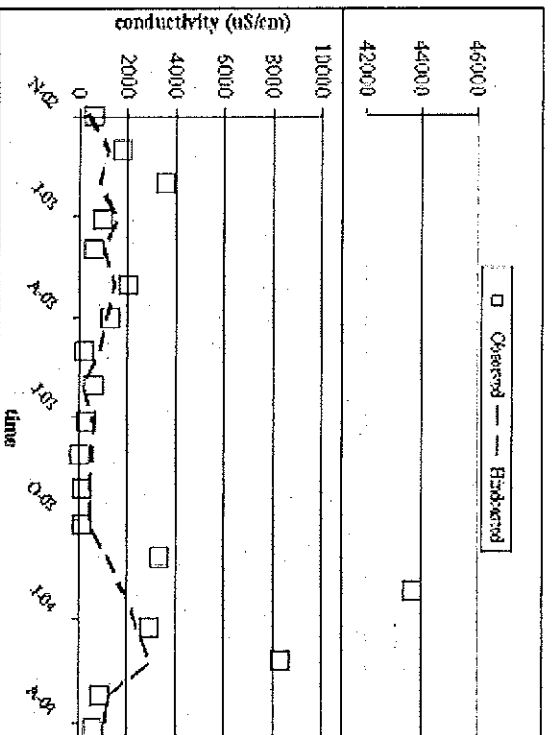


Figure 5-12 Average Basin Specific Conductivity

5.3.3 Ion Mass Fluxes

Monthly mass fluxes of each conservative deicer ion (σ_{ion}) were found for a full year after deicing began in November 2002, up until a new deicing season began in December 2003. The ion mass fluxes were determined by the model hindcast data at the infiltration basin in the same manner as the specific conductivity fluxes. Substituting concentration for specific conductivity in equation 5-3 yields the following relationship:

$$\sigma_{ion} = \sum (C \times A_{cell} \times \epsilon_M) \quad (5-6)$$

Figures 5-13a through d illustrate the mass fluxes hindcasted for Cl^- , Na^+ , Ca^{2+} , and Mg^{2+} over the course of a year after deicing was initiated. Figures 5-13a and b indicate that the mass fluxes Na^+ and Cl^- followed similar trends throughout the course of the year, rising during deicing and peaking in the spring, and that the fluxes were on the same order of magnitude. Figures 5-13c and d show that mass fluxes of Mg^{2+} and Ca^{2+} follow similar trends, reaching low points in the summer. However, the Ca^{2+} flux

appeared to remain more constant over the winter and spring than the Mg^{2+} flux, which peaks more significantly in the spring. The values are listed in Table 5-10.

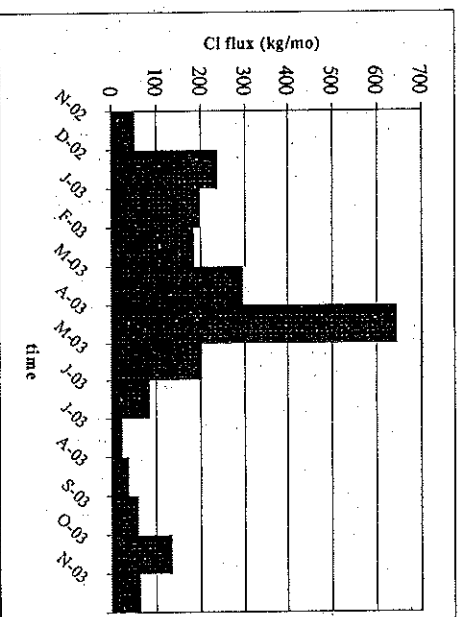


Figure 5-13a Chloride Mass Flux

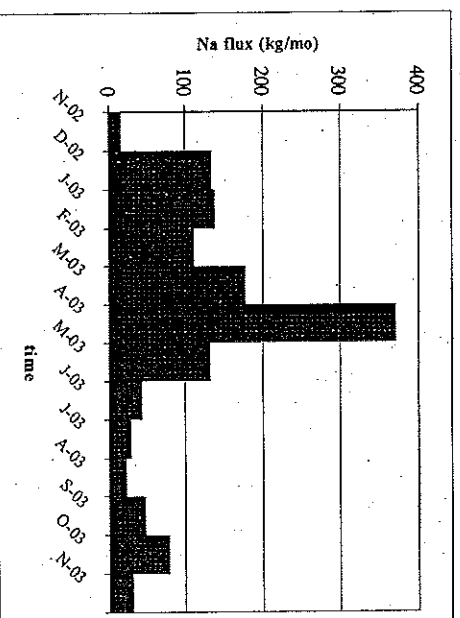


Figure 5-13b Sodium Mass Flux

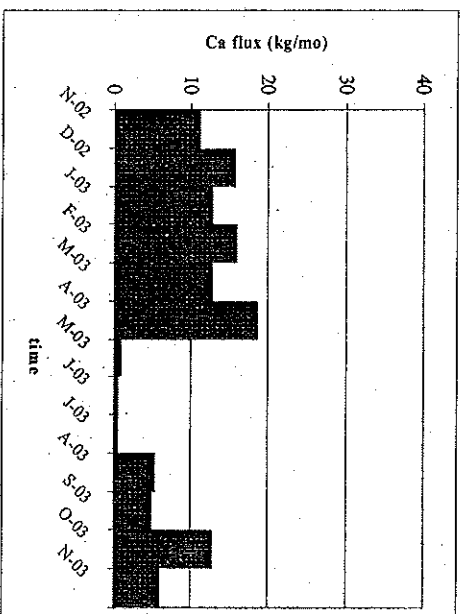


Figure 5-13c Calcium Mass Flux

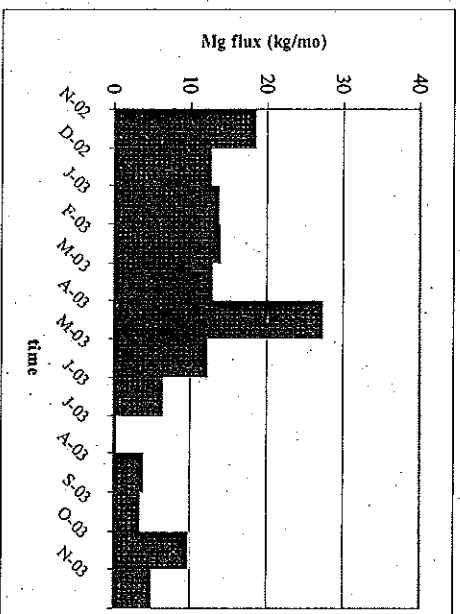


Figure 5-13d Magnesium Mass Flux

Table 5-10 Ion Mass Fluxes

Month	(kg/mo)			
	Cl ⁻	Na ⁺	Ca ²⁺	Mg ²⁺
Nov-02	55.2	17.1	11.2	18.6
Dec-02	238.7	134.2	15.8	12.7
Jan-03	202.3	137.2	12.8	13.7
Feb-03	187.5	111.7	16.0	14.0
Mar-03	299.6	177.1	12.8	12.8
Apr-03	646.4	371.3	18.6	27.3
May-03	205.0	131.0	1.0	12.3
Jun-03	86.7	43.0	0.7	6.4
Jul-03	26.5	29.1	0.7	0.5
Aug-03	40.7	22.2	5.3	3.9
Sep-03	62.1	47.3	5.0	3.6
Oct-03	134.9	77.7	12.8	9.7
Nov-03	64.0	31.0	6.0	5.0

The ratios of σ_{ion} to the specific conductivity flux, or the ion flux ratios (Δ , in units of kg-cm/mS-m³) were determined for each conservative ion, and are listed in Table 5-11.

Table 5-11 Ion Flux Ratios

Month	(kg-cm/mS-m ³)			
	Cl ⁻	Na ⁺	Ca ²⁺	Mg ²⁺
Nov-02	0.111	0.034	0.022	0.037
Dec-02	0.141	0.079	0.009	0.007
Jan-03	0.175	0.119	0.011	0.012
Feb-03	0.099	0.059	0.008	0.007
Mar-03	0.219	0.130	0.009	0.009
Apr-03	0.341	0.196	0.010	0.014
May-03	0.138	0.088	0.001	0.008
Jun-03	0.080	0.039	0.001	0.006
Jul-03	0.120	0.132	0.003	0.002
Aug-03	0.056	0.031	0.007	0.005
Sep-03	0.097	0.074	0.008	0.006
Oct-03	0.220	0.127	0.021	0.016
Nov-03	0.108	0.052	0.010	0.008
average	0.146	0.089	0.009	0.011

Figure 5-14 plots the monthly flux ratios hindcasted for Cl^- . There was a decreasing trend in the Cl^- flux ratio over the course of the year studied, which was suggestive of how quickly Cl^- dissolves and mobilizes compared to the other deicer ions.

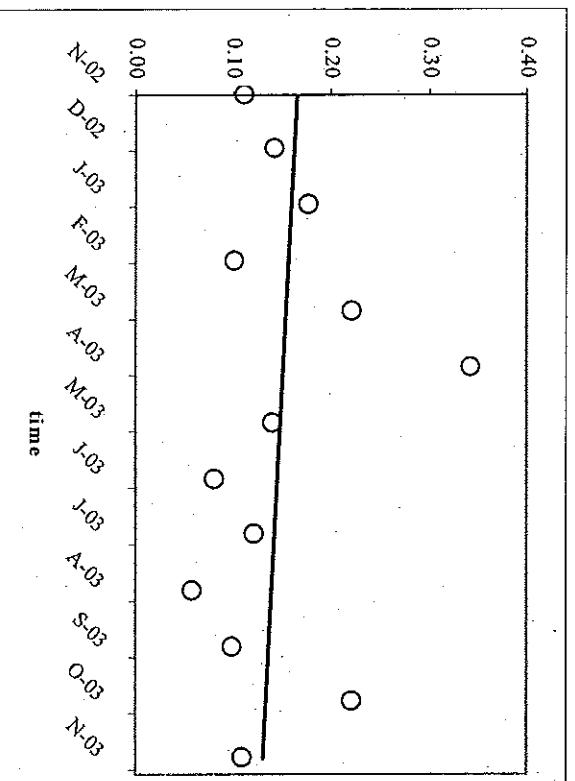


Figure 5-14 Chloride Flux Ratios

Stygar (2005) also noted a decreasing trend over the course of a year in the chloride flux ratios found in water discharging over the West Weir at the site.

The ambient ion concentrations listed in Table 2-3 were subtracted from the concentrations to hindcast the mass fluxes resulting strictly from deicer. These results were compared to the quantities of CMA, NaCl , and premix applied in the 2002 – 2003 deicer season. A record of deicers applied to SR25 is in Appendix O. The amount of NaCl , CaCl_2 , and premix reported was applied to 147 lane miles of SR25, of which only 11 lane miles were within the paved area discharging to the infiltration basin (see Section

4.3.3). The amount of CMA reported applied exclusively to the 11 lane miles that discharge to the basin. Therefore, the masses were adjusted to reflect only what was applied to the 11 lane miles of pavement.

The mass of deicer hindcasted as recovered in the groundwater (m_r) was found as:

$$m_r = \sum_{t_a}^{t_b} \sigma_{ion} \quad (5-7)$$

where t_a is the time when deicer is first applied, and t_b is the time just before a new deicing season begins. According to this analysis, approximately 1% of the total deicer mass that was applied was recovered in the groundwater hindcasted to the infiltration basin.

The applied ion mass ratios (λ_{app}) were found as:

$$\lambda_{app} = \frac{m_{ion,app}}{m_{d,app}} \quad (5-8)$$

Acetate was not studied here because it is not a conserved ion, but it is a key constituent in CMA. To account for this, the applied mass ratio was found by dividing the ion mass that was applied ($m_{ion, app}$) by the total deicer mass applied ($m_{d,app}$), which included acetate.

The hindcasted ion mass ratio (λ_{hind}) was similarly found, with the total deicer mass accounting for the acetate.

$$\lambda_{hind} = \left(\frac{\sigma_{ion}}{\sum \sigma_{ion}} \right) \times \left(\frac{\sum m_{ion,app}}{m_{d,app}} \right) \quad (5-9)$$

The deicer ion mass ratios that were hindcasted are listed in Table 5-12, and compared well with the ratios of deicer actually applied.

Table 5-12 Deicer Ion Mass Ratios

Ion	λ_{app}	λ_{hind}
Ca^{2+}	0.026	0.024
Na^{+}	0.299	0.280
Cl^{-}	0.469	0.486
Mg^{2+}	0.026	0.030

6 CONCLUSIONS

6.1 SUMMARY OF WORK COMPLETED

The main goal of this research was to evaluate when and where deicer contamination infiltrated to the groundwater table at the site, with a focus on the infiltration basin. The approach used assumed that the deicing contaminant was conservative, so that only Cl^- , Na^+ , Ca^{2+} , and Mg^{2+} ions were studied. Additionally, specific conductivity was used as a surrogate measurement of the deicer materials used at the site.

Groundwater samples were collected monthly by a traditional full purge sampling method from November 2002 to September 2004, from ninety-one wells located in and around the infiltration basin. Surface water samples were also collected from the exit weirs in the basin. Specific conductance was measured while extracting the water samples into sample bottles for laboratory analysis. Laboratory analysis included tests for dissolved cations and anions like Cl^- , Na^+ , Ca^{2+} , and Mg^{2+} .

Electrical conductivity measurements were taken on a frequent basis (often biweekly) from nine PCP locations in the basin area. PCP data from November 2002 to December 2004 was used in this project. Rainfall and discharge through one of the exit weirs (West Weir) in the infiltration basin was monitored continuously by field instrumentation. Rainfall data from August 2003 to July 2004 was used to characterize precipitation for the model, and weir discharge data from November 2002 to May 2004 was used to characterize the quality and volume of water draining into the basin from the highway.

A steady-state three-dimensional numerical model was developed. Calibration of the hydraulic model depended on time averaged monthly hydraulic head measurements collected in monitoring wells located throughout the basin area and near the downgradient cranberry bog (Mann Bog), from August 2003 to July 2004. A constant permeability value was calibrated with the model.

Once the hydraulic model was calibrated, streamlines were used to assess the hydraulics of the Plymouth aquifer. Streamlines were predicted forward in time to determine limits of the deicer contamination plume. The limits of the deicer plume supposed by these streamline analyses were compared to average observed specific conductivities from August 2003 through July 2004.

Modeling of streamlines backward in time "hindcasts" the travel times and previous locations of the contaminant. A hindcasting analysis was performed with the model to trace observed deicer particles back to the groundwater table. Travel times and source locations of the deicer particles were determined from the analysis.

The hindcasting analysis yielded travel times and locations where deicer initially entered the groundwater table. These data were the basis for creating isopleths of specific conductivity and conservative deicer constituents for the infiltration basin over the course of two deicing seasons and one non-deicing season, from November 2002 to May 2004. Vertical specific conductivity fluxes were hindcasted at the basin, and compared to the specific conductivity fluxes observed as discharging over the West Weir. Finally, ion mass fluxes were determined for the basin, as well as ion flux ratios that compared each ion mass flux to the specific conductivity flux. The ion fluxes were also

used to hindcast mass ratios of each conservative deicer constituent and compared to the ratio of deicer constituents applied on the highway.

6.2 CONCLUSIONS

6.2.1 Site Hydraulics

Once the hydraulic model was calibrated with time averaged hydraulic head measurements, it was first used to recover a constant permeability for the aquifer. A permeability of $1.5 \times 10^{-10} \text{ m}^2$ was found, a value which fell within the range indicated by slug test data collected at the site in 2003.

The effective basin area, where water discharging over the West Weir infiltrated into the water table, was calibrated to 250 m^2 . A basin recharge rate of $1.99 \times 10^{-6} \text{ m/s}$ water thus determined, which was two orders of magnitude larger than the ambient recharge rate of $1.34 \times 10^{-8} \text{ m/s}$. Since the paved area serviced by the drainage system was two orders of magnitude larger than the effective basin area, this result was reasonable.

6.2.2 Streamline Analyses

The deicer contamination area emanating from the basin has been established by previous studies, and the transverse and vertical limiting streamlines were also predicted by this model. The plume was determined to be approximately 20 m wide in the east-west direction, and as deep as 12 m below the water table. This result agreed well with a past study that used a two-dimensional analytical model (Fautoux, 2002).

Streamlines were also hindcasted from observation wells back to the water table to establish which wells were receiving water from the infiltration basin. The travel

times of deicer particles coming from the basin ranged from 1 day to about 1 month to reach the BM cluster (located inside the basin), and were about 4 or 5 months to reach the BY pcg location approximately 80 m away from the basin. Again, these results compared well with the results from the analytical model. Finally, the limiting streamline depth at well clusters located along the centerline of the plume was compared to observed specific conductivity profiles. The maximum limiting streamline depth z_L was 4.8 m below msl.

6.2.3 Contaminant Transport

As expected, hindcasted source isopleths of specific conductivity and ion concentrations confirmed that the infiltration basin was the largest source of deicer contamination at the site, with deicer infiltration peaking in the winter and in the spring. Specific conductivity values hindcasted were as high as 10,000 $\mu\text{S}/\text{cm}$ in the winter and as high as 5,000 $\mu\text{S}/\text{cm}$ in the spring. Chloride concentrations hindcasted were as high as 2,500 mg/L in the winter and as low as 10 mg/L in the summer and fall. Sodium concentrations hindcasted were as high as 1,500 mg/L in the winter and as low as 10 mg/L in the summer and fall. Calcium and magnesium concentrations hindcasted were as high as 50 mg/L in the winter and spring and below 10 mg/L in the summer and fall. A comparison of the monthly specific conductivity fluxes hindcasted with the model for a nineteen month period (which included the deicing seasons of 2002 – 2003 and 2003 – 2004) to the fluxes observed over the West Weir indicated that only general flux trends could be indicated by the hindcasts. The steady-state hydraulics of the model underestimated the flux of specific conductivity expected during the winter and spring.

Hindcasted average monthly specific conductivities of the groundwater in the basin for the first deicer season compared well to the specific conductivity observed over the West Weir, while the second deicing season was underestimated by the hindcasts. However, these results may be attributed to the fact that the basin area was more deeply frozen over the course of the winter of 2003 – 2004 than the previous winter, and a majority of basin wells could not be sampled until the spring. The frozen ground may not have allowed the discharge over the weir to fully infiltrate the water table.

The ion flux ratios found over the course of a year for Cl^- suggested a decreasing trend, which was also found for the water discharging over the weir by a previous study (Styggar, 2005). This result indicates the high mobility and solubility of Cl^- in comparison to the other deicer constituents. Finally, the hindcasted mass ratios for each deicer ion compared favorably to the composition of the deicers applied to the section of SR25 discharging to the basin.

It may be concluded that this particle hindcasting scheme may be used as a tool to determine relative orders of magnitude of deicer contaminant, but further investigation is needed to validate its use to find specific concentrations. One reason for this result may be the fact that larger storms pushed the contamination deeper into the aquifer than the steady-state hydraulics allowed in the model, and since dispersion was ignored in the particle analysis, this contamination was not picked up by the model.

6.3 RECOMMENDATIONS

The knowledge of the hydraulics of the site aquifer gained from previous studies was used as the basis for the study of deicer contaminant transport at the site. Further

study into the hydraulics of the site and the nature of the deicer contaminants should be performed to expand on the conclusions of this project.

The calibration of the hydraulic model depended on hydraulic head data time averaged over a twelve month period. Calibrating the model with head data averaged over a period of several years, further refining the layering of the model domain, and validating the model with an independent head data set might provide more faith in the calibration. It would also prove worthwhile to study several more deicing seasons, and compare infiltration results for milder winters to colder winters.

While the specific conductivity database includes biweekly measurements, only monthly analysis of the ions in the groundwater is performed. More frequent groundwater sampling would provide a better dataset that could be modeled and compared to the specific conductivity. Finally, further study is suggested of pervious areas (e.g., shoulders, medians) where deicer may be immobilized to gain a better understanding of where else deicer persists after leaving the highway pavement.

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APPENDIX A
August 2003 – July 2004 Precipitation Data

1 in=25.4 mm

Cranberry Station Data

Date	Total Adj Precip	
	in	m
31-Aug-03	2.82	0.071628
30-Sep-03	2.37	0.060198
31-Oct-03	5.23	0.132842
30-Nov-03	2.94	0.074676
31-Dec-03	5.99	0.152146
31-Jan-04	1.80	0.04572
29-Feb-04	2.41	0.061214
31-Mar-04	2.21	0.056134
30-Apr-04	5.54	0.140716
31-May-04	2.80	0.07112
30-Jun-04	1.65	0.04191
31-Jul-04	2.73	0.069342
Aug 03-Jul 04 Total	38.49	0.98
	977.646	mm/yr
	0.977646	m/yr
	3.1001E-08	m/s

Notes:

Cran Station reports rain as rain+melted snow--it is adjusted precip

Basin Rain Gauge Data

Date	Last Time Rec of Mo	Acc Precip in	Supp Cran data Rain	Adj Precip	
				in	m
Aug-03	9/1/2003 0:00	2.57		2.57	0.065278
Sep-03	10/1/2003 0:00	1.93		1.93	0.049022
Oct-03	10/30/2003 23:00	4.79	0.00	4.79	0.121666
Nov-03	12/1/2003 0:00	2.17		2.17	0.055118
Dec-03	1/1/2004 0:00	5.89		5.89	0.149606
Jan-04	2/1/2004 0:00	1.63		1.63	0.041402
Feb-04	3/1/2004 0:00	2.59		2.59	0.065786
Mar-04	4/1/2004 0:00	2.46		2.46	0.062484
Apr-04	5/1/2004 0:00	4.95		4.95	0.12573
May-04	6/1/2004 0:00	2.26		2.26	0.057404
Jun-04	7/1/2004 0:00	1.34	0.47	1.81	0.045974
Jul-04	8/1/2004 0:00	2.26		2.26	0.057404
Aug 03-Jul 04 Total				35.31	0.897
				896.874	mm/yr
				0.896874	m/yr
				2.84397E-08	m/s

Notes:

Supplement missing gage data with Cran Station data

Data missing 10/30/04 23:00 to 11/1---but no rain for this time period recorded by Cran

Data missing 6/2/04 17:20 to 6/6/04 12:00-supp with Cran Station

	TEMPERATURE F.	PRECIPITATION	WEATHER (Calendar Day)	RIVER STAGE
--	----------------	---------------	------------------------	-------------

CONDITION OF RIVER AT GAGE				SUPERVISING OFFICE		STATION INDEX NO.	
A. Obstructed by rough ice.	E. Ice gorge below gage			WFO, TAUNTON		19-2451-3	
B. Frozen, but open at gage.	F. Shore ice.						
C. Upper surface of smooth ice.	G. Flooding ice.						
D. Ice gorge above gage.	H. Pool stage.						

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Dept.	Phone #	
Fax # <u>545-2202</u>	Fax #	

TOTAL P.01

P.02/02

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STATION (Climatological)				MONTH		WS FORM B-91			
EAST WAREHAM (River Station, if different)				JAN 2004		(12-93)			
STATE		COUNTY		RIVER		RECORD			
MA		Plymouth							
TIME (Local) OF OBSERVATION		TEMP		PRECIPITATION		STANDARD TIME IN USE			
Midnight		MDNT		9 AM					
TYPE OF RIVER GAGE		ELEVATION OF RIVER GAGE ZERO		FLOOD STAGE		NORMAL POOL STAGE			
		Fl.		Fl.		Fl.			
TEMPERATURE F.			PRECIPITATION			WEATHER (Calendar Day)			
24 HRS. ENDING AT OBSERVATION			24-HR AMOUNTS			Mark 'X' for all types occurring each day.			
AT OBSN			At Co			Mark 'X' for all types occurring each day.			
MAX. MIN.			Rain, melted snow, etc. (in. and hundredths)			Fog			
			Snow, ice pellets, hail, ice on ground (in.)			Ice pellets			
						Glaze			
						Thunder			
						Hail			
						Damaging Wind			
						Time of observation if different from 0100			
						CONDITION			
						READING AT			
						TENDENCY			
						REMARKS (Special observations, etc.)			
1	45	29	29	0	0	0			SUNNY
2	38	25	37	.06	.50	.50			AMSNOW OVERCAST
3	46	36	44	.03	.25	0			Overcast Rain off + ON
4	50	37	37	0	0	0			Overcast Rain
5	38	36	37	.95	0	0			Overcast, Lt Rain
6	37	22	22	0.13	T	0			Mostly Clear + Sunny snowburst PM
7	24	18	19	0	0	0			Mostly Clear + Cold
8	23	13	13	0	0	0			Mostly Clear + Cold
9	13	3	3	0	0	0			Clear with cold
10	14	-0.4	5	0	0	0			Mostly Clear
11	27	2	27	0	0	0			Partly Cloudy
12	33	24	24	0.06	1.70	1.70			Overcast, flurries
13	42	12	12	1	.05	.30			Overcast
14	11	-0.4	6	0	0	.07			Mostly Clear
15	9	-4	-4	1.05	1.56	1.96			Overcast, Lt Snow
16	14	-6	12	0	0	1.16			Mostly Clear, Sunny, windy
17	39	13	27	0	0	0.5			Sunny, Clear
18	36	28	28	.03	.02	0.52			Clear, Breezy, Sunny
19	28	17	17	0.42	1.18	1.70			Sunny, Clear
20	25	13	17	0	0	1.6			Mostly Clear
21	31	9	9	0	0	0.4			Mostly Clear
22	37	7	23	0	0	0.55			Cloudy, overcast, Lt Snow PM
23	22	11	11	0	0	0.54			Mostly Clear
24	19	7	7	0	0	0.54			Clear, Sunny
25	17	1	9	0	0	0.54			Clear, Sunny
26	18	8	18	0	0	0.53			Mostly Clear
27	27	18	25	0	0	0.50			Cloudy
28	27	21	26	0.01	.70	1.20			Overcast Snow
29	28	18	18	0.04	2.13	2.83			Mostly Clear increasing clouds - Windy
30	26	14	18	0	0	1.80			Mostly Clear
31	28	17	18	0	0	1.83			Mostly Clear
32	28	14.2	SLM	1.80	8.09				
CONDITION OF RIVER AT GAGE			CHECK BAR (For true weight) NORMAL CK. BAR			Fog			
A. Obstructed by rough ice.			READING			Ice Pellets			
B. Frozen, but open at gage.			DATE			Glaze			
C. Upper surface of smooth ice.						Thunder			
D. Ice gorge above gage.						Hail			
E. Ice gorge below gage.						Damaging Wind			
F. Shove ice.						Time of observation if different from 0100			
G. Floating ice.						CONDITION			
H. Pool stage.						READING AT			
						TENDENCY			
						REMARKS (Special observations, etc.)			
						SUPERVISING OFFICE			
						STATION INDEX NO.			

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WFO, TAUNTON

19-2451-3

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STATION (Climatological)		(River Station, if different)		MONTH		WS FORM B-91 (12-93)		U.S. DEPARTMENT OF COMMERCE NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION NATIONAL WEATHER SERVICE											
EAST WAREHAM		Plymouth		March 2004		RECORD OF RIVER AND CLIMATOLOGICAL OBSERVATIONS													
STATE MA		COUNTY		RIVER															
TIME (local) OF OBSERVATION RIVER		TEMP.		PRECIPITATION		STANDARD TIME IN USE													
midnight		MDMT		9AM															
TYPE OF RIVER GAGE		ELEVATION OF RIVER GAGE ZERO		FLOOD STAGE		NORMAL POOL STAGE													
		FL		FL															
DATE	TEMPERATURE F			PRECIPITATION			WEATHER (Calendar Day)										RIVER STAGE		REMARKS (Special observations, etc.)
	24 HRB. ENDING AT OBSERVATION		AT OBSN.	24-HR AMOUNTS			Start "X" for all types occurring each day.										GAGE READING AT A.M.	TENDENCY	
	MAX.	MIN.		24-HR AMOUNTS															
				24-HR AMOUNTS	AI Os.	AI Os.	A.M.	NOON	P.M.										
1	55	28	37	0	0	0													Partly cloudy
2	50	36	48	0	0	0													Cloudy, overcast, rain, Pale pm
3	55	34	34	7	0	0													Clear
4	48	32	34	.03	0	0													Overcast, lt rain
5	46	32	39	7	0	0													Overcast, pm shower
6	55	39	39	.40	0	0													Cloudy, rain
7	48	33	35	.04	0	0													Sunny
8	36	28	28	1.0	0	1.5													Overcast, snow
9	36	24	24	.10	1.50	1.13													mostly cloudy
10	38	22	34	1.0	0	0.43													mostly cloudy
11	40	27	27	.20	0.43	0.86													Snow, sleet, windy
12	48	26	32	0	0	0													Partly cloudy, Pass. w/lt rain
13	43	28	29	.05	0	0													rain snow showers
14	38	21	38	1.0	0	0													mostly sunny
15	55	36	36	1.0	0	0													Am sun - Thim overcast, Pm
16	38	26	30	0	0	0													Am sunny -
17	32	28	30	0.46	6.00	0.13													mostly cloudy, heavy snow
18	33	23	26	0	1.50	3.6													Cloudy, overcast, snow showers
19	32	23	23	0.04	7	3.6													mostly cloudy, passive snow showers, lt snow
20	41	15	37	0	1.75														Snow, overcast
21	50	31	31	0.58	0	0													Cloudy rain pm
22	34	22	23	0	0	0													Slow clearing + windy
23	38	15	36	0	0	0													Mostly clear
24	51	29	39	0	0	0													Clear
25	51	39	45	0	0	0													Clear
26	56	43	43	0.03	0	0													Overcast, lt rain
27	55	42	43	0.10	0	0													Mostly cloudy, clearing, pm
28	44	33	33	0.08	0	0													lt rain
29	41	32	33	0	0	0													Partly cloudy
30	44	32	38	0	0	0													Partly cloudy
31	46	38	41	7	0	0													Mostly cloudy
32	44.4	32.6	37.4	2.24	11.18														Cloudy, overcast, lt rain, overcast
CONDITION OF RIVER AT GAGE				CHECK BAR (For mile-weight) NORMAL CK. BAR		OBSERVER		SUPERVISING OFFICE		STATION INDEX NO.									
READING				DATE		WFO, TAUNTON		19-2451-3											
A. Obstructed by rough ice. B. Frozen, but open at gage. C. Upper surface of smooth ice. D. Ice gorge above gage.				E. Ice gorge below gage. F. Shove ice. G. Flooding ice. H. Pool stage.															

TOTAL P.01

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APPENDIX B
November 2002 – September 2004 Ion Data

Plymouth Well Sampling Summary

Sample Date	Sample ID	Borehole ID	DO (mg/L)	Measured Conductivity (uS/cm)	Cyle Conductivity (uS/cm)	NH Charge	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ³⁺ Conc. (mg/L)
11/12/2002	13	AE	6.5	0.89	70	-16.5%	40.4	1.0	4.1	5.9	11.5	0.5	0.3	1.5	0.1
11/12/2002	14	AF	6.5	0.90	85	5%	37.0	0.8	6.5	7.8	11.1	1.2	1.9	4.5	2.5
11/12/2002	15	AG	6.5	0.74	312	35%	104.9	1.1	54.1	12.4	35.2	2.0	9.1	20.2	7.6
11/12/2002	16	AH	6.7	1.17	340	49%	134.7	1.7	58.2	15.3	48.4	2.1	9.0	10.7	7.2
11/12/2002	62	AK	6.3	2.02	154	-14.6%	39.3	0.0	24.0	14.4	19.0	0.7	4.3	6.2	2.3
11/12/2002	29	AL	6.8	0.80	101	-7.5%	58.0	1.1	11.5	11.5	12.8	0.6	3.0	5.3	2.5
11/12/2002	39	AS	6.7	0.95	214	0.5%	118.7	1.2	50.5	16.7	12.9	2.0	11.5	15.5	3.4
11/12/2002	57	AT	6.4	2.7	183	6.5%	61.7	0.0	23.6	18.5	24.3	1.3	6.1	10.7	0.3
11/12/2002	69	AU	5.9	0.04	65	70	14.5%	3.6	0.0	12.3	5.4	12.2	1.9	0.4	1.1
11/12/2002	33	AV	6.2	3.59	219	23%	14.7	0.9	56.1	3.2	22.9	1.8	4.9	12.0	0.0
11/12/2002	97	AW	6.3	0.00	72	69	2.7%	8.0	0.0	12.3	5.1	9.6	1.1	0.6	1.8
11/12/2002	31	AX	6.1	3.21	70	72	-0.3%	8.5	1.2	15.9	8.5	9.5	1.0	0.7	2.0
11/12/2002	32	AY	6.2	6.79	134	14%	11.9	1.0	25.5	4.5	14.0	0.8	3.5	8.2	0.0
11/12/2002	33	AY	6.2	6.79	134	14%	20.1	0.8	27.0	4.1	14.7	0.8	3.5	8.1	0.0
11/12/2002	58	AZ	5.8	5.18	65	63	4.2%	1.7	0.0	10.1	8.5	10.4	1.3	0.6	0.8
11/12/2002	59	BA	5.4	0.10	130	124	9.7%	0.0	0.0	27.4	9.0	21.7	1.6	0.8	1.7
11/12/2002	100	BB	5.6	1.30	73	79	14.4%	1.2	0.0	13.2	5.5	10.8	1.8	0.5	1.6
11/12/2002	23	BC	5.6	2.16	94	93	6.5%	1.8	0.0	18.9	7.5	16.3	1.2	0.4	0.8
11/12/2002	63	BD	6.7	0.03	114	114	-8.4%	45.6	0.0	13.4	10.2	10.5	6.2	3.2	4.5
11/12/2002	64	BD	6.7	0.03	117	126	-7.3%	56.8	0.0	11.3	9.7	17.5	0.7	2.2	4.9
11/12/2002	65	BD	6.8	0.03	155	176	1.0%	54.8	0.0	15.5	18.9	16.7	0.6	5.2	4.2
11/12/2002	66	BD	6.9	0.09	158	183	-8.5%	60.6	0.0	15.6	19.0	18.6	0.9	6.0	5.1
11/12/2002	67	BD	6.8	0.09	169	163	-4.1%	59.7	0.0	25.0	5.4	18.2	0.8	4.8	5.7
11/12/2002	68	BD	6.3	3.47	91	87	4.9%	12.2	0.0	15.0	5.5	12.5	1.7	1.0	2.1
11/12/2002	69	BD	6.8	0.10	127	140	-1.0%	49.3	0.0	13.4	10.2	10.5	6.2	3.2	4.5
11/12/2002	70	BD	6.9	0.00	231	227	2.7%	120.2	0.0	24.8	15.4	25.2	1.0	10.1	14
11/12/2002	73	BD	5.8	5.18	107	102	14.0%	4.7	0.0	21.5	4.0	13.7	2.0	1.5	3.6
11/12/2002	53	BD	6.7	0.09	173	205	7.7%	54.3	0.0	21.2	17.5	17.0	0.6	7.6	12.6
11/12/2002	54	BE	5.9	2.22	114	109	1.7%	11.4	0.0	23.9	4.1	13.6	1.8	1.6	3.3
11/12/2002	55	BE	5.9	7.22	114	105	7.7%	6.1	0.0	23.4	3.9	17.7	1.6	2.2	3.4
11/12/2002	93	BE	6.0	0.03	329	324	2.7%	101.3	0.0	31.4	35.2	1.2	9.6	10.2	5.3
11/12/2002	94	BH	6.4	0.00	67	70	-13.7%	16.3	0.0	11.3	6.0	9.7	0.9	0.1	1.2
11/12/2002	92	BI	5.8	6.16	165	163	19.1%	2.5	0.0	36.7	5.0	25.2	1.7	2.2	6.0
11/12/2002	34	BJ	6.4	2.41	218	330	14.0%	41.4	1.0	20.9	2.8	30.2	1.2	9.7	22.1
11/12/2002	37	BK	5.9	0.29	117	113	11.1%	3.1	0.0	26.5	3.5	15.6	1.4	1.6	3.6
11/12/2002	35	BL	6.3	3.39	169	113	3.3%	72.4	1.2	18.2	5.7	16.7	0.8	1.0	3.6
11/12/2002	42	BM	5.6	4.46	145	137	3.2%	6.1	0.0	35.0	5.7	22.2	1.2	0.7	2.5
11/12/2002	43	BM	6.5	0.55	243	249	-2.1%	2.9	0.0	15.6	13.6	2.6	0.8	3.2	11.7
11/12/2002	44	BM	6.5	0.55	243	269	2.1%	76.7	0.7	35.7	13.8	28.8	0.9	4.9	14.0
11/12/2002	45	BM	6.7	0.15	151	159	-11.9%	62.8	0.0	16.7	1.9	17.7	0.9	1.3	6.8
11/12/2002	46	BM	6.2	4.04	100	101	0.3%	16.9	0.0	18.2	5.1	13.6	1.6	0.9	2.9
11/12/2002	47	BM	6.1	6.50	92	94	-4.4%	10.7	0.0	18.9	6.0	10.3	1.3	0.8	1.9
11/12/2002	48	BM	5.8	9.91	83	78	4.9%	0.0	0.0	15.5	4.9	13.0	1.0	1.3	0.0
11/12/2002	49	BM	5.5	8.01	89	83	6.5%	4.2	0.0	18.0	4.2	11.8	1.1	0.7	2.4
11/12/2002	50	BM	5.5	8.01	124	131	-11.4%	2.5	0.0	27.1	4.5	17.3	1.4	1.6	3.6
11/12/2002	51	BM	5.4	8.11	119	109	8.0%	4.2	0.0	24.6	4.9	16.3	1.3	1.0	2.7
11/12/2002	40	BN	6.6	2.39	117	134	-10.1%	43.9	0.7	19.2	7.2	17.2	1.1	1.7	3.6
11/12/2002	28	BO	5.8	0.09	75	81	-2.4%	12.1	1.0	15.2	4.4	10.8	1.3	0.5	2.1
11/12/2002	19	BO	6.7	0.25	335	366	-3.2%	132.1	1.4	48.9	11.3	49.9	1.5	6.8	14.8
11/12/2002	20	BO	6.9	0.28	334	282	-10.5%	120.9	1.2	38.0	7.2	35.6	1.2	4.3	9.9
11/12/2002	21	BO	6.9	0.27	230	258	-5.2%	78.4	1.2	41.6	8.3	26.4	1.3	6.6	11.9
11/12/2002	22	BO	6.9	0.27	230	260	-4.5%	84.0	1.3	41.4	7.5	26.4	1.5	6.3	12.0
11/12/2002	23	BO	6.9	0.26	218	219	1.0%	67.2	1.4	55.2	5.9	30.0	1.5	7.5	13.9
11/12/2002	24	BO	6.9	0.34	212	214	-0.6%	74.5	1.3	31.4	9.1	25.7	1.0	3.9	7.3
11/12/2002	25	BO	6.9	0.02	177	183	-13.5%	65.9	0.3	29.2	6.5	19.9	1.1	3.2	6.1
11/12/2002	26	BO	6.6	0.90	108	126	-15.3%	49.5	1.0	15.4	7.6	19.3	2.6	0.6	1.3
11/12/2002	27	BO	6.0	7.69	103	103	2.4%	19.3	0.9	16.5	6.1	13.7	1.5	1.3	3.3
11/12/2002	17	BP	6.7	0.03	260	271	-4.5%	66.8	0.3	53.4	7.4	20.1	1.2	5.7	11.7
11/12/2002	18	BQ	6.4	5.33	61	63	-20.0%	21.2	0.0	10.3	5.5	8.4	0.8	0.4	1.1
11/12/2002	41	BR	5.9	0.09	85	86	4.7%	5.8	0.0	18.4	4.0	11.6	1.3	1.0	2.4
11/12/2002	95	BS	6.1	0.00	65	67	-0.6%	11.8	0.0	10.6	5.3	8.5	1.0	0.9	1.9
11/12/2002	74	BT	6.7	0.00	219	269	-4.5%	45.6	0.0	17.9	12.2	38.2	1.5	9.9	14.9
11/12/2002	75	BT	6.9	0.00	210	349	0.8%	147.1	0.0	35.4	14.4	35.2	1.0	10.8	21.4
11/12/2002	76	BT	7.0	0.00	217	385	2.1%	131.8	0.0	58.4	6.4	36.5	1.4	11.6	23.1
11/12/2002	77	BT	7.1	0.00	237	356	0.8%	130.1	0.3	31.3	10.0	24.2	1.2	9.9	20.6
11/12/2002	78	BT	7.1	0.00	237	301	1.6%	125.6	0.4	29.0	10.1	25.9	1.4	9.6	19.5
11/12/2002	79	BT	7.1	0.00	242	330	4.3%	138.2	0.2	30.1	12.8	27.9	1.4	10.3	23.5
11/12/2002	80	BT	7.2	0.00	234	255	2.5%	110.0	0.0	29.0	11.9	25.3	1.2	21.2	4.3
11/12/2002	81	BT	7.2	0.00	232	184	-0.4%	56.7	0.0	24.1	7.8	20.5	0.7	6.8	13.9
11/12/2002	82	BT	7.2	0.00	187	192	-3.2%	13.6	0.0	16.7	6.3	16.3	0.8	5.3	11.5
11/12/2002	83	BT	6.2	0.43	101	93	6.3%	6.9	0.0	21.5	4.0	13.8	1.3	0.7	-2.9
11/12/2002	84	BT	6.7	0.09	172	169	9.0%	30.1	0.0	39.2	5.3	21.3	0.7	3.2	7.8
11/12/2002	85	BT	6.5	0.00	144	158	9.1%	32.1	0.0	16.5	17.8	19.0	2.1	3.7	6.9
11/12/2002	86	BU	6.7	0.09	150	178	3.4%	62.1	0.0	21.6	5.4	15.3	0.9	3.5	10.9
11/12/2002	87	BU	6.7	0.09	150	178	4.0%	49.5	0.0	21.6	5.4	14.6	1.0	6.0	11.1
11/12/2002	88	BV	6.6	0.00	110	116	-14.7%	27.5	0.2	10.8	4.4	10.2	1.5	4.5	3.5
11/12/2002	89	BV	6.6	0.00	78	78	6.1%	9.3	0.0	14.1	4.8	12.6	0.9	0.8	1.5
11/12/2002	90	BZ	6.8	0.00	418	472	5.2%	131.2	0.0	82.0	9.8	72.7	1.7	8.2	18.9
11/12/2002	91	CA	6.4	1.03	210	223	6.5%	48.1	1.2	33.1	14.0	31.6	1.3	3.4	9.0
11/12/2002	92	CB	6.7	0.10	137	141	1.7%	48.2	0.0	15.8	9.5	27.3	1.5	2.3	4.4
11/12/2002	93	CC	6.1	1.25	89	82	5.9%	7.2	1.0	15.4	4.9	12.9	1.1	1.7	0.0
11/12/2002	94	CD	6.8	0.00	237	272	-4.7%	185.3	0.0	25.3	10.2	25.4	0.9	5.9	13.4
11/12/2002	95	ST	5.9	3.39	189	197	17.5%	10.2	0.0	42.6	5.4	22.6	2.5	4.2	10.5
11/12/2002	11	UB101	5.9	11.59	33	51	2.1%	2.6	1.1	6.3	6.0	7.0	0.9	0.7	1.0

Updated 35519.0 SVK NM = not analyzed NS = not sampled BDL = below detection limit DND = did not detect
 If listed as 0, below 1. rounded, but above detection limit

Plymouth Well Sampling Summary

Sample Date	Sample ID	Borehole ID	DO (mg/L)	Measured Conductivity (mS/cm)	Cyle Conductivity (mS/cm)	Net Change	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ³⁺ Conc. (mg/L)	Updated	385190	SVK	ND1 - NS	not measured not accepted	BDL = below detection limit DND = did not detect if listed as BDL, rounded, but above detection limit	
11/12/2002	12	UB102	5.6	17.54	51	1.5%	3.4	1.0	8.4	5.7	7.3	1.0	0.5	0.9	0.0							
11/12/2002	7	UB102	5.3	9.97	111	6.5%	1.0	0.7	23.8	7.3	18.9	1.1	0.6	1.1	0.0							
11/12/2002	5	UB203	5.9	8.71	57	-3.0%	2.6	0.8	9.5	8.3	7.8	0.3	0.5	1.9	0.0							
11/12/2002	8	UB204	5.5	3.61	61	6.6%	2.7	0.7	9.9	5.3	8.5	0.9	0.4	1.1	0.0							
11/12/2002	5	UB255	5.6	3.36	82	89	13.1%	1.6	0.8	15.5	6.0	11.2	1.0	1.5	2.4	0.0						
11/12/2002	9	UC102	5.7	10.74	55	41	-5.3%	4.8	0.8	6.5	7.2	5.8	1.8	0.5	0.7	0.0						
11/12/2002	10	UC102	5.7	10.74	55	41	-0.3%	3.4	0.8	6.5	6.8	4.8	1.9	0.7	1.2	0.0						
11/12/2002	1	UC102	6.7	11.61	110	129	0.0	19.4	0.0	16.0	27.5	19.0	1.1	0.3	0.2	0.0						
11/12/2002	1	UC203	6.1	10.70	76	74	-5.9%	12.0	0.6	11.3	8.0	10.9	3.1	0.2	0.5	0.0						
11/12/2002	2	UC204	5.8	11.02	76	93	-17.6%	8.5	1.1	9.3	23.0	9.1	4.1	0.6	1.2	0.0						
11/12/2002	4	UC205	5.6	6.65	106	166	7.6%	4.7	0.8	14.1	18.4	9.5	5.2	1.9	4.0	0.0						
11/12/2002	95	West Well	6.7	0.00	133	135	-4.7%	41.4	0.0	15.3	10.4	16.9	2.0	5.3	2.3	0.1						
12/19/2002	101	AB	6.2	9.84	114	104	8.0%	3.2	1.5	12.7	19.0	14.2	0.9	1.9	3.5	1.1						
12/19/2002	102	AC	6.5	10.65	91	84	9.5%	9.9	BDL	12.7	7.5	11.4	0.9	0.9	3.3	0.2						
12/19/2002	103	AD	6.1	9.40	695	648	20.1%	11.8	1.5	171.5	2.6	76.0	1.0	16.9	42.6	0.3						
12/19/2002	34	AE	6.7	5.79	76	102	41.8%	13.8	0.0	4.9	23.1	7.9	-0.9	1.3	1.3	0.0						
12/19/2002	35	AF	6.4	7.39	71	61	10.4%	14.4	0.0	5.1	6.4	7.9	0.9	1.1	2.5	1.0						
12/19/2002	35	AG	6.5	2.07	165	152	24.2%	25.5	0.0	19.0	12.7	25.9	6.0	4.3	9.4	2.3						
12/19/2002	36	AH	6.8	0.95	101	56	17.0%	22.6	0.0	6.9	9.5	10.9	0.9	2.2	5.8	0.4						
12/19/2002	92	AI	6.4	6.50	85	81	3.3%	12.6	1.9	11.9	6.9	10.4	0.5	0.8	3.1	0.6						
12/19/2002	95	AJ	6.4	8.49	114	106	15.8%	13.2	1.7	16.2	5.7	13.9	1.5	1.8	4.5	2.0						
12/19/2002	37	AK	6.2	9.55	79	76	-1.5%	7.9	0.0	139.2	5.7	52.9	1.3	39.5	37.1	5.5						
12/19/2002	39	AL	6.5	1.72	548	567	25.1%	15.5	1.6	12.0	7.4	14.9	0.6	1.0	2.4	0.2						
12/19/2002	94	AN	6.6	9.85	101	89	12.3%	10.5	1.6	14.7	10.1	14.9	1.1	1.5	4.3	0.7						
12/19/2002	95	AO	6.2	8.23	111	103	18.2%	17.2%	1.6	10.0	10.0	16.9	0.5	4.7	16.6	2.6						
12/19/2002	95	AP	6.6	4.95	169	173	17.6%	37.3	BDL	11.3	7.0	9.1	0.1	1.2	3.5	0.9						
12/19/2002	40	AQ	6.1	4.26	85	76	6.3%	11.6	BDL	11.3	7.0	9.1	0.1	1.2	3.5	0.9						
12/19/2002	81	AR	5.7	9.44	100	85	10.8%	5.2	0.0	17.7	4.5	9.8	0.7	2.5	3.4	1.0						
12/19/2002	39	AS	6.1	1.50	1033	1433	40.5%	16.6	BDL	456.6	8.8	264.8	5.2	29.3	34.8	6.4						
12/19/2002	20	AT	6.7	2.55	2206	1193	82.3%	8.2%	0.0	620.4	14.0	415.7	2.3	30.5	30.3	1.1						
12/19/2002	97	AU	6.1	1.60	71	71	0.0%	6.3%	1.6	11.2	4.9	12.1	1.5	0.4	1.2	0.0						
12/19/2002	97	AV	6.5	2.64	112	107	12.3%	26.1	BDL	34.0	7.2	27.4	1.3	2.4	7.7	0.2						
12/19/2002	100	AV	6.5	2.48	139	155	11.0%	27.8	1.6	32.9	7.2	26.9	1.4	2.7	7.4	0.1						
12/19/2002	112	AW	6.3	1.65	115	71	3.4%	7.0	1.7	12.4	5.4	9.7	1.2	0.7	2.0	0.0						
12/19/2002	104	AX	6.2	6.18	77	65	11.1%	4.6	1.3	10.5	5.7	9.7	1.0	0.6	2.0	0.0						
12/19/2002	109	AY	6.3	7.81	145	144	18.0%	22.1	1.8	21.0	5.8	17.1	1.0	2.5	9.0	0.0						
12/19/2002	110	AY	6.3	7.81	145	145	12.2%	22.5	1.7	21.2	5.8	16.3	0.9	2.4	9.9	0.0						
12/19/2002	113	AZ	5.8	7.10	69	69	13.9%	12.7	1.7	10.1	7.9	9.7	1.2	0.8	2.3	0.1						
12/19/2002	114	BA	5.7	9.10	85	75	-9.5%	1.2	2.7	15.8	7.4	9.3	1.1	0.4	1.9	0.0						
12/19/2002	115	BB	5.6	0.60	82	75	11.0%	2.1	1.4	14.8	5.0	12.9	1.6	0.5	1.1	0.1						
12/19/2002	48	BC	6.3	4.37	82	75	7.0%	5.4	0.0	13.1	7.0	11.2	0.9	0.4	2.0	0.0						
12/19/2002	49	BC	6.3	4.37	82	72	3.0%	11.5%	15.9	BDL	3.9	13.8	7.6	0.5	2.9	4.3	1.8					
12/19/2002	51	BC	7.6	1.24	95	78	10.7%	21.9	BDL	4.2	8.8	8.3	0.5	1.9	4.4	0.9						
12/19/2002	52	BC	7.6	1.24	95	78	8.0%	14.4	BDL	3.5	12.5	7.7	0.5	2.0	3.4	1.7						
12/19/2002	53	BC	7.5	1.72	79	72	9.0%	0.4%	5.6	BDL	49.0	9.9	13.7	1.0	6.6	8.8	16.1					
12/19/2002	54	BC	7.1	0.66	223	192	-1.4%	0.5	BDL	49.0	9.9	13.7	1.0	6.6	8.8	16.1						
12/19/2002	54	BC	7.1	0.66	223	187	-2.4%	7.5	BDL	7.4	10.6	12.1	1.2	0.3	1.3	0.0						
12/19/2002	56	BC	7.1	0.62	85	75	2.4%	22.1	BDL	8.5	11.1	9.6	0.5	3.9	6.4	2.7						
12/19/2002	57	BC	7.0	0.88	113	105	14.9%	32.1	BDL	8.2	14.7	15.2	1.1	2.9	7.8	0.5						
12/19/2002	58	BC	7.3	1.52	114	114	23.7%	33.7	BDL	8.5	11.9	11.5	0.7	3.2	7.5	0.7						
12/19/2002	59	BC	7.2	1.71	115	114	-4.5%	3.9	BDL	163.1	8.2	31.9	1.5	15.5	26.8	5.7						
12/19/2002	60	BC	6.7	0.65	574	511	-10.5%	9.9	0.0	16.8	9.1	17.3	1.7	2.2	3.2	0.0						
12/19/2002	61	BC	6.4	0.98	116	114	12.4%	22.5	0.0	18.0	12.7	12.4	0.7	5.1	10.7	0.9						
12/19/2002	90	BD	7.0	0.91	111	132	32.3%	6.9	0.0	13.0	10.9	29.9	1.1	0.6	0.9	0.0						
12/19/2002	74	BE	6.4	2.79	107	115	14.1%	4.6	1.6	24.6	4.9	16.8	1.4	1.4	4.4	0.0						
12/19/2002	75	BF	6.2	3.05	115	248	18.1%	47.8	BDL	32.6	14.5	30.8	1.1	6.2	14.9	4.3						
12/19/2002	75	BO	6.7	4.55	246	248	14.4%	5.3	BDL	11.8	5.6	14.0	2.0	0.5	1.1	0.0						
12/19/2002	77	BN	6.3	0.60	76	74	18.0%	4.8	BDL	11.8	5.2	7.9	0.9	0.9	2.5	0.0						
12/19/2002	77	BN	6.3	0.60	76	66	14.3%	4.4	BDL	29.0	4.0	19.3	1.5	1.8	4.1	0.0						
12/19/2002	78	BI	6.0	6.12	151	129	15.6%	35.1	1.7	29.7	4.5	22.2	0.9	3.4	10.6	0.9						
12/19/2002	105	BJ	6.6	11.04	193	184	4.8%	17.7	BDL	13.3	5.2	10.2	1.0	0.7	2.4	0.0						
12/19/2002	79	BK	6.0	1.25	75	137	7.4%	13.9	2.1	25.0	9.2	22.5	0.5	0.9	3.7	0.0						
12/19/2002	111	BL	6.5	3.40	149	103	10.3%	2.7	0.9	23.5	6.4	22.5	1.2	0.2	0.1	0.0						
12/19/2002	16	BM	6.5	5.00	118	103	7.5%	35.4	0.0	373.0	9.7	207.6	1.5	13.2	14.0	3.1						
12/19/2002	17	BM	6.5	0.17	1439	1203	24.3%	13.8	0.0	723.0	7.9	645.6	5.2	46.7	45.6	14.5						
12/19/2002	18	BM	6.4	0.16	2490	2338	0.6%	24.2	0.0	205.8	8.9	519.7	4.7	31.0	19.5	0.1						
12/19/2002	19	BM	6.4	0.30	2068	2415	0.1%	24.2	0.0	264.2	10.5	133.2	4.0	22.1	32.5	0.1						
12/19/2002	20	BM	6.0	0.20	987	887	10.3%	4.0	0.0	17.9	6.2	14.3	1.2	0.8	1.2	0.0						
12/19/2002	21	BM	6.0	0.77	107	95	4.0%	7.2	0.0	18.2												

Sample Date	Sample ID	Borehole ID	pH	DO (mg/L)	Measured Conductivity (mS/cm)	Cyle Conductivity (mS/cm)	Net Charge	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ³⁺ Conc. (mg/L)
12 19 2002	33	BOB	6.1	7.24	141	99	-15.1%	9.6	0.9	24.6	6.7	10.5	1.1	0.7	2.0	0.0
12 19 2002	49	DP	6.5	0.21	302	258	4.0%	55.5	0.0	42.3	14.6	34.7	1.4	5.1	5.8	19.1
12 19 2002	27	DQ	6.0	0.09	91	76	7.3%	7.4	0.0	14.1	4.8	11.1	1.1	0.8	2.0	0.0
12 19 2002	24	DR	5.5	4.05	281	257	12.3%	3.1	0.0	67.7	1.9	23.4	2.5	4.4	13.1	0.0
12 19 2002	82	DS	6.1	0.20	48	75	25.1%	8.5	0.0	9.0	5.7	13.9	1.8	1.0	2.1	0.0
12 19 2002	62	DTA	6.9	1.08	133	124	14.2%	25.8	BDL	12.1	11.7	15.5	0.8	3.3	6.0	1.8
12 19 2002	63	DTB	6.9	1.25	255	255	14.9%	55.1	0.0	37.0	6.4	25.2	0.7	8.9	15.2	4.1
12 19 2002	64	DTc	7.1	0.32	243	245	16.2%	59.1	BDL	33.8	8.3	27.0	0.8	7.8	15.6	3.6
12 19 2002	65	DTG	7.2	0.18	227	230	18.7%	54.5	BDL	28.4	8.6	25.1	0.7	6.4	16.0	2.9
12 19 2002	66	DTd	7.2	0.18	237	240	19.0%	57.5	BDL	25.7	11.2	24.6	0.7	6.8	17.3	3.9
12 19 2002	67	DTe	7.3	0.18	164	164	15.9%	44.3	BDL	16.8	5.6	17.9	0.7	3.9	10.8	3.2
12 19 2002	68	DTF	7.3	0.18	145	142	15.0%	33.7	BDL	14.5	10.2	14.3	0.7	3.8	8.8	2.3
12 19 2002	69	DTG	7.3	0.16	155	147	11.3%	35.9	BDL	19.3	4.1	14.5	0.7	4.0	8.4	2.9
12 19 2002	70	DTH	7.2	0.16	158	156	17.4%	33.4	BDL	20.8	5.5	15.2	0.7	5.1	10.3	3.6
12 19 2002	71	DTI	5.9	5.54	221	212	12.0%	3.2	BDL	54.9	2.9	25.0	1.9	3.6	9.1	0.0
12 19 2002	72	DTJ	6.7	1.87	216	195	16.3%	26.9	BDL	33.7	7.1	23.1	0.7	4.3	11.2	10.1
12 19 2002	73	DTK	6.6	1.31	172	171	19.4%	16.3	BDL	22.8	16.3	18.9	2.3	6.4	9.9	3.4
12 19 2002	83	DU	6.4	5.17	140	119	12.3%	18.7	1.3	28.0	3.1	14.4	1.0	4.6	4.5	0.0
12 19 2002	84	DV	6.7	0.50	119	110	19.2%	27.5	3.1	10.1	4.3	10.1	1.4	5.4	6.6	1.8
12 19 2002	85	DW	6.4	0.59	93	85	-3.5%	9.0	0.0	18.2	5.4	10.9	1.0	0.6	2.3	0.0
12 19 2002	86	DZ	6.6	0.17	359	316	16.1%	65.5	0.0	49.0	10.6	59.3	1.3	4.1	11.3	8.5
12 19 2002	106	CA	6.4	1.17	203	197	19.4%	28.2	1.5	21.0	12.1	21.2	1.3	2.0	10.5	0.0
12 19 2002	87	CB	6.6	2.17	211	197	16.4%	29.5	0.0	31.1	9.3	25.0	1.2	0.7	12.0	0.4
12 19 2002	107	CC	6.2	3.00	87	45	10.3%	6.6	1.6	16.0	4.5	11.8	1.2	0.8	3.1	0.0
12 19 2002	108	CD	6.6	0.81	1212	1101	9.3%	32.4	58.1	313.7	2.3	164.1	2.1	39.8	47.4	0.0
12 19 2002	31	ST	6.7	1.02	148	133	8.2%	22.7	0.0	20.3	9.0	18.3	1.7	2.3	4.6	2.3
12 19 2002	14	UB101	5.7	10.65	59	48	1.5%	1.0	0.0	9.1	5.8	7.1	0.8	0.2	0.8	0.0
12 19 2002	15	UB102	5.8	10.70	59	48	-0.5%	0.6	0.0	9.1	6.0	6.9	0.8	0.2	0.7	0.0
12 19 2002	11	UB101	5.3	10.29	711	181	3.1%	0.1	0.0	49.1	6.7	24.0	0.9	0.0	0.5	0.0
12 19 2002	9	UB102	5.5	10.72	62	70	29.9%	0.2	0.0	10.1	6.7	12.8	1.8	1.2	1.6	0.0
12 19 2002	10	UB102	5.5	10.32	62	52	2.7%	0.1	0.0	9.9	6.4	8.5	0.8	0.2	0.5	0.0
12 19 2002	7	UB103	5.6	10.42	61	51	4.7%	1.5	0.0	9.6	5.3	7.5	1.0	0.2	1.0	0.0
12 19 2002	8	UB104	5.6	10.07	65	52	9.1%	1.0	0.0	10.4	6.0	8.7	1.0	0.5	1.1	0.0
12 19 2002	6	UB105	5.7	9.97	94	79	16.9%	3.2	0.0	13.2	7.1	11.7	1.2	1.2	2.5	0.0
12 19 2002	12	UC101	5.7	10.42	55	21	21.6%	1.4	0.0	6.7	6.5	7.1	2.1	0.9	1.5	0.0
12 19 2002	13	UC102	5.5	10.32	65	69	5.5%	1.0	0.0	11.2	6.6	8.5	1.1	0.6	1.2	0.0
12 19 2002	4	UC201	5.7	9.36	346	303	0.3%	1.4	0.0	85.2	13.1	62.3	1.2	0.0	0.0	0.0
12 19 2002	5	UC202	5.9	9.66	55	49	-3.5%	3.2	0.0	14.5	15.2	16.1	1.0	0.0	0.0	0.0
12 19 2002	1	UC203	6.1	8.65	75	69	8.0%	4.8	0.0	8.9	8.6	10.5	3.8	0.3	0.5	0.0
12 19 2002	2	UC204	5.9	9.07	74	65	11.1%	5.1	0.0	7.5	9.6	9.4	4.3	0.4	0.9	0.0
12 19 2002	3	UC205	5.7	3.59	166	87	14.3%	14.3	0.0	10.2	8.9	4.5	1.3	3.1	3.1	0.0
12 19 2002	59	West Well	6.9	6.47	7593	2690	12.0%	93.1	59.2	2158.5	27.9	1317.7	6.1	229.2	165.0	0.3
1 21 2003	40	AB	6.4	11.14	85	88	na	8.7	0.0	14.1	9.3	88	88	88	88	0.0
1 21 2003	41	AB	6.4	11.14	85	94	10.4%	6.4	0.0	15.3	9.6	11.8	1.3	2.8	2.7	0.0
1 21 2003	45	AC	5.6	12.22	104	101	70.2%	3.8	0.0	15.8	8.3	14.7	0.6	2.8	3.3	0.0
1 21 2003	39	AD	6.7	10.71	105	104	-9.8%	24.8	16.7	79.9	10.7	10.4	0.4	2.6	1.0	0.4
1 21 2003	56	AE	7.0	4.47	217	214	-9.3%	19.6	0.0	60.0	3.5	35.7	1.0	0.0	1.9	0.0
1 21 2003	59	AE	7.0	4.47	217	220	-15.7%	15.8	0.0	65.5	3.9	34.7	1.0	0.0	1.1	0.0
1 21 2003	60	AF	6.9	3.61	125	101	-9.6%	12.0	0.0	22.8	5.8	8.4	0.7	2.5	3.5	1.1
1 21 2003	63	AG	7.1	4.24	119	114	-13.9%	16.1	0.0	39.0	2.8	17.8	1.1	0.0	0.7	0.0
1 21 2003	56	AH	7.3	0.42	165	181	-10.6%	26.3	0.0	37.8	3.9	15.6	0.9	0.0	2.2	0.3
1 21 2003	50	AI	6.7	6.44	71	76	5.4%	7.6	0.0	8.3	4.9	8.6	0.7	2.9	8.7	0.1
1 21 2003	31	AK	6.8	9.56	52	71	14.7%	14.1	0.0	5.6	8.1	10.6	0.8	2.8	1.5	0.0
1 21 2003	32	AK	6.8	9.56	52	60	-13.3%	15.1	0.0	5.4	8.2	7.3	0.5	2.3	1.0	0.1
1 21 2003	17	AL	6.3	6.03	219	249	2.6%	17.9	0.0	61.7	8.2	43.8	0.7	3.7	2.6	0.9
1 21 2003	47	AM	6.4	0.60	161	174	0.1%	39.5	0.0	25.5	13.2	18.0	0.9	5.7	6.7	0.0
1 21 2003	44	AN	6.6	7.35	84	87	3.3%	19.0	0.0	10.8	6.2	12.2	0.6	2.6	2.5	0.1
1 21 2003	37	AO	7.4	4.54	139	135	-0.3%	49.8	0.0	14.5	11.1	15.8	0.8	4.3	4.4	0.1
1 21 2003	102	AP	6.2	2.60	115	104	17.5%	15.8	0.0	13.4	7.5	15.2	0.6	4.4	2.9	0.0
1 21 2003	97	AQ	6.3	2.03	81	64	-7.3%	6.2	0.0	9.9	9.7	8.0	0.2	0.0	1.9	1.6
1 21 2003	81	AR	6.0	4.70	120	84	9.5%	5.0	0.0	14.3	8.8	14.0	0.4	0.0	2.3	0.0
1 21 2003	30	AS	6.4	0.20	520	522	1.5%	30.3	0.0	150.0	4.1	82.5	2.9	12.5	8.7	1.9
1 21 2003	69	AT	6.7	0.65	389	344	-13.3%	63.1	0.0	73.9	15.3	57.7	0.6	0.0	7.9	2.1
1 21 2003	42	AU	0.0	1.33	77	77	23.8%	0.0	0.0	5.4	10.4	1.0	2.3	2.9	2.9	0.0
1 21 2003	112	AV	6.2	10.41	139	139	7.5%	10.4	0.0	23.5	11.0	20.4	1.0	3.3	2.7	0.0
1 21 2003	117	AW	7.4	1.49	73	94	13.0%	10.4	0.0	14.3	11.5	11.6	1.2	2.1	2.3	0.0
1 21 2003	110	AX	6.0	9.70	181	70	7.8%	3.4	0.0	13.0	6.3	10.3	1.0	1.5	1.0	0.0
1 21 2003	111	AX	6.0	9.70	181	73	-0.6%	3.3	0.0	12.9	9.4	9.1	1.1	1.9	1.1	0.0
1 21 2003	109	AY	6.7	6.24	150	136	6.6%	26.3	0.0	19.6	10.4	22.8	0.7	1.4	3.5	0.0
1 21 2003	116	AZ	7.5	7.70	75	85	-14.5%	4.6	0.0	16.8	12.3	10.8	1.0	1.5	0.2	0.0
1 21 2003	118	BA	7.2	9.70	37	40	6.0%	4.1	0.0	13.9	8.1	11.0	1.1	1.6	1.7	0.0
1 21 2003	115	BB	8.0	2.20	18	18	1.6%	0.0	0.0	17.0	5.8	12.4	1.6	1.8	2.3	0.0
1 21 2003	49	BC	5.9	0.00	83	43	3.4%	5.0	0.0	15.7	7.9	12.4	0.9	1.2	1.4	0.0
1 21 2003	70	BC*	7.0	0.91	758	712	-0.7%	83.6	0.0	201.9	3.5	147.2	1.4	4.5	3.9	3.1
1 21 2003	62	BC*	7.0	0.65	670	644	-2.8%	33.5	0.0	197.0	6.3	121.6	0.8	0.0	8.0	1.5
1 21 2003	58	BC*	7.0	0.58	1192	1063	-0.8%	65.1	0.0	344.8	1.0	218.4	1.4	0.0	14.6	15.8
1 21 2003	24	BC*	6.4	0.64	637	649	-16.1%	17.2	55.2	204.8	8.5	290.0	1.2	8.0	22.2	11.7
1 21 2003	23	BC*	6.1	0.55	1195	1176	-1.5%	12.3	0.0	404.2	8.7	203.0	1.8	21.5	18.1	27.1
1 21 2003	22	BC*	6.5	0.78	1073	1073	-1.7%	44.4	7.6	108.6	8.9	77.7	1.4	8.8	5.2	2.2
1 21 2003	53	BC*	6.9	0.58	1815	1763	-109.6%	54.3	0.0	584.7	1.0	na	na	na	na	10.0
1 21 2003	54	BC*	7.0	0.55	1455	1253</										

Phonoth Well Sampling Summary

Sample Date	Sample ID	Borehole ID	DO (mg/L)	Measured Conductivity (mS/cm)	Calc Conductivity (mS/cm)	Net Charge
12/1/2003	103	DE	6.4	0.03	1643	3.4%
12/1/2003	106	DE	6.6	0.07	157	3.1%
12/1/2003	91	BU	6.8	4.25	177	-1.1%
12/1/2003	75	BH	5.9	4.25	65	-6.4%
12/1/2003	85	BI	5.8	4.23	161	0.9%
12/1/2003	109	BI	6.3	1.34	234	2.1%
12/1/2003	113	BU	6.2	1.45	75	0.3%
12/1/2003	108	HL	6.7	6.03	153	2.4%
12/1/2003	72	BSI	5.9	0.09	114	-2.8%
12/1/2003	71	BNL	7.3	0.20	160	-6.5%
12/1/2003	61	BNL	7.0	0.19	170	-7.1%
12/1/2003	65	BNL	6.1	0.09	154	-13.4%
12/1/2003	64	BNL	6.6	6.09	107	-12.5%
12/1/2003	68	BNL	6.2	8.50	129	-17.2%
12/1/2003	67	BNL	6.0	8.50	129	-17.2%
12/1/2003	68	BNL	6.2	8.50	129	-17.2%
12/1/2003	73	BNL	5.8	8.00	124	-10.5%
12/1/2003	65	BNL	5.7	7.90	92	-4.5%
12/1/2003	74	BNL	0.0	7.00	0	0.0%
12/1/2003	36	BN	6.7	7.00	922	3.7%
12/1/2003	25	BO	6.2	5.19	211	2.3%
12/1/2003	16	BO	6.3	0.62	233	17.2%
12/1/2003	57	BO	7.1	0.73	189	-8.6%
12/1/2003	29	BO	6.5	0.56	353	2.9%
12/1/2003	26	BO	6.5	0.54	833	-3.7%
12/1/2003	19	BO	6.2	0.71	444	3.4%
12/1/2003	20	BO	6.5	0.70	294	-6.6%
12/1/2003	21	BO	6.5	0.70	294	-6.6%
12/1/2003	23	BO	6.3	1.96	181	-22.5%
12/1/2003	35	BO	6.3	7.97	125	-12.3%
12/1/2003	24	BP	6.4	0.50	794	1.3%
12/1/2003	18	BQ	6.1	3.42	77	-5.6%
12/1/2003	27	BR	6.2	0.07	234	4.4%
12/1/2003	85	BS	5.9	0.39	64	-2.4%
12/1/2003	41	BT	7.1	1.64	121	-7.4%
12/1/2003	81	BT	6.5	1.03	454	-8.2%
12/1/2003	93	BT	6.3	0.95	230	-5.1%
12/1/2003	99	BT	6.3	0.95	230	-4.7%
12/1/2003	94	BT	7.2	0.75	146	-6.5%
12/1/2003	76	BT	6.2	0.71	653	-11.4%
12/1/2003	90	BT	6.7	0.27	1318	-9.2%
12/1/2003	90	BT	6.4	0.18	1350	-2.1%
12/1/2003	77	BT	7.0	0.00	142	-13.5%
12/1/2003	78	BT	7.0	0.00	142	-13.5%
12/1/2003	55	BT	6.1	7.97	141	6.0%
12/1/2003	83	BT	6.9	0.54	172	-5.3%
12/1/2003	39	BT	6.7	1.47	133	-14.4%
12/1/2003	88	BU	6.6	0.70	174	-12.8%
12/1/2003	89	BU	6.6	0.70	174	-12.8%
12/1/2003	45	BN	6.6	0.66	116	15.2%
12/1/2003	79	BY	6.0	5.55	86	-100.0%
12/1/2003	80	BY	6.0	5.55	86	-100.0%
12/1/2003	91	BZ	7.9	0.70	224	5.1%
12/1/2003	47	CA	6.4	1.87	175	9.1%
12/1/2003	56	CB	6.8	0.00	261	-0.7%
12/1/2003	101	CC	6.3	2.50	82	-2.5%
12/1/2003	104	CD	6.6	0.65	414	12.9%
12/1/2003	18	ST	6.4	0.49	128	0.0%
12/1/2003	14	UB101	5.5	8.70	67	0.0%
12/1/2003	15	UB102	5.5	8.93	53	6.5%
12/1/2003	6	UB201	5.4	8.67	192	1.4%
12/1/2003	7	UB202	5.5	9.82	55	-0.8%
12/1/2003	9	UB203	5.6	9.90	58	0.0%
12/1/2003	10	UB204	5.6	9.90	58	0.0%
12/1/2003	8	UB204	5.6	8.85	65	0.0%
12/1/2003	11	UB205	5.6	9.69	84	0.0%
12/1/2003	12	UC101	5.7	5.58	59	-13.6%
12/1/2003	13	UC102	5.6	7.53	66	-13.6%
12/1/2003	1	UC201	6.2	10.20	214	0.0%
12/1/2003	3	UC202	5.8	10.25	118	1.6%
12/1/2003	5	UC203	5.7	9.67	108	-3.7%
12/1/2003	2	UC204	5.9	9.45	79	0.0%
12/1/2003	4	UC205	5.6	4.95	101	-21.4%
12/1/2003	114	West Well	6.5	1.45	3353	-34.4%
2/20/2003	57	AA	6.3	15.30	71	8.3%
2/20/2003	54	AB	6.2	9.69	102	6.0%
2/20/2003	59	AC	6.5	15.45	74	7.0%
2/20/2003	58	AD	6.4	5.25	203	11.8%
2/20/2003	5	AE	6.8	7.45	152	7.7%
2/20/2003	3	AF	6.6	4.27	107	13.1%
2/20/2003	8	AG	6.6	1.01	183	14.4%
2/20/2003	2	AH	6.4	0.23	457	12.0%
2/20/2003	53	AI	6.3	6.85	112	8.1%
2/20/2003	52	AJ	6.4	11.67	81	13.5%
2/20/2003	6	AK	6.8	0.69	64	3.5%
2/20/2003	35	AL	6.5	2.79	254	11.3%

Updated	4/5/19	SVK	NMI-NS	not measured not sampled	BOL = below detection limit DND = did not detect if listed as 0, below 1, rounded, but above detection limit			
HCO ₃ ⁻ Conc. (mg/L)	Atteble Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ²⁺ Conc. (mg/L)
35.8	0.0	433.2	12.9	259.8	1.7	20.3	13.0	17.0
7.2	0.0	31.5	11.9	21.0	1.2	1.1	0.3	0.0
22.8	0.0	23.9	10.4	19.9	0.7	0.0	0.7	3.5
4.1	0.0	11.4	5.7	8.8	0.7	0.0	0.5	0.0
1.2	0.0	35.7	7.5	22.0	1.3	0.0	2.1	0.0
27.9	0.0	39.6	13.6	28.0	0.9	5.7	4.8	0.6
4.2	0.0	14.3	6.3	9.9	0.9	1.8	0.8	0.0
19.1	0.0	21.5	9.7	20.2	0.6	2.7	1.8	0.0
3.9	0.0	24.5	6.5	17.5	0.9	0.0	0.7	0.0
53.5	0.0	17.6	5.3	15.6	0.7	0.0	5.2	0.8
47.9	0.0	32.1	4.4	19.7	0.4	0.0	5.6	1.7
35.8	0.0	22.0	2.2	14.5	0.5	0.0	4.0	3.6
12.1	0.0	23.9	3.5	13.0	1.0	0.0	1.7	0.0
5.9	0.0	31.5	2.4	15.1	1.3	0.0	1.9	0.0
4.4	0.0	30.9	3.3	15.3	1.1	0.0	1.5	0.0
3.1	0.0	28.7	2.9	16.0	1.1	0.0	1.7	0.1
3.0	0.0	19.0	7.3	14.2	1.0	0.0	0.4	0.0
0.0	0.0	21.9	4.7	14.1	1.1	0.0	0.7	0.1
75.3	53.4	231.9	10.0	172.0	1.7	18.4	13.8	16.6
11.8	0.0	61.9	4.1	28.2	2.1	5.8	7.2	0.0
49.9	0.0	30.5	13.5	29.0	1.1	10.2	9.3	4.1
47.2	0.0	28.7	11.5	25.7	0.8	0.0	4.1	2.3
30.9	0.0	79.6	11.5	43.1	1.4	10.1	10.8	11.7
46.5	0.0	234.5	3.9	87.9	2.5	21.5	23.8	51.4
34.2	0.0	101.6	13.1	56.7	1.6	12.4	10.3	33.4
44.5	0.0	54.5	15.7	37.1	1.5	8.0	6.3	17.0
43.1	0.0	54.4	16.0	38.4	1.7	8.1	6.1	10.7
14.6	60.1	50.6	8.8	22.8	3.6	3.2	2.5	6.1
17.9	0.0	23.3	9.0	17.5	1.6	2.2	2.5	0.2
22.3	0.0	275.0	7.7	99.2	5.4	16.4	21.2	41.2
7.4	0.0	16.1	9.0	9.4	1.0	1.7	2.1	0.0
11.6	0.0	59.6	2.7	26.9	2.2	5.9	7.1	43.5
3.3	0.0	10.9	5.3	8.5	0.7	0.0	0.7	0.0
30.5	0.0	10.5	12.5	12.9	0.6	0.0	4.0	1.6
5.4	0.0	117.5	4.4	30.3	0.9	0.0	19.7	5.7
12.6	0.0	55.9	8.7	19.1	0.5	0.0	11.3	2.9
12.4	0.0	56.0	8.9	20.2	0.5	0.0	11.0	2.9
18.8	0.0	26.2	10.3	15.6	0.4	0.0	4.5	1.9
3.8	0.0	331.1	5.0	35.0	1.1	0.0	45.8	17.1
3.0	0.0	425.9	4.6	72.0	1.8	0.0	84.4	22.7
2.2	0.0	429.3	3.4	124.2	2.3	52.5	41.2	49.8
38.3	0.0	21.2	7.1	14.0	0.7	0.0	3.8	3.9
38.3	0.0	19.1	6.5	15.7	0.6	0.0	4.8	0.0
4.3	0.0	28.2	5.1	20.3	1.2	0.0	1.7	0.0
36.2	0.0	26.0	7.3	21.4	0.4	0.0	2.9	8.3
31.9	0.0	12.9	21.9	14.2	2.2	6.6	5.8	1.1
18.5	0.0	23.4	6.3	14.8	0.8	0.0	2.2	0.0
19.4	0.0	23.6	6.4	13.8	0.8	0.0	3.0	0.0
30.7	0.0	19.8	4.0	19.9	1.4	2.7	4.0	1.5
0.0	0.0	17.3	4.4	0.0	0.0	0.0	0.0	0.0
3.1	0.0	17.5	4.2	11.4	0.9	0.7	0.9	0.0
44.3	1.5	33.7	10.5	33.8	0.8	0.0	10.0	7.1
32.6	0.0	24.9	10.0	22.1	1.1	4.1	5.6	0.0
54.2	0.0	59.9	8.3	37.5	0.6	0.0	9.9	8.9
4.7	0.0	16.2	6.8	10.9	1.0	1.9	0.6	0.0
45.5	0.0	92.1	1.6	59.5	1.1	11.8	14.5	11.4
19.8	0.0	14.6	10.7	0.0	0.0	0.0	0.0	0.3
2.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4	1.5
2.1	0.0	9.4	7.7	7.9	0.8	1.3	1.3	0.0
1.3	0.0	49.0	17.4	33.8	0.9	3.2	1.9	0.0
2.1	0.0	11.5	9.7	7.9	0.7	1.2	1.2	0.0
1.9	0.0	0.0	6.5	0.7	1.3	1.1	1.1	0.0
1.9	0.0	0.0	7.2	0.9	1.7	1.5	1.5	0.0
1.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.9	0.0	15.5	8.2	11.6	0.9	2.3	1.4	0.0
3.2	0.0	10.4	19.2	9.0	1.0	1.4	1.0	0.0
2.7	0.0	9.8	8.6	7.1	2.7	2.3	2.0	0.0
2.7	0.0	52.5	8.4	34.6	0.8	1.4	0.9	0.0
2.7	0.0	29.0	4.3	16.2	1.7	1.0	1.7	0.1
2.8	0.0	19.5	12.2	13.5	2.4	1.0	0.8	0.0
0.0	0.0	9.1	9.4	8.3	3.6	1.2	1.1	0.2
3.4	0.0	12.6	10.6	0.0	0.0	0.0	0.0	0.0
124.2	29290.6	9384.3	55.1	6221.0	245.4	893.8	614.0	0.4
6.1	0.0	4.7	15.9	10.4	1.0	1.1	1.7	0.0
3.0	0.0	21.7	8.2	14.2	0.8	1.4	2.9	0.0
5.0	0.0	13.6	6.3	10.3	0.3	1.2	2.1	0.0
22.0	0.0	35.9	14.5	32.3	0.4	4.0	6.2	0.0
17.1	0.0	33.6	14.5	32.3	0.6	2.4	2.7	1.4
7.0	0.0	27.0	4.6	8.7	0.6	4.3	5.8	1.7
42.2	0.0	25.8	6.5	27.2	1.6	5.7	2.3	3.1
11.0	0.0	171.1	4.9	33.0	2.1	21.3	25.6	1.2
8.1	0.0	25.3	7.4	15.8	0.8	2.5	3.3	1.0
13.9	0.0	9.4	5.4	11.5	0.5	2.3	2.1	1.2
15.0	0.0	7.3	5.4	9.5	0.3	1.7	1.6	0.9
17.3	0.0	68.8	0.0	50.0	0.8	4.8	3.5	3.5

Physiologic Wall Sampling Summary				Updated 3/5/2000 SVK				NM- NS = not measured not sampled		BDA = below detection limit DND = did not detect						
Physiologic Wall Sampling Summary				Updated 3/5/2000 SVK				NM- NS = not measured not sampled		BDA = below detection limit DND = did not detect						
Sample Date	Sample ID	Barcode ID	pH	DO (mg/L)	Microbial Conductivity (uS/cm)	Cate Conductivity (uS/cm)	Net Charge	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	CT Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ²⁺ Conc. (mg/L)
3/18/2000	19	AD	6.1	10.93	420	377	6.8%	21.7	1.9	95.0	9.1	55.8	0.4	5.5	11.5	0.0
3/18/2000	20	AE	6.6	0.63	1149	1017	5.9%	23.4	1.4	120.9	1.5	167.1	2.6	23.2	23.0	0.0
3/18/2000	21	AF	6.6	2.60	237	281	6.5%	10.9	0.0	73.7	5.0	35.8	1.0	7.5	9.1	2.1
3/18/2000	22	AF	6.6	2.60	237	281	6.5%	10.9	0.0	74.4	5.2	35.7	1.0	7.5	9.1	2.1
3/18/2000	23	AG	6.6	2.94	359	392	-1.5%	23.6	2.8	88.1	2.2	60.5	1.9	5.5	4.5	1.7
3/18/2000	115	AI	6.6	1.89	372	294	3.5%	20.7	2.4	71.1	3.7	47.8	1.0	4.8	4.7	0.1
3/18/2000	21	AH	6.8	5.41	372	315	-6.8%	21.0	7.2	62.1	3.0	49.5	0.6	3.8	2.6	0.2
3/18/2000	24	AI	6.9	5.41	372	315	-6.8%	21.0	7.2	62.1	3.0	49.5	0.6	3.8	2.6	0.2
3/18/2000	25	AJ	6.6	10.64	105	165	5.3%	8.8	0.0	25.5	6.3	20.2	0.4	4.8	6.0	0.4
3/18/2000	26	AK	7.0	1.12	151	145	-2.7%	22.6	2.1	263.2	4.2	181.6	1.9	24.1	19.8	8.4
3/18/2000	27	AL	6.7	2.45	959	547	11.0%	59.4	1.3	81.6	10.0	51.6	0.8	2.9	3.0	0.1
3/18/2000	27	AL	6.7	8.35	425	415	2.3%	26.1	0.0	109.9	9.4	20.5	1.1	6.2	6.8	0.9
3/18/2000	28	AM	6.6	12.97	101	101	0.0%	30.9	1.9	35.0	8.2	36.7	1.1	15.3	14.6	0.5
3/18/2000	29	AN	6.7	3.37	324	302	0.6%	24.3	0.0	15.2	10.0	8.7	0.8	4.5	3.5	0.1
3/18/2000	31	AP	6.4	14.60	103	95	1.2%	9.0	1.9	14.9	9.3	6.6	0.8	4.9	4.0	0.2
3/18/2000	32	AQ	6.8	14.60	103	95	1.2%	9.0	1.9	14.9	9.3	6.6	0.8	4.9	4.0	0.2
3/18/2000	33	AQ	6.8	14.60	103	95	1.2%	9.0	1.9	14.9	9.3	6.6	0.8	4.9	4.0	0.2
3/18/2000	35	AR	5.4	5.85	145	122	1.9%	2.6	2.8	20.0	2.0	298.4	3.0	168.3	1.7	17.2
3/18/2000	35	AR	5.4	5.85	145	122	1.9%	2.6	2.8	20.0	2.0	298.4	3.0	168.3	1.7	17.2
3/18/2000	35	AS	0.0	0.75	1039	945	10.6%	16.5	14.1	5.2	11.8	1.1	2.1	2.0	19.1	0.0
3/18/2000	36	AT	6.8	1.04	1229	92	3.3%	13.8	1.0	19.2	3.2	37.5	2.2	16.3	13.2	0.0
3/18/2000	37	AU	6.4	1.25	77	87	3.8%	19.2	2.1	13.6	5.3	10.3	1.0	1.7	3.4	0.0
3/18/2000	38	AV	7.7	1.60	83	82	-13.1%	6.6	1.3	17.5	4.6	11.0	1.4	11.0	16.5	0.0
3/18/2000	39	AX	6.1	13.18	102	91	4.5%	7.3	1.7	197.2	6.9	4.9	1.3	1.4	1.4	0.0
3/18/2000	40	AY	5.9	8.39	407	349	6.7%	2.5	1.8	12.						

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Typical Well Sampling Summary					Updated		38519.0		SVK		NS -		not measured		BOL - data detection limit	
							DND = add not detected						if listed as below 1, rounded to 1, otherwise detection limit			
Sample Date	Sample ID	Borehole ID	pH	DO (mg/L)	Measured Conductivity (µS/cm)	Cable Conductivity (µS/cm)	Net Charge	ICO ₂ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ³⁺ Conc. (mg/L)
10/24/2003	56	BOC	6.9	1.82	495	375	4.3%	76.5	0.1	79.1	0.9	62.1	1.3	9.0	7.7	3.4
10/24/2003	57	BOC	6.9	0.66	452	416	-0.8%	39.1	0.2	111.2	5.5	45.5	0.9	14.9	13.4	NS
10/24/2003	58	BOC	6.9	1.47	521	491	0.8%	49.3	0.1	130.8	1.8	67.4	1.1	16.9	10.4	6.4
10/24/2003	59	BOC	6.8	0.64	439	499	-2.3%	38.9	0.1	109.0	5.4	52.4	1.4	8.8	8.1	NS
10/24/2003	44	OTJ	6.1	1.73	131	122	1.5%	8.3	0.1	24.4	3.9	18.1	1.2	2.8	3.4	3.4
10/24/2003	45	OTJ	6.1	0.92	122	122	1.5%	8.3	0.1	24.4	3.9	18.1	1.2	2.8	3.4	3.4
10/24/2003	29	HH	6.4	0.76	655	592	3.6%	65.7	0.2	149.2	9.7	102.3	1.5	13.1	9.1	4.8
10/24/2003	23	HE	6.4	2.89	116	116	1.7%	11.5	0.2	36.5	6.3	24.2	1.1	2.9	2.1	BDL
10/24/2003	41	HE	6.1	3.59	74	74	1.0%	10.7	0.1	13.0	7.9	15.1	0.8	0.7	0.5	BDL
10/24/2003	42	HE	6.1	3.09	74	74	1.0%	10.7	0.1	14.2	9.2	13.3	0.8	1.3	0.9	BDL
10/24/2003	18	HE	6.1	0.70	85	85	3.3%	5.9	0.1	101.4	5.4	75.6	1.8	7.4	9.9	BDL
10/24/2003	47	HH	5.7	0.69	79	65	2.3%	3.2	0.2	12.9	0.3	63.7	0.4	1.8	0.9	BDL
10/24/2003	46	BI	5.6	6.25	355	243	4.0%	9.5	0.2	100.1	4.6	53.6	2.0	6.7	2.8	BDL
10/24/2003	28	BJ	5.9	1.19	394	353	4.0%	9.5	0.2	100.1	4.6	53.6	2.0	6.7	2.8	BDL
10/24/2003	24	HK	5.6	5.65	69	69	6.3%	3.4	0.4	13.7	5.1	11.4	0.8	0.9	0.8	BDL
10/24/2003	25	HK	6.4	0.50	153	153	12.5%	20.7	0.2	22.9	5.6	27.0	0.6	1.7	1.9	BDL
10/24/2003	33	HK	6.2	1.00	82	79	1.5%	5.9	0.2	14.1	8.6	15.8	0.8	0.8	0.8	BDL
10/24/2003	31	BLA	6.6	0.78	495	456	0.5%	45.0	0.3	116.5	12.1	63.9	2.1	11.1	9.0	15.4
10/24/2003	72	BLA	6.7	0.58	435	400	2.4%	41.8	0.3	119.5	7.5	63.5	1.5	7.5	7.1	BDL
10/24/2003	73	BLA	6.1	5.10	449	414	0.6%	15.8	0.3	94.1	2.5	48.4	2.3	6.7	5.4	BDL
10/24/2003	74	BLA	5.6	5.28	327	317	0.5%	5.3	0.3	65.4	2.7	30.9	1.8	5.1	4.7	BDL
10/24/2003	75	BLA	5.6	5.38	243	229	1.4%	4.2	-0.3	42.7	5.2	25.5	1.7	2.7	2.6	BDL
10/24/2003	76	BLA	5.6	4.57	174	167	2.8%	6.1	-0.3	28.7	5.2	25.5	1.7	2.7	2.6	BDL
10/24/2003	77	BLA	5.6	4.57	133	135	2.7%	6.9	0.1	28.8	7.0	21.2	1.3	1.4	1.3	BDL
10/24/2003	78	BLA	5.6	4.57	149	149	1.2%	5.9	0							

Dynamics Well Sampling Summary				Updated		3/25/19		SVK		NM - NS		not measured not sampled		BDL = below detection limit DND = did not detect (Reported as 0; below 1, rounded; all above detection limit)	
Sample Date	Sample ID	Borehole ID	DO pH	Measured Conductivity (mS/cm)	Cate Conductivity (mS/cm)	Net Charge	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ³⁺ Conc. (mg/L)
6/12/2004	92	CU	6.5	0.45	443	NA	NS	19.3	47.3	9.9	68.1	1.1	7.6	8.4	8.1
6/12/2004	103	East Weir	6.7	0.7	450	335	106.1	0.6	65.6	1.1	61.8	4.4	16.6	8.0	2.3
6/12/2004	1	TranA block 1	8.4	NSM	44	2	232.5	BDL	0.4	0.2	0.7	0.0	0.0	0.0	0.0
6/12/2004	73	TranB block 1	7.3	NSM	4	2	43.5%	BDL	0.3	0.2	0.7	0.0	0.0	0.0	BDL
6/12/2004	27	ST	6.9	6.22	165	109	-2.1%	17.5	0.3	35.6	6.5	1.1	1.0	2.6	3.3
6/12/2004	NS	U1R01	NSM	NSM	NSM	NA	NA	NS	NS	NS	NS	NS	NS	NS	NS
6/12/2004	NS	U1R02	NSM	NSM	NSM	NA	NA	NS	NS	NS	NS	NS	NS	NS	NS
6/12/2004	12	U2R01	6.0	11.92	756	694	-0.1%	2.6	0.2	21.6	5.0	12.1	1.8	11.4	4.4
6/22/2004	11	U2R05	6.6	10.19	165	154	-1.0%	7.3	0.4	4.2	4.3	2.4	0.9	2.4	1.4
6/22/2004	7	U2R03	6.2	10.47	35	57	-12.6%	BDL	0.7	9.8	5.2	7.4	0.7	8.3	6.6
6/22/2004	8	U2R04	7.5	10.19	60	59	-3.8%	9.0	0.4	10.7	4.3	7.7	1.0	9.7	8.8
6/22/2004	9	U2R05	6.9	6.81	120	114	-5.8%	21.1	0.2	22.2	4.5	12.3	1.0	2.9	3.1
6/22/2004	10	U2R05	6.9	6.81	120	113	-2.1%	22.9	0.2	21.8	4.5	12.3	1.0	2.9	3.1
6/22/2004	NS	U2C01	NSM	NSM	NSM	NA	NA	NS	NS	NS	NS	NS	NS	NS	NS
6/22/2004	NS	U2C02	NSM	NSM	NSM	NA	NA	NS	NS	NS	NS	NS	NS	NS	NS
6/22/2004	4	U2C03	6.0	9.85	650	631	-0.4%	4.7	1.0	16.2	5.0	111.6	2.4	8.9	4.6
6/22/2004	3	U2C02	6.5	10.24	254	237	-2.0%	9.1	0.9	67.7	3.9	42.0	1.7	2.1	1.2
6/22/2004	2	U2C03	7.1	9.23	105	104	-0.5%	13.6	0.5	22.1	4.7	14.2	3.3	1.2	6.9
6/22/2004	6	U2C04	6.1	9.00	125	120	-0.4%	5.9	0.6	22.2	4.7	14.2	3.3	1.2	6.9
6/22/2004	5	U2C05	6.9	7.16	120	102	-16.3%	28.9	0.7	11.3	12.6	9.4	5.0	1.8	1.8
6/22/2004	59	West Weir	6.5	1.95	700	684	-2.3%	49.0	1.4	155.5	7.3	117.4	2.4	12.9	4.4
6/22/2004	90	West Weir	6.5	2.95	700	559	-5.1%	58.3	1.6	156.4	7.2	115.7	2.4	13.4	4.6
7/13/2004	70	AA	NSM	NSM	NSM	NS	NS	NS	NS	NS	0.0	0.0	0.0	0.0	NS
7/13/2004	71	AB	6.7	8.10	316	NA	NA	NS	NS	NS	41.9	1.8	5.7	6.9	BDL
7/13/2004	72	AC	6.8	10.82	248	224	-9.3%	33.4	0.3	22.3	2.9	69.7	1.3	4.8	5.8
7/13/2004	105	AD	6.3	6.58	415	107	34.5%	34.5	0.3	28.4	4.9	65.8	1.2	4.9	5.7
7/13/2004	45	AE	6.3	0.69	437	218	-2.2%	56.5	0.3	94.4	5.4	82.6	0.7	1.6	1.0
7/13/2004	61														

Physio-Wet Sampling Summary

Phynessa Well Sampling Summary								Updated	38519.0	SVK	NM - NS	not measured not sampled		BDL = below detection limit DND = did not detect If listed as 0, below L, rounded, but above detection limit					
Sample Date	Sample ID	Batchcode ID	pH	DO (mg/L)	Measured Conductivity (mS/cm)	Calc Conductivity (mS/cm)	Net Charge	HCO ₃ ⁻ Conc. (mg/L)	Acetate Conc. (mg/L)	Cl ⁻ Conc. (mg/L)	SO ₄ ²⁻ Conc. (mg/L)	Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Fe ²⁺ Conc. (mg/L)			
9/23/2024	64	BTc	6.8	0.24	478	NA	NA	56.5	0.4	151.9	0.5	BDL	BDL	BDL	BDL	2.0			
9/23/2024	97	BTd	6.6	0.22	63	560	4.4%	63.0	0.3	144.9	0.9	107.1	1.0	7.5	7.1	3.2			
9/23/2024	65	BTd	7.0	0.22	332	482	1.9%	39.3	1.0	110.9	3.2	55.9	1.0	5.0	5.1	2.7			
9/23/2024	66	BTd	7.0	0.22	332	489	1.3%	39.6	0.5	111.2	3.3	51.8	1.0	5.3	5.3	2.6			
9/23/2024	63	BTf	6.6	0.23	844	738	2.0%	117.6	0.6	183.2	2.3	142.9	1.4	9.8	18.2	5.1			
9/23/2024	57	BTg	6.6	0.23	1682	214	1.5%	125.0	0.3	255.9	0.8	172.7	1.7	16.0	15.7	7.1			
9/23/2024	58	BTg	6.7	0.23	435	367	5.9%	79.1	0.6	71.1	5.8	71.8	0.8	3.5	3.5	1.8			
9/23/2024	59	BTg	7.1	0.31	157	137	-9.9%	38.5	0.3	24.0	0.9	18.1	0.3	3.1	3.6	6.4			
9/23/2024	59	BTj	7.0	0.33	320	297	1.0%	53.9	0.2	63.5	4.2	35.9	0.5	3.1	2.8	4.6			
9/23/2024	dy	BTk	NM	NM	NM	NM	NM	NS	NS	NS	NS	0.0	0.0	0.0	0.0	NS			
9/23/2024	57	BU	6.4	0.85	928	817	0.6%	75.7	0.3	241.2	0.7	157.5	1.4	12.7	7.9	BDL			
9/23/2024	32	BX	7.2	0.54	116	235	60.3%	35.3	0.6	11.2	3.9	66.7	1.3	9.9	6.6	1.3			
9/23/2024	79	BY	6.8	1.07	130	111	1.6%	39.6	0.7	13.5	7.5	18.6	0.7	1.8	2.0	BDL			
9/23/2024	55	BZ	6.9	1.44	330	319	-0.8%	44.6	0.3	79.6	6.1	51.4	1.1	4.4	4.0	6.8			
9/23/2024	65	CA	7.0	6.87	270	289	-0.5%	54.6	1.4	43.6	17.5	48.8	1.9	2.7	3.3	BDL			
9/23/2024	56	CB	6.4	2.39	289	289	1.1%	21.7	0.4	71.4	7.6	49.9	1.3	7.3	2.7	BDL			
9/23/2024	70	CC	6.9	5.22	89	84	-9.1%	15.7	0.7	19.8	4.1	12.1	1.0	1.4	1.3	BDL			
9/23/2024	67	CD	6.9	1.58	423	335	-1.5%	63.6	0.3	84.5	10.4	65.8	1.2	4.9	4.9	8.7			
9/23/2024	dy	East Wick	NM	NM	NM	NM	NM	NS	NS	NS	NS	0.0	0.0	0.0	0.0	NS			
9/23/2024	1	Field Block I	8.2	NM	15	33	-4.1%	BDL	0.5	5.2	0.3	2.7	1.1	0.1	0.0	BDL			
9/23/2024	28	ST	6.3	2.40	581	534	0.1%	25.6	0.5	156.1	8.2	89.8	2.5	7.6	8.0	BDL			
9/23/2024	dy	UB191	NM	NM	NM	NM	NM	NS	NS	NS	NS	0.0	0.0	0.0	0.0	NS			
9/23/2024	15	UB192	5.7	10.65	33	49	2.5%	3.0	0.5	7.7	6.0	7.7	0.9	0.6	0.4	BDL			
9/23/2024	9	UB191	5.1	10.74	433	394	1.3%	0.7	0.3	119.0	6.4	73.3	1.3	4.3	1.7	BDL			
9/23/2024	7	UB193	5.4	10.31	179	163	1.5%	1.5	0.4	43.9	4.8	21.0	1.2	2.1	1.2	BDL			
9/23/2024	4	UB203	5.7	9.61	61	54	5.3%	1.9	0.6	10.2	4.9	8.2	1.0	0.8	0.6	BDL			
9/23/2024	10	UB204	5.6	9.31	65	NA	NA	1.9	NS	NS	NS	8.3	0.8	1.0	0.8	BDL			
9/23/2024	11	UB204	5.6	9.31	65	52	5.3%	1.7	0.4	11.1	4.4	6.7	0.8	1.5	1.2	BDL			
9/23/2024	12	UB205	5.4	7.65	170	101	9.1%	2.6	0.8	22.6	4.6	17.6	1.9	2.4	2.5	BDL			
9/23/2024	13	UC191	5.7	10.49	36	32	7.3%	BDL	0.5	9.2	6.8	8.1	0.9	0.7	0.6	BDL			
9/23/2024	14	UC192	5.6	9.59	54	48	6.6%	2.5	0.4	6.3	6.4	6.5	1.9	0.9	0.6	BDL			
9/23/2024	3	UC201	6.9	10.00	499	478	2.6%	10.3	0.3	123.4	8.1	83.6	1.6	4.1	2.0	BDL			
9/23/2024	2	UC202	7.2	9.65	159	149	-4.3%	12.7	0.3	31.8	8.2	24.3	1.4	0.6	0.4	BDL			
9/23/2024	4	UC203	6.8	8.60	89	83	-12.9%	18.7	0.3	13.2	5.5	9.6	3.2	1.1	0.8	BDL			
9/23/2024	5	UC204	6.6	9.85	84	80	-5.8%	15.8	0.4	11.7	8.9	9.1	4.9	0.8	0.7	BDL			
9/23/2024	6	UC205	6.3	6.24	101	91	-9.8%	19.6	0.3	10.4	12.3	9.3	5.0	1.9	1.8	BDL			
9/23/2024	45	West Wick	6.8	7.07	176	151	4.1%	43.1	0.3	22.4	5.3	19.8	0.9	9.6	2.0	0.8			

APPENDIX C
November 2002 – September 2004 PCP Data

AT pep	Point Location (m nstl)										
number	A	B	C	D	E	F	G	H	I	J	K
Date	1	2	3	4	5	6	7	8	9	10	11
11/12/2002	394	1881	185	18447	131	122	123	131	126	127	214
12/17/2002	232	2362	272	18490	120	127	144	152	144	142	156
1/21/2003	775	2532	294	20074	126	132	139	168	123	119	152
2/20/2003	304	2866	276	19711	477	133	144	131	125	27	95
3/10/2003	698	3220	11968	18896	1701	1886	793	215	129	98	118
3/18/2003	320	2708	1107	19211	790	196	162	144	107	93	132
5/21/2003	4831	3200	251	205	196	166	162	150	118	94	125
6/15/2003	898	6696	1611	20581	629	516	395	171	99	111	111
6/15/2003	521	7114	1835	22765	1202	714	199	170	102	118	132
7/11/2003	1349	6462	926	25116	1293	446	145	143	127	141	136
7/10/2003	1186	5472	949	23748	279	189	129	139	122	124	130
7/16/2003	1204	5392	536	23119	269	130	126	137	123	117	131
7/20/2003	988	5663	441	22373	195	121	131	181	115	112	128
7/29/2003	714	2784	638	20957	504	119	128	186	101	101	128
8/26/2003	677	3619	896	19213	483	582	541	302	109	101	98
9/18/2003	816	3101	517	15800	529	420	482	166	116	92	98
10/16/2003	440	2726	435	14377	617	340	183	168	146	90	82
10/30/2003	249	2688	696	14718	442	281	172	173	126	96	73
11/11/2003	333	1840	272	15883	196	115	98	130	163	92	84
12/4/2003	246	2172	189	17391	91	103	114	130	119	73	80
12/18/2003	258	2167	281	18084	91	86	104	117	127	84	84
1/6/2004	273	2196	214	16954	85	105	100	136	107	75	79
1/23/2004	14990	24681	218	17511	90	91	124	176	122	98	94
2/11/2004	6860	4292	590	16927	137	109	124	176	122	98	94
2/8/2004	2099	1844	233	8646	86	96	105	145	65	47	61
2/16/2004	13332	10051	973	18538	1130	948	123	152	116	78	121
2/29/2004	5130	2939	534	18553	453	140	142	163	102	102	99
3/12/2004	2560	2800	465	19011	230	140	127	172	109	100	103
3/12/2004	3182	2724	347	18751	221	135	125	165	103	91	104
3/21/2004	2305	2274	259	19058	172	133	172	163	106	97	109
3/30/2004	863	2418	216	17353	141	112	115	151	91	85	80
4/4/2004	522	2653	253	19105	165	123	124	170	108	93	88
4/10/2004	682	2857	270	19000	169	128	135	188	111	99	99
4/20/2004	1008	2957	460	2061	203	94	110	498	71	74	67
4/30/2004	902	5440	1773	21823	223	1298	1857	716	118	102	106
5/9/2004	648	5440	1032	22084	256	1291	2075	331	129	134	242
5/16/2004	777	6156	1822	25807	601	2543	3696	241	118	104	194
5/25/2004	1097	8866	2178	2695	566	4229	2460	153	118	102	110
5/30/2004	656	5361	1032	26542	664	1987	2704	144	111	104	112
6/14/2004	1926	5630	690	27221	392	1794	1281	137	110	107	103
6/22/2004	1792	7182	571	29175	583	412	564	136	126	130	109
7/1/2004	1056	3140	423	25769	252	250	189	111	126	147	99
7/13/2004	1016	473	488	26011	267	236	207	113	132	153	99
7/19/2004	1051	2857	349	24039	247	235	204	116	141	163	96
7/28/2004	846	2783	479	23809	228	220	198	115	157	138	93
8/3/2004	1037	2865	612	26755	247	251	217	161	180	133	109
8/12/2004	1173	2699	462	22522	312	224	187	316	178	113	93
8/20/2004	675	5919	646	21105	4221	219	192	145	159	117	91
9/3/2004	1435	5064	844	28697	287	1139	844	346	591	156	106
9/19/2004	502	3139	656	19072	567	426	211	409	186	109	97
10/9/2004	1078	3012	5154	18261	549	692	536	418	234	108	107
10/26/2004	772	3233	593	16125	544	462	444	418	225	111	107
11/6/2004	512	2634	428	17738	382	424	386	376	161	91	81
11/11/2004	670	2515	267	17738	433	357	248	306	122	88	90
11/21/2004	383	2101	269	17240	154	216	206	195	153	92	72
12/11/2004	323	2229	2984	19306	204	184	140	136	154	154	125
12/20/2004	433	2328	278	20607	225	170	175	143	151	182	166

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number	1	2	3	4	5	6	7	8	9	10	11
Date	Point Location (in msl)										
11/12/2002	67	194	375	407	383	276	392	119	155	136	259
12/18/2002	n/a	86	169	147	185	956	143	889	87	139	971
1/21/2003	454	200	2059	2409	1893	1749	1994	1506	1814	2748	771
2/20/2003	1284	3115	3602	48	1787	3026	480	185	280	237	3718
3/10/2003	1118	3864	1701	283	2583	3650	2074	2146	4304	6148	4094
3/18/2003	9248	5945	5861	640	1990	1660	989	1900	3115	2992	367
4/23/2003	1380	413	610	892	5239	2922	1522	1022	853	1239	367
5/21/2003	1763	5255	7181	8404	3740	433	659	169	212	150	187
6/3/2003	1466	4758	2908	676	424	1219	652	200	180	140	172
6/15/2003	1695	2597	697	367	1171	542	787	703	192	123	182
7/10/2003	771	790	2408	1404	2512	2602	2668	2378	327	120	181
7/16/2003	760	1710	2108	1397	1184	2095	1537	233	173	108	179
7/20/2003	572	2022	1273	1292	1496	1166	664	199	158	110	196
7/29/2003	359	1233	1085	1356	1176	1277	522	194	142	101	196
8/26/2003	298	965	1172	1670	655	452	480	176	117	98	183
9/12/2003	731	992	466	1141	260	245	246	129	98	105	172
9/18/2003	654	582	416	389	270	232	429	308	108	102	174
10/16/2003	353	846	632	293	265	273	542	363	304	98	172
10/30/2003	798	1254	1088	442	393	283	458	165	123	138	189
11/1/2003	582	994	803	627	608	562	572	196	123	135	192
12/4/2003	444	812	761	767	757	373	862	174	142	122	183
12/11/2003	528	501	278	449	454	344	936	169	149	135	221
1/6/2004	966	289	168	339	511	345	980	128	142	137	223
1/23/2004	373	191	2306	339	4249	5240	4107	4729	1787	2282	709
2/1/2004	466	4214	2678	4086	1514	610	1029	185	173	178	709
2/8/2004	1239	3689	4076	3459	865	331	871	260	112	117	160
2/8/2004	1265	3769	4128	3476	869	326	851	257	110	116	222
2/16/2004	1604	6330	5908	6541	5064	8018	4220	5486	8018	169	233
2/29/2004	1973	3069	1973	4315	7300	4828	8820	5418	8428	10233	9029
3/7/2004	1339	2442	3718	5840	6035	6354	6977	3933	3631	4841	9101
3/12/2004	1626	2923	4293	1752	2606	3337	2023	4586	3964	4258	2829
3/21/2004	1467	4293	1484	1524	1549	3074	3631	3631	1901	1240	6115
3/30/2004	897	33121	1524	1178	3483	3074	3708	3399	3026	1577	3042
4/4/2004	653	3696	1554	1178	1178	2894	2202	2582	3699	4327	3418
4/10/2004	818	2325	1706	1267	5700	5039	3769	2804	4971	5836	7033
4/20/2004	2083	5376	2955	4186	5700	5039	3769	2804	4971	5836	7033
5/16/2004	2461	22572	2353	3751	1352	887	1089	1172	1445	1383	3312
5/25/2004	1846	2565	1436	3085	460	423	949	261	222	195	419
5/30/2004	1772	1398	1862	2739	489	464	879	261	222	195	419
6/4/2004	1967	1126	1725	1626	392	365	876	281	224	186	317
6/14/2004	1460	1231	1284	1131	1836	446	1128	392	246	203	336
6/22/2004	1298	1500	1145	1171	988	616	1685	504	248	198	340
7/1/2004	880	1470	916	1145	2017	823	1685	1177	733	154	264
7/13/2004	1111	1521	1256	867	2449	1955	2553	1738	608	178	282
7/19/2004	1483	1461	1397	813	2439	1524	2244	2207	212	202	295
7/28/2004	1128	1441	1778	2484	1656	1356	925	270	226	210	275
8/3/2004	1098	1302	1632	2538	823	814	790	212	234	209	260
8/12/2004	1173	1080	1156	1954	664	447	839	217	228	205	262
8/20/2004	1115	1122	1239	974	1136	445	1022	207	214	195	279
9/3/2004	183	536	819	882	912	1122	1562	937	197	180	246
9/19/2004	335	177	371	342	1133	1138	1144	339	226	264	512
10/9/2004	32	230	380	1090	686	1053	1638	867	571	454	282
10/26/2004	744	162	323	860	870	925	6	334	450	608	357
11/6/2004	783	145	375	430	654	484	713	405	459	340	246
11/1/2004	698	131	560	734	677	494	717	529	367	295	300
11/21/2004	915	108	753	754	600	570	1000	459	392	333	259
12/1/2004	851	154	271	761	3569	572	774	318	268	196	256
12/26/2004	680	284	333	446	731	567	815	287	241	182	307

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Date	Point Location (mmsl)										
	7	6	5	5	4	4	3	2	2	1	-1
11/12/2002	n/a	1223	804	543	383	276	560	511	517	130	144
12/18/2002	n/a	1223	1406	1632	1251	1912	1931	2528	2387	2556	186
1/21/2003	487	1532	1235	1835	516	344	462	348	644	179	212
2/20/2003	1690	374	1231	1613	1430	424	420	1075	596	145	160
3/10/2003	1327	386	882	756	567	487	549	736	922	1045	496
3/18/2003	1103	310	847	832	632	461	587	810	872	1512	630
4/23/2003	3796	5505	5424	2279	3602	1948	2072	1437	1168	248	183
5/21/2003	11709	438	1209	1732	2346	1366	2091	743	782	163	117
6/3/2003	1399	2820	1508	1743	1750	2855	4631	2532	1387	487	140
6/15/2003	716	1494	4404	2569	3658	2529	2147	2108	1741	167	157
7/1/2003	642	1364	1816	3029	3509	3420	3187	1390	1672	162	162
7/10/2003	791	1231	2284	3842	3830	3353	1257	696	780	134	124
7/20/2003	843	1719	2915	3298	3264	1878	1129	583	755	131	124
7/29/2003	1078	1799	3186	3051	2957	766	1273	569	674	128	128
8/26/2003	1346	1619	2963	2338	2030	817	480	1107	519	111	118
9/2/2003	600	1021	1931	1261	1328	1594	1107	1171	474	157	114
9/18/2003	653	1048	1931	1467	1231	1070	1165	1110	587	143	118
10/6/2003	110	600	1468	1548	1122	793	1023	1392	791	246	123
10/30/2003	127	97	545	545	498	901	1030	985	468	300	182
11/11/2003	178	600	1468	1548	1122	793	1030	1329	731	301	167
11/12/2003	178	97	544	657	1007	774	747	1179	652	245	161
12/4/2003	109	1137	556	1094	738	574	410	474	456	135	172
12/18/2003	1159	2254	2244	6782	4827	2012	519	467	355	149	151
1/6/2004	808	2369	4780	11868	9064	640	352	414	357	120	146
1/23/2004	8994	4214	5240	1576	815	335	278	448	280	136	177
2/1/2004	7889	889	2359	1751	582	364	1815	478	387	154	153
2/8/2004	1961	2797	5327	1729	1182	1625	901	148	141	85	99
2/16/2004	1616	1319	1769	2028	8751	1897	2053	3219	3465	2259	1938
2/29/2004	5524	1437	5240	10950	8751	2464	3319	8127	5117	3311	5117
3/7/2004	2462	1107	1704	3621	635	940	726	1634	4256	231	1365
3/12/2004	16762	2823	1832	4304	1931	889	520	518	1460	207	205
3/21/2004	4191	18164	11369	11066	10117	9101	696	424	815	333	175
3/30/2004	4831	1590	1143	868	523	935	6051	393	728	189	148
4/4/2004	653	1983	3562	3821	3800	1137	2472	2720	5268	1932	170
4/10/2004	1125	864	2769	3483	1504	3363	3986	6763	7397	2163	2113
4/20/2004	1176	2218	1708	2222	1173	756	565	561	1740	247	1529
4/30/2004	1069	952	2864	2932	1149	760	576	651	1215	198	162
5/9/2004	1166	1360	2408	2761	1627	678	790	608	1074	192	152
5/16/2004	1392	1231	2102	1909	1980	1189	874	894	1246	487	296
5/25/2004	1772	921	1546	4255	4596	2467	3162	1253	2650	1763	1437
5/30/2004	1281	1240	1823	1711	4540	2815	3177	3234	2700	3203	230
6/4/2004	861	1259	2726	2510	4282	3255	2224	2401	2718	2890	296
6/14/2004	1305	1881	4995	4376	5106	2161	2820	2640	2312	2283	197
6/22/2004	1792	1910	4295	4390	3000	1026	1651	1549	1896	316	155
7/1/2004	1173	902	2115	2756	1080	757	539	623	1048	203	127
7/13/2004	1588	811	1849	1842	1116	607	552	496	1074	192	141
7/19/2004	989	1262	1607	1414	919	530	544	385	1025	184	135
7/28/2004	1441	1113	1163	1509	755	521	494	356	1119	212	171
8/3/2004	1098	586	1462	1524	797	543	517	316	991	192	149
8/12/2004	616	1143	1255	1524	797	543	517	316	991	192	149
8/20/2004	111	187	1227	1688	1169	1175	1022	581	974	208	117
9/3/2004	343	357	394	700	1247	1558	1031	968	1107	367	115
9/19/2004	112	143	1139	683	680	973	1084	1284	929	546	228
10/9/2004	105	104	705	954	659	1023	1072	578	1141	681	242
10/26/2004	343	162	808	1881	1360	979	1167	835	1350	359	185
11/6/2004	114	210	803	914	1145	1029	772	578	1147	425	308
11/11/2004	167	198	1441	1795	866	824	607	446	961	413	480
11/21/2004	429	43	140	216	191	222	82	17	290	19	28
12/11/2004	141	143	515	680	302	421	417	693	911	337	156
12/20/2004	105	165	667	835	506	830	1106	688	1147	363	246

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Date	Point Location (in msl)										
	7	5	3	2	1	1	0	0	-1	-3	-4
11/12/2002	--	--	--	--	219	387	448	284	287	296	301
12/18/2002	--	--	--	--	251	193	222	157	244	250	242
1/21/2003	--	--	--	--	1434	1377	1734	1854	585	358	243
2/20/2003	135	374	2101	2628	2085	2299	1861	1971	2055	1126	210
3/10/2003	112	1739	1890	630	290	547	--	1656	430	430	186
3/18/2003	--	1750	1954	640	237	135	19	1122	305	265	227
4/23/2003	1587	1583	1119	991	753	1266	680	1277	1579	1301	1590
5/21/2003	847	420	596	2264	2159	999	1350	1098	3001	3316	3427
6/3/2003	949	1163	4308	1352	1237	1776	1852	2415	2576	5357	2427
6/15/2003	684	3913	2202	1835	5488	5419	1432	5341	1010	5797	3633
7/1/2003	1252	2136	1834	1847	1404	2825	2890	3439	1018	2538	1364
7/10/2003	1065	1642	1265	2061	1671	1641	1432	1915	1356	470	308
7/16/2003	903	1382	1273	1564	1700	1360	1329	1681	1372	757	182
7/20/2003	749	933	1356	1525	1411	1469	1567	1139	1752	439	162
8/26/2003	936	894	1758	1244	1375	1413	1761	1140	1393	202	138
9/2/2003	327	642	1404	1681	1811	1104	1353	1295	1454	1598	191
9/18/2003	272	564	1150	878	294	795	552	678	742	180	170
10/16/2003	385	545	789	553	393	198	301	175	207	197	160
10/30/2003	554	538	803	709	332	337	286	231	585	301	182
11/1/2003	417	568	653	548	420	315	402	442	282	177	123
12/4/2003	264	223	639	617	653	373	293	178	238	245	120
12/18/2003	212	520	785	509	341	345	346	233	236	239	181
1/6/2004	217	260	309	509	238	239	264	177	256	276	152
1/23/2004	147	154	210	700	524	262	297	215	1430	290	142
2/1/2004	178	159	242	1167	1718	455	938	1374	804	533	118
2/8/2004	114	148	902	1960	2421	1655	2852	1241	1265	761	119
2/16/2004	63	151	2418	869	927	771	528	527	1220	246	170
2/29/2004	122	456	2281	3042	2324	5779	664	662	331	271	132
3/7/2004	123	438	2727	634	1240	758	484	260	284	255	137
3/12/2004	138	498	2779	1998	429	133	294	198	268	213	119
3/21/3/004	164	330	1042	1230	399	133	242	142	211	115	66
4/4/2004	166	1192	1746	1735	430	754	303	188	1668	304	1233
4/10/2004	46	1411	1425	2229	1932	1691	1082	618	1859	654	3086
4/20/2004	198	797	966	1963	2882	3669	705	1721	2959	5254	3045
4/30/2004	175	840	1642	2862	3800	3779	4397	4362	3107	6164	3058
5/9/2004	127	884	3001	3751	2974	3483	4483	4558	6239	6257	4968
5/16/2004	246	1258	2683	5176	3461	4197	3952	3718	5100	5831	2761
5/25/2004	253	1910	3514	5303	3889	4293	4368	4128	4845	6964	5287
5/30/2004	294	1876	2649	3248	3492	2418	3718	3062	3080	5223	5239
6/4/2/004	307	1524	2346	2828	2890	3255	4718	3773	2890	2890	2030
6/14/2004	214	1676	2426	2808	2699	2195	3877	4638	2746	2682	1203
6/22/2004	235	818	1360	2561	2122	1915	1195	3601	3647	2789	1330
7/1/2004	1056	5679	1692	1145	303	217	1011	1661	4540	349	204
7/13/2004	1143	744	1082	578	277	249	897	245	358	306	204
7/19/2004	1051	797	978	990	424	258	476	231	311	277	199
7/28/2004	1034	982	923	897	621	387	330	237	280	265	186
8/3/2/004	976	1107	714	1132	823	781	329	292	441	171	178
8/12/2004	1115	1048	826	1358	1594	671	484	659	859	242	172
8/20/2004	880	872	904	1461	1688	699	575	420	942	214	162
9/3/2004	744	685	1183	912	760	305	375	656	369	336	364
9/19/2004	614	742	799	769	623	1125	1565	1197	987	1437	1309
10/9/2004	129	257	543	818	741	965	12	693	856	312	211
10/26/2004	515	269	323	860	870	925	6	334	450	608	357
11/6/2004	277	177	669	753	709	726	683	405	315	397	252
11/11/2004	307	187	427	1033	812	631	6	362	339	442	240
11/21/2004	343	216	376	339	698	781	9	516	511	583	184
12/11/2004	258	187	233	707	659	542	298	405	512	421	234
12/20/2004	309	170	256	613	450	510	na	344	483	484	246

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Date	6	5	3	1	1	0	0	-1	-2	-3	-5
11/12/2002	506	269	590	597	301	304	280	227	201	207	181
12/18/2002	263	191	196	326	301	276	222	169	159	163	124
1/21/2003	354	333	253	229	184	172	162	151	170	167	182
2/20/2003	270	249	300	179	238	182	300	299	357	237	237
3/18/2003	1718	1587	3322	421	417	352	245	146	160	104	99
4/23/2003	1518	310	467	528	720	584	486	479	442	465	703
5/21/2003	1359	823	788	686	1799	5571	1301	1324	1421	521	779
6/3/2003	383	493	467	4624	5303	5571	2607	3131	2180	3020	5109
6/15/2003	521	213	3009	6239	2927	4335	4653	1757	1741	4774	3963
7/1/2003	803	2980	852	2216	2955	1933	2038	988	982	197	218
7/10/2003	1095	250	387	203	279	311	325	275	217	196	166
7/16/2003	2287	2123	208	184	184	194	239	220	196	138	162
7/20/2003	1527	220	176	183	168	169	189	181	179	128	155
7/29/2003	234	181	179	180	167	170	166	160	158	124	157
8/26/2003	208	175	173	186	166	185	203	160	134	123	136
9/2/2003	818	180	169	192	168	183	172	142	117	99	112
9/18/2003	761	1043	172	193	182	180	169	151	143	117	123
10/16/2003	440	763	598	608	617	850	801	695	468	240	182
10/30/2003	610	753	615	627	719	478	944	289	234	181	152
11/1/2003	611	704	843	356	336	344	175	144	261	162	155
12/4/2003	645	668	833	505	454	344	293	160	149	153	148
12/18/2003	837	722	449	283	199	287	173	175	148	119	121
1/6/2004	715	722	394	396	232	180	158	136	161	132	140
1/23/2004	866	12	437	409	349	293	224	197	149	145	118
2/1/2004	960	736	560	525	210	203	194	149	125	145	130
2/16/2004	1032	646	466	216	184	175	153	121	103	117	108
2/28/2004	878	565	383	348	203	267	197	176	131	136	145
3/1/2004	287	555	493	228	181	173	172	451	147	120	126
3/12/2004	269	465	568	676	613	184	183	166	333	394	394
3/21/2004	594	396	505	523	838	334	194	185	422	166	138
3/30/2004	414	596	349	372	191	190	182	157	158	128	114
4/4/2004	104	5376	71	828	172	172	148	145	136	125	110
4/10/2004	580	299	193	196	194	177	187	157	136	114	404
4/20/2004	470	269	296	322	285	441	283	218	280	370	734
4/30/2004	501	299	198	225	1927	697	768	781	1018	1416	2650
5/9/2004	253	510	1838	2830	2838	3874	2865	2805	2686	1852	4141
5/16/2004	389	821	490	1662	2015	2279	2487	3096	3046	3134	4582
5/25/2004	760	1841	1476	3404	2050	1974	2460	2228	2111	2644	4343
5/30/2004	531	2010	2099	1886	1187	1590	1690	1720	1592	2507	4889
6/4/2004	1107	1590	2001	919	963	1196	944	926	1548	2167	4472
6/14/2004	1367	1300	428	365	314	281	328	250	361	1123	5470
6/22/2004	1483	1057	429	278	249	239	225	202	212	264	244
7/7/2004	704	601	458	215	216	2173	195	163	157	290	197
7/13/2004	730	473	349	242	216	229	169	177	172	221	204
7/19/2004	680	399	279	226	212	219	150	168	170	177	178
7/28/2004	689	314	267	217	193	181	152	169	164	179	172
8/3/2004	671	270	265	206	192	195	158	168	163	192	188
8/12/2004	763	273	284	464	166	447	168	168	175	199	212
8/20/2004	939	436	271	1169	455	381	415	168	162	247	227
9/3/2004	801	1013	758	1217	760	748	594	562	646	153	152
9/19/2004	335	799	970	1309	1076	1521	873	350	668	805	1822
10/9/2004	539	356	651	709	631	783	1221	982	1141	1193	1184
10/26/2004	515	377	485	672	816	707	833	668	619	608	655
11/6/2004	451	806	482	806	954	877	862	347	430	227	224
11/11/2004	363	435	480	1088	487	467	386	501	339	206	210
11/21/2004	406	296	280	754	872	901	529	516	267	233	215
12/11/2004	411	330	353	870	659	542	566	347	222	227	201
12/20/2004	556	398	667	668	450	397	408	287	241	254	277

BY pcg
 number
 Date
 Point Location (m nsl)

Destroyed by Vandals. No Readings on 11/12/02																							
12/18/2003		No Readings																					
1/1/12/2002	372	312	270	299	18	333	264	358	298	296	245	1/12/2003	1111	1704	2318	1910	1926	1409	64	1520	887	296	245
2/20/2003	372	312	270	299	18	333	264	358	298	296	245	3/18/2003	1111	1704	2318	1910	1926	1409	64	1520	887	296	245
3/18/2003	1111	1704	2318	1910	1926	1409	64	1520	887	296	245	4/23/2003	3451	4817	3051	2246	2489	3182	159	1628	2116	1394	682
5/21/2003	780	858	771	1801	561	966	79	710	543	1336	2523	6/23/2003	3664	740	1472	2454	2263	2925	617	433	258	325	894
7/10/2003	912	2394	703	698	731	1083	419	289	227	225	195	7/16/2003	783	472	1273	292	265	288	27	295	247	241	688
7/20/2003	1317	666	312	542	176	129	186	18	206	176	184	7/29/2003	1551	1263	1302	982	3045	3518	61	391	253	274	272
8/26/2003	206	228	197	240	199	307	18	253	243	246	205	9/18/2003	109	169	172	170	170	230	58	263	177	149	170
9/18/2003	109	169	172	170	170	230	58	263	177	149	170	10/16/2003	633	382	598	470	337	567	34	579	410	600	292
10/16/2003	633	382	598	470	337	567	34	579	410	600	292	10/30/2003	471	806	321	436	442	534	29	636	351	241	547
11/11/2003	833	541	489	493	518	531	20	531	296	367	527	12/4/2003	675	724	667	241	229	235	23	237	238	183	184
12/4/2003	675	724	667	241	229	235	23	237	238	183	184	1/6/2004	292	202	197	209	181	221	12	225	179	174	170
1/6/2004	292	202	197	209	181	221	12	225	179	174	170	1/23/2004	253	241	227	251	215	250	15	215	176	184	183
2/1/2004	281	276	245	225	198	231	15	209	173	199	175	2/8/2004	282	243	186	202	179	226	15	207	159	173	175
2/8/2004	282	243	186	202	179	226	15	207	159	173	175	2/16/2004	457	289	271	278	249	249	18	205	183	174	242
2/16/2004	457	289	271	278	249	249	18	205	183	174	242	3/7/2004	324	281	256	335	278	335	18	250	217	184	184
3/7/2004	324	281	256	335	278	335	18	250	217	184	184	3/12/2004	255	199	202	267	238	429	18	262	201	198	182
3/12/2004	255	199	202	267	238	429	18	262	201	198	182	3/21/2004	384	320	243	255	205	224	12	163	133	140	129
3/21/2004	384	320	243	255	205	224	12	163	133	140	129	4/10/2004	327	403	324	541	602	523	15	369	339	235	171
4/10/2004	327	403	324	541	602	523	15	369	339	235	171	4/20/2004	773	941	1116	1964	2217	2331	101	2368	1740	296	1529
4/20/2004	773	941	1116	1964	2217	2331	101	2368	1740	296	1529	5/30/2004	735	2108	409	375	473	266	90	1107	204	296	1722
5/30/2004	735	2108	409	375	473	266	90	1107	204	296	1722	5/16/2004	648	544	241	389	1108	839	46	676	850	960	759
5/16/2004	648	544	241	389	1108	839	46	676	850	960	759	5/25/2004	928	1603	2108	2695	2333	3242	53	482	485	1741	197
5/25/2004	928	1603	2108	2695	2333	3242	53	482	485	1741	197	6/4/2004	1624	2814	3131	4940	4540	5299	139	5505	4499	4407	187
6/4/2004	1624	2814	3131	4940	4540	5299	139	5505	4499	4407	187	6/14/2004	2299	2839	2783	3428	3246	2264	102	2890	2673	3117	1896
6/14/2004	2299	2839	2783	3428	3246	2264	102	2890	2673	3117	1896	6/22/2004	1978	2319	1861	1829	2195	2941	134	4250	3647	4404	3694
6/22/2004	1978	2319	1861	1829	2195	2941	134	4250	3647	4404	3694	7/13/2004	921	601	352	351	432	724	67	1315	1816	2654	5639
7/13/2004	921	601	352	351	432	724	67	1315	1816	2654	5639	7/19/2004	433	473	307	289	245	506	45	1028	1002	2774	5639
7/19/2004	433	473	307	289	245	506	45	1028	1002	2774	5639	8/12/2004	301	262	219	276	238	252	26	294	410	963	1651
8/12/2004	301	262	219	276	238	252	26	294	410	963	1651	8/20/2004	704	293	213	227	201	241	19	232	208	260	114
8/20/2004	704	293	213	227	201	241	19	232	208	260	114	9/3/2004	830	357	1456	1703	1186	1495	469	750	676	550	425
9/3/2004	830	357	1456	1703	1186	1495	469	750	676	550	425	9/19/2004	257	274	2197	1765	1076	1551	24	438	348	216	285
9/19/2004	257	274	2197	1765	1076	1551	24	438	348	216	285	10/26/2004	343	431	1482	1183	1360	1523	111	1114	844	664	417
10/26/2004	343	431	1482	1183	1360	1523	111	1114	844	664	417	11/6/2004	421	511	1391	1209	1008	1210	39	925	774	906	0
11/6/2004	421	511	1391	1209	1008	1210	39	925	774	906	0	11/11/2004	391	562	1014	925	622	769	55	780	961	1120	390
11/11/2004	391	562	1014	925	622	769	55	780	961	1120	390	11/21/2004	400	528	430	593	600	901	32	860	795	1222	605
11/21/2004	400	528	430	593	600	901	32	860	795	1222	605	12/11/2004	528	440	543	707	714	993	33	780	512	393	696
12/11/2004	528	440	543	707	714	993	33	780	512	393	696	12/20/2004	587	454	528	557	675	906	175	860	543	303	430
12/20/2004	587	454	528	557	675	906	175	860	543	303	430												

APPENDIX D
November 2002 – September 2004 Spike Recovery Data

Plymouth Groundwater Quality Sampling Trip
12-Nov-02

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	12	1	0	
					Spiking Soln	200	250	500	
					Recovered	29	52	59	
					Recovery	95%	201%	117%	
Anion Std	1	10.00	0.00	AU	Well Conc				12
					Spiking Soln				30
					Recovered				26
					Recovery				186%

Plymouth Groundwater Quality Sampling Trip
19-Dec-02

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	12	1	0	
					Spiking Soln	200	250	500	
					Recovered	30	49	59	
					Recovery	97%	188%	116%	
Anion Std	1	10.00	0.00	AU	Well Conc				12
					Spiking Soln				30
					Recovered				15
					Recovery				109%

Plymouth Groundwater Quality Sampling Trip
21-Jan-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	10	3	2	
					Spiking Soln	206	272	533	
					Recovered	33	30	60	
					Recovery	112%	100%	108%	
Anion Std	1	10.00	0.00	AU	Well Conc				14
					Spiking Soln				30
					Recovered				17
					Recovery				109%

Plymouth Groundwater Quality Sampling Trip
20-Feb-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	237	22	29	
					Spiking Soln	206	272	533	
					Recovered	238	45	78	
					Recovery	102%	95%	97%	
Anion Std	1	10.00	0.00	AU	Well Conc				326
					Spiking Soln				30
					Recovered				306
					Recovery				103%

Plymouth Groundwater Quality Sampling Trip
23-Apr-03

Sample	Spike	Sample	NaN ₃	Well		Na ⁺	Mg ²⁺	Ca ²⁺	Cl ⁻
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ID	Volume (ml)	Volume (ml) (Total)	Volume (ml)	ID		Conc. (mg/L)	Conc. (mg/L)	Conc. (mg/L)	Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	9	2	2	
					Spiking Soln	206	272	533	
					Recovered	31	33	56	
					Recovery	108%	113%	102%	
Anion Std	1	10.00	0.00	AU	Well Conc				14
					Spiking Soln				30
					Recovered				15
					Recovery				100%

Plymouth Groundwater Quality Sampling Trip
15-Jun-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	K ⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AU	Well Conc	9	1	2	
					Spiking Soln	201	503	506	
					Recovered	28	50	28	
					Recovery	98%	97%	54%	
Anion Std	1	10.00	0.00	AU	Well Conc				17
					Spiking Soln				30
					Recovered				18
					Recovery				102%

Plymouth Groundwater Quality Sampling Trip
18-Sep-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
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Cation Std	1	10.00	0.00	AB	Well Conc	57	10	6	113
					Spiking Soln	200	40	50	
					Recovered	70	14	11	
					Recovery	98%	104%	100%	

Anion Std	1	10.00	0.00	AB	Well Conc				113
					Spiking Soln				400
					Recovered				141
					Recovery				100%

**Plymouth Groundwater Quality Sampling Trip
18-Sep-03**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BCf	Well Conc	100	9	12	118
					Spiking Soln	200	40	50	
					Recovered	110	14	19	
					Recovery	100%	121%	120%	

Anion Std	1	10.00	0.00	BCf	Well Conc	100	9	12	118
					Spiking Soln				400
					Recovered				149
					Recovery				102%

**Plymouth Groundwater Quality Sampling Trip
30-Oct-03**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
	1	10.00	0.00	AA	Well Conc	85	12	8	

Cation Std					Spiking Soln	205	39	49
					Recovered	96	15	13
					Recovery	98%	102%	102%

Anion Std	1	10.00	0.00	AA	Well Conc			165
					Spiking Soln			410
					Recovered			188
					Recovery			99%

Plymouth Groundwater Quality Sampling Trip
30-Oct-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BTe	Well Conc	41	8	12	
					Spiking Soln	205	39	49	
					Recovered	55	11	16	
					Recovery	97%	102%	102%	
Anion Std	1	10.00	0.00	BTe	Well Conc				76
					Spiking Soln				410
					Recovered				108
					Recovery				99%

Plymouth Groundwater Quality Sampling Trip
30-Oct-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BU	Well Conc	31	1	1	
					Spiking Soln	205	39	49	
					Recovered	47	5	6	
					Recovery	97%	106%	103%	

Anion Std	1	10.00	0.00	BU	Well Conc Spiking Soln Recovered Recovery	25 410 68 106%
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Plymouth Groundwater Quality Sampling Trip
11-Nov-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AS	Well Conc Spiking Soln Recovered Recovery	19 208 36 94%	1 40 5 105%	1 51 6 107%	
Anion Std	1	10.00	0.00	AS	Well Conc Spiking Soln Recovered Recovery				8 423 47 94%

Plymouth Groundwater Quality Sampling Trip
11-Nov-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	CB	Well Conc Spiking Soln Recovered Recovery	43 208 57 96%	5 40 9 103%	6 51 11 103%	
Anion Std	1	10.00	0.00	CB	Well Conc Spiking Soln Recovered				66 423 100

Recovery

98%

Plymouth Groundwater Quality Sampling Trip
11-Nov-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BTd	Well Conc	49	10	13	
					Spiking Soln	208	40	51	
					Recovered	62	13	17	
					Recovery	95%	100%	101%	
Anion Std	1	10.00	0.00	BTd	Well Conc				92
					Spiking Soln				423
					Recovered				124
					Recovery				99%

Plymouth Groundwater Quality Sampling Trip
18-Dec-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BCe	Well Conc	21	2	4	
					Spiking Soln	207	42	52	
					Recovered	32	6	8	
					Recovery	81%	105%	92%	
Anion Std	1	10.00	0.00	BCe	Well Conc				29
					Spiking Soln				393
					Recovered				58
					Recovery				89%

Plymouth Groundwater Quality Sampling Trip
18-Dec-03

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BE	Well Conc	15	2	3	
					Spiking Soln	207	42	52	
					Recovered	37	6	9	
					Recovery	108%	100%	115%	
Anion Std	1	10.00	0.00	BE	Well Conc				22
					Spiking Soln				393
					Recovered				65
					Recovery				109%

Plymouth Groundwater Quality Sampling Trip
Jan 04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BL	Well Conc	30	4	4	
					Spiking Soln	201	51	41	
					Recovered	52	9	10	
					Recovery	111%	102%	131%	
Anion Std	1	10.00	0.00	BL	Well Conc				49
					Spiking Soln				400
					Recovered				86
					Recovery				102%

Plymouth Groundwater Quality Sampling Trip
Jan 04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
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Cation Std	1	10.00	0.00	BZ	Well Conc	33	0	1
					Spiking Soln	201	51	41
					Recovered	55	5	6
					Recovery	110%	94%	139%

Anion Std	1	10.00	0.00	BZ	Well Conc			22
					Spiking Soln			400
					Recovered			63
					Recovery			104%

Plymouth Groundwater Quality Sampling Trip
24-Feb-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BTj	Well Conc	18	1	1	16
					Spiking Soln	206	41	51	
					Recovered	37	5	6	
					Recovery	101%	105%	105%	
Anion Std	1	10.00	0.00	BTj	Well Conc				16
					Spiking Soln				369
					Recovered				53
					Recovery				102%

Plymouth Groundwater Quality Sampling Trip
24-Feb-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BMd	Well Conc	503	28	30	774
					Spiking Soln	206	41	51	
					Recovered	473	30	32	
					Recovery	100%	99%	100%	

Anion Std	1	10.00	0.00	BMD	Well Conc	774
					Spiking Soln	369
					Recovered	726
					Recovery	99%

Plymouth Groundwater Quality Sampling Trip
24-Feb-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	CA	Well Conc	46	14	10	
					Spiking Soln	206	41	51	
					Recovered	62	17	14	
					Recovery	100%	101%	101%	
Anion Std	1	10.00	0.00	CA	Well Conc				100
					Spiking Soln				369
					Recovered				127
					Recovery				100%

Plymouth Groundwater Quality Sampling Trip
30-Mar-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AR	Well Conc	25	4	6	
					Spiking Soln	200	40	50	
					Recovered	43	8	11	
					Recovery	102%	102%	102%	
Anion Std	1	10.00	0.00	AR	Well Conc	25	4	6	50
					Spiking Soln				376
					Recovered				74
					Recovery				89%

Plymouth Groundwater Quality Sampling Trip
30-Mar-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BOh	Well Conc	290	8	9	
					Spiking Soln	200	40	50	
					Recovered	282	12	13	
					Recovery	100%	100%	100%	
Anion Std	1	10.00	0.00	BOh	Well Conc				422
					Spiking Soln				376
					Recovered				417
					Recovery				100%

Plymouth Groundwater Quality Sampling Trip
30-Mar-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BQ	Well Conc	9	1	0	
					Spiking Soln	200	40	50	
					Recovered	27	5	6	
					Recovery	97%	110%	109%	
Anion Std	1	10.00	0.00	BQ	Well Conc				9
					Spiking Soln				376
					Recovered				38
					Recovery				83%

Plymouth Groundwater Quality Sampling Trip
20-Apr-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	CC	Well Conc Spiking Soln Recovered Recovery	11 187 29 99%	1 40 5 105%	1 50 6 103%	
Anion Std	1	10.00	0.00	CC	Well Conc Spiking Soln Recovered Recovery				17 386 53 98%

Plymouth Groundwater Quality Sampling Trip
20-Apr-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BO	Well Conc Spiking Soln Recovered Recovery	11 187 28 99%	1 40 5 104%	1 50 6 102%	
Anion Std	1	10.00	0.00	BO	Well Conc Spiking Soln Recovered Recovery				14 386 49 95%

Plymouth Groundwater Quality Sampling Trip
20-Apr-04

Sample ID	Spike Volume (ml)	Sample Volume (ml)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
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		(Total)						
	1	10.00	0.00	AM	Well Conc	46	3	3
Cation Std					Spiking Soln	187	40	50
					Recovered	59	7	8
					Recovery	98%	99%	99%

Anion Std	1	10.00	0.00	AM	Well Conc			70
					Spiking Soln			386
					Recovered			97
					Recovery			96%

**Plymouth Groundwater Quality Sampling Trip
25-May-04**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BCe	Well Conc	90	3	0	
					Spiking Soln	201	38	48	
					Recovered	98	7	8	
					Recovery	97%	103%	160%	
Anion Std	1	10.00	0.00	BCe	Well Conc				80
					Spiking Soln				401
					Recovered				110
					Recovery				98%

**Plymouth Groundwater Quality Sampling Trip
25-May-04**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BJ	Well Conc	74	6	6	
					Spiking Soln	201	38	48	
					Recovered	84	10	10	

					Recovery	97%	101%	101%	
Anion Std	1	10.00	0.00	BJ	Well Conc				129
					Spiking Soln				401
					Recovered				154
					Recovery				99%

**Plymouth Groundwater Quality Sampling Trip
25-May-04**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BL	Well Conc	22	5	5	
					Spiking Soln	201	38	48	
					Recovered	37	8	9	
					Recovery	93%	101%	100%	
Anion Std	1	10.00	0.00	BL	Well Conc				38
					Spiking Soln				401
					Recovered				71
					Recovery				97%

**Plymouth Groundwater Quality Sampling Trip
22-Jun-04**

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AQ	Well Conc	58	1	2	
					Spiking Soln	208	40	52	
					Recovered	63	5	7	
					Recovery	86%	111%	108%	
Anion Std	1	10.00	0.00	AQ	Well Conc				43
					Spiking Soln				390
					Recovered				78

Recovery

101%

Plymouth Groundwater Quality Sampling Trip
SPIKES

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BCc	Well Conc	89	27	22	
					Spiking Soln	208	40	52	
					Recovered	102	30	27	
					Recovery	101%	103%	107%	
Anion Std	1	10.00	0.00	BCc	Well Conc				195
					Spiking Soln				390
					Recovered				217
					Recovery				101%

Plymouth Groundwater Quality Sampling Trip
SPIKES

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BTe	Well Conc	266	2	3	
					Spiking Soln	208	40	52	
					Recovered	243	6	8	
					Recovery	94%	97%	102%	
Anion Std	1	10.00	0.00	BTe	Well Conc				308
					Spiking Soln				390
					Recovered				321
					Recovery				101%

Plymouth Groundwater Quality Sampling Trip
13-Jul-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AD	Well Conc Spiking Soln Recovered Recovery	66 206 82 103%	6 42 9 102%	5 52 10 105%	
Anion Std	1	10.00	0.00	AD	Well Conc Spiking Soln Recovered Recovery				38 393 128 174%

Plymouth Groundwater Quality Sampling Trip
13-Jul-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AJ	Well Conc Spiking Soln Recovered Recovery	151 206 155 99%	5 42 8 100%	6 52 11 102%	
Anion Std	1	10.00	0.00	AJ	Well Conc Spiking Soln Recovered Recovery				250 393 263 100%

Plymouth Groundwater Quality Sampling Trip
13-Jul-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
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Cation Std	1	10.00	0.00	BTd	Well Conc	92	0	1	
					Spiking Soln	206	42	52	
					Recovered	102	4	6	
					Recovery	99%	97%	101%	

Anion Std	1	10.00	0.00	BTd	Well Conc				71
					Spiking Soln				393
					Recovered				106
					Recovery				103%

Plymouth Groundwater Quality Sampling Trip
12-Aug-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AL	Well Conc	104	1	1	
					Spiking Soln	209	43	54	
					Recovered	111	5	7	
					Recovery	97%	102%	104%	
Anion Std	1	10.00	0.00	AL	Well Conc				123
					Spiking Soln				423
					Recovered				148
					Recovery				97%

Plymouth Groundwater Quality Sampling Trip
12-Aug-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BC	Well Conc	11	0	1	
					Spiking Soln	209	43	54	
					Recovered	35	6	8	
					Recovery	111%	130%	139%	

Anion Std	1	10.00	0.00	BC	Well Conc Spiking Soln Recovered Recovery				12 423 52 99%
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Plymouth Groundwater Quality Sampling Trip
12-Aug-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BOd	Well Conc Spiking Soln Recovered Recovery	66 209 75 93%	22 43 23 98%	22 54 25 98%	
Anion Std	1	10.00	0.00	BOd	Well Conc Spiking Soln Recovered Recovery				188 423 209 99%

Plymouth Groundwater Quality Sampling Trip
23-Sep-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	BO	Well Conc Spiking Soln Recovered Recovery	10 206 31 104%	1 40 5 111%	1 54 6 99%	
Anion Std	1	10.00	0.00	BO	Well Conc Spiking Soln Recovered Recovery				14 391 50 96%

Plymouth Groundwater Quality Sampling Trip
23-Sep-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	AE	Well Conc	54	0	0	
					Spiking Soln	206	40	54	
					Recovered	69	5	6	
					Recovery	100%	109%	115%	
Anion Std	1	10.00	0.00	AE	Well Conc				38
					Spiking Soln				391
					Recovered				72
					Recovery				99%

Plymouth Groundwater Quality Sampling Trip
23-Sep-04

Sample ID	Spike Volume (ml)	Sample Volume (ml) (Total)	NaN ₃ Volume (ml)	Well ID		Na ⁺ Conc. (mg/L)	Mg ²⁺ Conc. (mg/L)	Ca ²⁺ Conc. (mg/L)	Cl ⁻ Conc. (mg/L)
Cation Std	1	10.00	0.00	ST	Well Conc	90	8	8	
					Spiking Soln	206	40	54	
					Recovered	101	12	12	
					Recovery	100%	107%	100%	
Anion Std	1	10.00	0.00	ST	Well Conc				156
					Spiking Soln				391
					Recovered				188
					Recovery				105%

APPENDIX E
Ground Surface Elevations

Model coordinates		model surface elevations (m)	X	Y	model surface elevations (m)
X	Y				
301.09057	572.24979	35.98	412.38219	467.526608	32.79
306.9915	559.69508	35.58	409.83711	466.417136	32.79
317.05599	531.53156	34.79	410.76675	466.362272	32.79
315.30339	515.78559	34.46	411.6842	466.081856	32.82
368.71654	495.90044	32.86	412.49497	465.731336	32.89
343.36633	482.10824	32.97	413.56786	465.563696	32.89
352.50118	466.96273	32.92	413.01922	474.76256	32.80
336.932	520.70202	34.31	389.94282	480.288584	32.85
360.92586	525.35631	33.93	386.4559	484.101632	32.85
346.81057	504.77926	33.00	387.2179	483.620048	32.85
308.46978	466.78899	36.93	388.2146	483.284768	32.85
392.12518	537.98418	34.42	389.17472	482.858048	32.85
396.02967	516.45006	33.40	385.92555	482.775752	32.81
415.12844	496.83922	33.09	386.64793	482.483144	32.81
437.18377	481.23042	35.47	387.60805	481.958888	32.81
469.0628	456.566	34.38	388.59865	481.580936	32.81
385.89507	465.1065	32.87	390.41526	482.973872	32.85
412.96436	463.8111	32.89	359.82248	485.671352	32.81
425.7751	484.75695	35.09	384.69416	464.054936	32.79
308.738	468.61779	36.85	459.6902	455.008472	34.61
358.96904	349.55072	36.10	432.53557	508.677656	32.67
309.11595	470.83369	36.84	431.91073	508.348472	32.67
313.02044	463.33561	36.86	431.36514	508.043672	32.64
360.9289	349.63302	36.10	430.84088	507.693152	32.64
362.68455	350.3371	36.10	430.1947	507.449312	32.64
365.2723	351.22407	36.12	429.65826	507.14756	32.64
428.05501	482.85805	35.09	429.03951	506.861048	32.64
416.74083	490.42623	34.80	428.4543	506.595872	32.64
417.97832	490.06657	34.83	427.97881	506.486144	32.64
418.99635	489.76482	34.88	426.33289	510.015728	32.71
420.24908	489.53012	34.85	425.97627	508.738616	32.71
421.45609	489.2558	34.85	441.05473	520.110704	32.50
421.77613	489.21922	34.95	427.97881	481.89488	35.17
422.07788	489.14607	34.95	440.9511	537.4904	32.33
422.52594	489.14302	34.91	441.72529	535.881056	32.33
423.4952	488.92662	34.91	408.41674	440.15252	35.05
425.1655	489.61242	34.64	373.42266	465.66428	33.02
425.14112	485.5921	35.09	616.79936	380.222744	32.41
424.72659	486.01273	35.09	841.94598	442.243448	32.86
426.72303	483.52251	35.09	590.10926	475.2134577	32.55
449.71714	506.858	33.14	812.49315	540.626792	31.73
448.87894	507.53161	33.14	813.59043	541.7576	32.68
448.0316	508.34238	33.14	410.6997	543.653456	32.36
310.69786	476.8413	36.83	586.10295	716.676224	33.04
408.7825	440.69506	34.89	806.85435	873.255032	32.81
316.77862	463.94216	36.96	449.29652	227.347256	39.97
413.68064	471.48291	32.79	342.00997	715.4936	36.08
410.44671	467.66986	32.79	365.50503	585.5291878	33.39
411.4617	467.65158	32.79	367.56963	582.7195964	33.39
			370.08858	579.7446367	33.41
			509.03122	546.994064	35.24
			510.53084	546.762416	35.28
			512.02741	546.530768	35.45

APPENDIX F
August 2003 – July 2004 Hydraulic Head Data

Well	Date	Head (m-MSL)	Well	Date	Head (m-MSL)	Well	Date	Head (m-MSL)
AA	8/26/2003	7.54	AA	12/18/2003	dry	AA	4/20/2004	7.46
AB	8/26/2003	7.58	AB	12/18/2003	7.42	AB	4/20/2004	7.48
AC	8/26/2003	7.61	AC	12/18/2003	7.50	AC	4/20/2004	7.54
AD	8/26/2003	7.64	AD	12/18/2003	7.53	AD	4/20/2004	7.55
AE	8/26/2003	7.60	AE	12/18/2003	7.52	AE	4/20/2004	7.52
AF	8/26/2003	7.69	AF	12/18/2003	7.57	AF	4/20/2004	7.60
AG	8/26/2003	7.71	AG	12/18/2003	7.57	AG	4/20/2004	7.61
AH	8/26/2003	7.76	AH	12/18/2003	7.61	AH	4/20/2004	7.64
AI	8/26/2003	7.65	AI	12/18/2003	dry	AI	4/20/2004	7.56
AJ	8/26/2003	7.63	AJ	12/18/2003	7.53	AJ	4/20/2004	7.55
AK	8/26/2003	7.71	AK	12/18/2003	7.62	AK	4/20/2004	7.61
AL	8/26/2003	7.69	AL	12/18/2003	7.58	AL	4/20/2004	7.60
AM	8/26/2003	7.82	AM	12/18/2003	dry	AM	4/20/2004	7.72
AN	8/26/2003	7.61	AN	12/18/2003	7.53	AN	4/20/2004	7.56
AO	8/26/2003	7.60	AO	12/18/2003	7.50	AO	4/20/2004	7.53
AP	8/26/2003	7.66	AP	12/18/2003	7.58	AP	4/20/2004	7.60
AQ	8/26/2003	7.64	AQ	12/18/2003	7.60	AQ	4/20/2004	7.63
AR	8/26/2003	7.73	AR	12/18/2003	7.67	AR	4/20/2004	7.71
AS	8/26/2003	7.78	AS	12/18/2003	7.67	AS	4/20/2004	7.70
AT	8/26/2003	7.76	AT	12/18/2003	7.67	AT	4/20/2004	7.71
AU	8/26/2003	7.67	AU	12/18/2003	7.63	AU	4/20/2004	7.66
AV	8/26/2003	7.81	AV	12/18/2003	7.66	AV	4/20/2004	7.72
AW	8/26/2003	8.07	AW	12/18/2003	7.91	AW	4/20/2004	7.96
AX	8/26/2003	7.79	AX	12/18/2003	7.65	AX	4/20/2004	7.70
AY	8/26/2003	7.90	AY	12/18/2003	7.77	AY	4/20/2004	7.80
AZ	8/26/2003	8.09	AZ	12/18/2003	7.93	AZ	4/20/2004	7.98
BA	8/26/2003	8.04	BA	12/18/2003	7.89	BA	4/20/2004	7.93
BB	8/26/2003	8.08	BB	12/18/2003	7.92	BB	4/20/2004	7.96
BC	8/26/2003	7.68	BC	12/18/2003	7.67	BC	4/20/2004	7.70
BCa	8/26/2003	7.69	BCa	12/18/2003	7.60	BCa	4/20/2004	7.62
BCb	8/26/2003	7.69	BCb	12/18/2003	7.60	BCb	4/20/2004	7.61
Bcc	8/26/2003	7.73	Bcc	12/18/2003	7.64	Bcc	4/20/2004	7.66
BCd	8/26/2003	7.69	BCd	12/18/2003	7.60	BCd	4/20/2004	7.64
Bce	8/26/2003	7.70	Bce	12/18/2003	7.62	Bce	4/20/2004	7.63
Bcf	8/26/2003	7.69	Bcf	12/18/2003	7.60	Bcf	4/20/2004	7.63
BCg	8/26/2003	7.70	BCg	12/18/2003	7.60	BCg	4/20/2004	7.64
BCh	8/26/2003	7.70	BCh	12/18/2003	7.60	BCh	4/20/2004	7.64
BCi	8/26/2003	7.71	BCi	12/18/2003	7.61	BCi	4/20/2004	7.64
BCj	8/26/2003	7.69	BCj	12/18/2003	7.60	BCj	4/20/2004	7.63
BD	8/26/2003	7.72	BD	12/18/2003	7.64	BD	4/20/2004	7.67
BE	8/26/2003	7.68	BE	12/18/2003	7.61	BE	4/20/2004	7.63
BF	8/26/2003	7.71	BF	12/18/2003	7.70	BF	4/20/2004	7.68
BG	8/26/2003	7.60	BG	12/18/2003	7.55	BG	4/20/2004	7.56
BH	8/26/2003	7.57	BH	12/18/2003	7.54	BH	4/20/2004	7.57
BI	8/26/2003	7.56	BI	12/18/2003	7.55	BI	4/20/2004	7.58
BJ	8/26/2003	7.80	BJ	12/18/2003	7.65	BJ	4/20/2004	7.68
BK	8/26/2003	7.83	BK	12/18/2003	7.74	BK	4/20/2004	7.78
BL	8/26/2003	7.83	BL	12/18/2003	7.68	BL	4/20/2004	7.71
BM	8/26/2003	7.71	BM	12/18/2003	7.64	BM	4/20/2004	7.67
BMa	8/26/2003	7.74	BMa	12/18/2003	7.66	BMa	4/20/2004	7.68
BMb	8/26/2003	7.74	BMb	12/18/2003	7.65	BMb	4/20/2004	7.68
BMc	8/26/2003	7.76	BMc	12/18/2003	7.66	BMc	4/20/2004	7.69
BMd	8/26/2003	7.75	BMd	12/18/2003	7.66	BMd	4/20/2004	7.68
BMe	8/26/2003	7.74	BMe	12/18/2003	7.66	BMe	4/20/2004	7.69
BMf	8/26/2003	7.74	BMf	12/18/2003	7.66	BMf	4/20/2004	7.69
BMg	8/26/2003	7.75	BMg	12/18/2003	7.67	BMg	4/20/2004	7.70
BMh	8/26/2003	7.75	BMh	12/18/2003	7.65	BMh	4/20/2004	7.70
BN	8/26/2003	7.74	BN	12/18/2003	7.63	BN	4/20/2004	7.66
BO	8/26/2003	7.74	BO	12/18/2003	7.63	BO	4/20/2004	7.66
Boa	8/26/2003	7.72	Boa	12/18/2003	7.62	Boa	4/20/2004	7.64
Bob	8/26/2003	7.72	Bob	12/18/2003	7.61	Bob	4/20/2004	7.64
Boc	8/26/2003	7.73	Boc	12/18/2003	7.62	Boc	4/20/2004	7.64
Bod	8/26/2003	7.73	Bod	12/18/2003	7.61	Bod	4/20/2004	7.65
Boe	8/26/2003	7.72	Boe	12/18/2003	7.61	Boe	4/20/2004	7.63
Bof	8/26/2003	7.74	Bof	12/18/2003	7.62	Bof	4/20/2004	7.65
BOg	8/26/2003	7.74	BOg	12/18/2003	7.64	BOg	4/20/2004	7.64
Boh	8/26/2003	7.73	Boh	12/18/2003	7.64	Boh	4/20/2004	7.65

AW	9/18/2003	7.88	AW	1/20/2004	7.87	AW	5/25/2004	7.94
AX	9/18/2003	7.72	AX	1/20/2004	7.60	AX	5/25/2004	7.71
AY	9/18/2003	7.81	AY	1/20/2004	7.75	AY	5/25/2004	7.79
AZ	9/18/2003	7.95	AZ	1/20/2004	7.89	AZ	5/25/2004	7.97
BA	9/18/2003	7.93	BA	1/20/2004	7.85	BA	5/25/2004	7.93
BB	9/18/2003	7.94	BB	1/20/2004	7.87	BB	5/25/2004	7.94
BC	9/18/2003	7.65	BC	1/20/2004	7.59	BC	5/25/2004	7.67
BCa	9/18/2003	7.60	BCa	1/20/2004	7.52	BCa	5/25/2004	7.60
BCb	9/18/2003	7.54	BCb	1/20/2004	7.22	BCb	5/25/2004	7.58
BCC	9/18/2003	7.61	BCC	1/20/2004	7.57	BCC	5/25/2004	7.64
BCd	9/18/2003	7.57	BCd	1/20/2004	7.54	BCd	5/25/2004	7.59
BCE	9/18/2003	7.60	BCE	1/20/2004	7.54	BCE	5/25/2004	7.61
BCf	9/18/2003	7.63	BCf	1/20/2004	7.54	BCf	5/25/2004	7.60
BCg	9/18/2003	7.63	BCg	1/20/2004	7.54	BCg	5/25/2004	7.64
BCh	9/18/2003	7.60	BCh	1/20/2004	7.55	BCh	5/25/2004	7.64
BCi	9/18/2003	7.60	BCi	1/20/2004	7.55	BCi	5/25/2004	7.62
BCj	9/18/2003	7.61	BCj	1/20/2004	7.58	BCj	5/25/2004	7.64
BD	9/18/2003	7.63	BD	1/20/2004	7.58	BD	5/25/2004	7.63
BE	9/18/2003	7.48	BE	1/20/2004	7.54	BE	5/25/2004	7.68
BF	9/18/2003	7.74	BF	1/20/2004	7.58	BF	5/25/2004	7.53
BG	9/18/2003	7.51	BG	1/20/2004	7.48	BG	5/25/2004	7.54
BH	9/18/2003	7.48	BH	1/20/2004	7.46	BH	5/25/2004	7.54
BI	9/18/2003	7.51	BI	1/20/2004	7.47	BI	5/25/2004	7.54
BJ	9/18/2003	7.71	BJ	1/20/2004	7.59	BJ	5/25/2004	7.69
BK	9/18/2003	7.70	BK	1/20/2004	7.66	BK	5/25/2004	7.76
BL	9/18/2003	7.71	BL	1/20/2004	7.62	BL	5/25/2004	7.71
BM	9/18/2003	7.55	BM	1/20/2004	7.55	BM	5/25/2004	7.66
BMa	9/18/2003	7.65	BMa	1/20/2004	7.57	BMa	5/25/2004	7.67
Bmb	9/18/2003	7.64	Bmb	1/20/2004	7.56	Bmb	5/25/2004	7.66
Bmc	9/18/2003	7.63	Bmc	1/20/2004	7.56	Bmc	5/25/2004	7.67
Bmd	9/18/2003	7.65	Bmd	1/20/2004	7.56	Bmd	5/25/2004	7.67
Bme	9/18/2003	7.64	Bme	1/20/2004	7.56	Bme	5/25/2004	7.67
Bmf	9/18/2003	7.51	Bmf	1/20/2004	7.56	Bmf	5/25/2004	7.67
Bmg	9/18/2003	7.56	Bmg	1/20/2004	7.59	Bmg	5/25/2004	7.68
Bmh	9/18/2003	7.64	Bmh	1/20/2004	7.56	Bmh	5/25/2004	7.67
BN	9/18/2003	7.62	BN	1/20/2004	7.53	BN	5/25/2004	7.65
BO	9/18/2003	7.63	BO	1/20/2004	7.50	BO	5/25/2004	7.64
BOa	9/18/2003	7.62	BOa	1/20/2004	7.48	BOa	5/25/2004	7.64
BOb	9/18/2003	7.50	BOb	1/20/2004	7.53	BOb	5/25/2004	7.63
BOc	9/18/2003	7.64	BOc	1/20/2004	7.56	BOc	5/25/2004	7.64
BOd	9/18/2003	7.61	BOd	1/20/2004	7.61	BOd	5/25/2004	7.65
BOe	9/18/2003	7.58	BOe	1/20/2004	7.52	BOe	5/25/2004	7.62
BOf	9/18/2003	7.64	BOf	1/20/2004	7.56	BOf	5/25/2004	7.65
BOg	9/18/2003	7.64	BOg	1/20/2004	7.56	BOg	5/25/2004	7.64
BOh	9/18/2003	7.62	BOh	1/20/2004	7.55	BOh	5/25/2004	7.65
BP	9/18/2003	7.66	BP	1/20/2004	7.55	BP	5/25/2004	7.67
BQ	9/18/2003	7.64	BQ	1/20/2004	7.52	BQ	5/25/2004	7.64
BR	9/18/2003	7.67	BR	1/20/2004	7.52	BR	5/25/2004	7.69
BS	9/18/2003	7.67	BS	1/20/2004	7.60	BS	5/25/2004	7.68
BTa	9/18/2003	7.53	BTa	1/20/2004	7.49	BTa	5/25/2004	7.56
BTb	9/18/2003	7.54	BTb	1/20/2004	7.50	BTb	5/25/2004	7.57
BTc	9/18/2003	7.54	BTc	1/20/2004	7.49	BTc	5/25/2004	7.57
BTd	9/18/2003	7.54	BTd	1/20/2004	7.49	BTd	5/25/2004	7.57
BTe	9/18/2003	7.55	BTe	1/20/2004	7.50	BTe	5/25/2004	7.44
BTf	9/18/2003	7.42	BTf	1/20/2004	7.36	BTf	5/25/2004	7.56
BTg	9/18/2003	7.55	BTg	1/20/2004	7.49	BTg	5/25/2004	7.61
BTh	9/18/2003	7.56	BTh	1/20/2004	7.50	BTh	5/25/2004	7.57
BTi	9/18/2003	7.54	BTi	1/20/2004	7.48	BTi	5/25/2004	7.86
BTj	9/18/2003	7.52	BTj	1/20/2004	7.48	BTj	5/25/2004	7.54
BTk	9/18/2003	7.51	BTk	1/20/2004	7.48	BTk	5/25/2004	7.52
BU	9/18/2003	7.46	BU	1/20/2004	7.44	BU	5/25/2004	7.64
BX	9/18/2003	7.62	BX	1/20/2004	7.57	BX	5/25/2004	7.50
BY	9/18/2003	7.36	BY	1/20/2004	7.39	BY	5/25/2004	7.45
BZ	9/18/2003	7.42	BZ	1/20/2004	7.37	BZ	5/25/2004	7.50
CA	9/18/2003	7.48	CA	1/20/2004	7.62	CA	5/25/2004	7.76
CB	9/18/2003	7.74	CB	1/20/2004	7.68	CB	5/25/2004	7.97
CC	9/18/2003	8.05	CC	1/20/2004	7.88	CC	5/25/2004	7.97
CD	9/18/2003	7.57	CD	1/20/2004	7.53	CD	5/25/2004	7.61

BJ	10/30/2003	7.44	BJ	2/24/2004	7.58	BJ	6/22/2004	7.59
BK	10/30/2003	7.52	BK	2/24/2004	7.68	BK	6/22/2004	7.65
BL	10/30/2003	7.49	BL	2/24/2004	7.60	BL	6/22/2004	7.61
BM	10/30/2003	7.43	BM	2/24/2004	frozen	BM	6/22/2004	7.57
BMa	10/30/2003	7.45	BMa	2/24/2004	frozen	BMa	6/22/2004	7.57
BMb	10/30/2003	7.46	BMb	2/24/2004	frozen	BMb	6/22/2004	7.57
BMc	10/30/2003	7.42	BMc	2/24/2004	frozen	BMc	6/22/2004	7.57
BMd	10/30/2003	7.45	BMd	2/24/2004	7.53	BMd	6/22/2004	7.57
BMe	10/30/2003	7.48	BMe	2/24/2004	frozen	BMe	6/22/2004	7.57
BmF	10/30/2003	7.46	BmF	2/24/2004	7.18	BmF	6/22/2004	7.57
BmG	10/30/2003	7.46	BmG	2/24/2004	frozen	BmG	6/22/2004	7.58
BmH	10/30/2003	7.46	BmH	2/24/2004	frozen	BmH	6/22/2004	7.70
BN	10/30/2003	7.42	BN	2/24/2004	frozen	BN	6/22/2004	7.43
BO	10/30/2003	7.45	BO	2/24/2004	frozen	BO	6/22/2004	7.58
BOa	10/30/2003	7.43	BOa	2/24/2004	frozen	BOa	6/22/2004	7.59
BOb	10/30/2003	7.43	BOb	2/24/2004	frozen	BOb	6/22/2004	7.59
BOc	10/30/2003	7.38	BOc	2/24/2004	frozen	BOc	6/22/2004	7.49
BOD	10/30/2003	7.41	BOD	2/24/2004	frozen	BOD	6/22/2004	7.53
BOe	10/30/2003	7.42	BOe	2/24/2004	frozen	BOe	6/22/2004	7.51
BOF	10/30/2003	7.38	BOF	2/24/2004	frozen	BOF	6/22/2004	7.55
BOg	10/30/2003	7.39	BOg	2/24/2004	frozen	BOg	6/22/2004	7.54
BOh	10/30/2003	7.41	BOh	2/24/2004	frozen	BOh	6/22/2004	7.54
BP	10/30/2003	7.45	BP	2/24/2004	frozen	BP	6/22/2004	7.57
BQ	10/30/2003	7.38	BQ	2/24/2004	6.61	BQ	6/22/2004	7.54
BR	10/30/2003	7.46	BR	2/24/2004	frozen	BR	6/22/2004	7.58
BS	10/30/2003	7.47	BS	2/24/2004	7.60	BS	6/22/2004	7.58
BTa	10/30/2003	7.36	BTa	2/24/2004	7.49	BTa	6/22/2004	7.49
BTb	10/30/2003	7.38	BTb	2/24/2004	7.49	BTb	6/22/2004	7.48
BTc	10/30/2003	7.38	BTc	2/24/2004	7.50	BTc	6/22/2004	7.47
BTd	10/30/2003	7.36	BTd	2/24/2004	7.49	BTd	6/22/2004	7.47
BTe	10/30/2003	7.39	BTe	2/24/2004	7.49	BTe	6/22/2004	7.48
BTf	10/30/2003	7.25	BTf	2/24/2004	7.36	BTf	6/22/2004	7.35
BTg	10/30/2003	7.37	BTg	2/24/2004	7.51	BTg	6/22/2004	7.46
BTi	10/30/2003	7.36	BTi	2/24/2004	7.50	BTi	6/22/2004	7.43
BTj	10/30/2003	7.39	BTj	2/24/2004	7.49	BTj	6/22/2004	7.40
BTK	10/30/2003	7.36	BTK	2/24/2004	7.45	BTK	6/22/2004	7.45
BU	10/30/2003	7.32	BU	2/24/2004	7.42	BU	6/22/2004	7.41
BX	10/30/2003	7.46	BX	2/24/2004	7.54	BX	6/22/2004	7.53
BY	10/30/2003	7.28	BY	2/24/2004	7.39	BY	6/22/2004	7.36
BZ	10/30/2003	7.28	BZ	2/24/2004	7.36	BZ	6/22/2004	7.34
CA	10/30/2003	7.22	CA	2/24/2004	7.39	CA	6/22/2004	7.39
CB	10/30/2003	7.56	CB	2/24/2004	7.71	CB	6/22/2004	7.67
CC	10/30/2003	7.72	CC	2/24/2004	7.88	CC	6/22/2004	7.87
CD	10/30/2003	7.39	CD	2/24/2004	7.52	CD	6/22/2004	7.50
ST	10/30/2003	7.18	ST	2/24/2004	7.29	ST	6/22/2004	7.59
10	10/13/2003	7.50	10	2/19/2004	7.74	10	6/15/2004	7.76
11	10/13/2003	7.41	11	2/19/2004	7.68	11	6/15/2004	7.62
12	10/13/2003	7.23	12	2/19/2004	7.53	12	6/15/2004	7.52
13B	10/13/2003	7.25	13B	2/19/2004	7.43	13B	6/15/2004	7.35
13C	10/13/2003	7.83	13C	2/19/2004	7.55	13C	6/15/2004	7.30
14A	10/13/2003	6.89	14A	2/19/2004	7.33	14A	6/15/2004	7.39
14B	10/13/2003	6.89	14B	2/19/2004	7.33	14B	6/15/2004	7.40
14C	10/13/2003	6.91	14C	2/19/2004	7.34	14C	6/15/2004	7.37
14D	10/13/2003	6.93	14D	2/19/2004	7.29	14D	6/15/2004	7.36
15	10/13/2003	6.67	15	2/19/2004	7.02	15	6/15/2004	7.04
16	10/13/2003	6.74	16	2/19/2004	6.74	16	6/15/2004	6.77
18	10/13/2003	7.81	18	2/19/2004	7.99	18	6/15/2004	8.12
19	10/13/2003	7.58	19	2/19/2004	7.86	19	6/15/2004	7.87
20	10/13/2003	6.73	20	2/19/2004	7.05	20	6/15/2004	7.10
23	10/13/2003	7.12	23	2/19/2004	7.30	23	6/15/2004	7.38
23A	10/13/2003	7.24	23A	2/19/2004	7.30	23A	6/15/2004	7.38
23B	10/13/2003	7.28	23B	2/19/2004	7.31	23B	6/15/2004	7.39
24	10/13/2003	6.65	24	2/19/2004	7.34	24	6/15/2004	7.36
24A	10/13/2003	6.66	24A	2/19/2004	7.33	24A	6/15/2004	7.37
24B	10/13/2003	6.67	24B	2/19/2004	6.88	24B	6/15/2004	7.35

BQ	11/11/2003	7.40	BQ	3/30/2004	7.53	BQ	7/13/2004	0.00
BR	11/11/2003	7.42	BR	3/30/2004	7.55	BR	7/13/2004	0.00
BS	11/11/2003	7.43	BS	3/30/2004	7.57	BS	7/13/2004	0.00
BTa	11/11/2003	7.33	BTa	3/30/2004	7.47	BTa	7/13/2004	0.00
BTb	11/11/2003	7.35	BTb	3/30/2004	7.49	BTb	7/13/2004	0.00
BTc	11/11/2003	7.35	BTc	3/30/2004	7.49	BTc	7/13/2004	0.00
BTd	11/11/2003	7.35	BTd	3/30/2004	7.45	BTd	7/13/2004	0.00
BTe	11/11/2003	7.34	BTe	3/30/2004	7.54	BTe	7/13/2004	0.00
BTf	11/11/2003	7.22	BTf	3/30/2004	7.39	BTf	7/13/2004	0.00
BTg	11/11/2003	7.35	BTg	3/30/2004	7.46	BTg	7/13/2004	0.00
BTi	11/11/2003	7.35	BTi	3/30/2004	7.50	BTi	7/13/2004	0.00
BTj	11/11/2003	7.34	BTj	3/30/2004	7.49	BTj	7/13/2004	0.00
BTk	11/11/2003	7.34	BTk	3/30/2004	7.48	BTk	7/13/2004	0.00
BU	11/11/2003	7.31	BU	3/30/2004	7.46	BU	7/13/2004	0.00
BX	11/11/2003	7.39	BX	3/30/2004	7.54	BX	7/13/2004	0.00
BY	11/11/2003	7.25	BY	3/30/2004	7.37	BY	7/13/2004	0.00
BZ	11/11/2003	7.24	BZ	3/30/2004	7.43	BZ	7/13/2004	0.00
CA	11/11/2003	7.24	CA	3/30/2004	7.39	CA	7/13/2004	0.00
CB	11/11/2003	7.47	CB	3/30/2004	7.65	CB	7/13/2004	0.00
CC	11/11/2003	7.72	CC	3/30/2004	7.87	CC	7/13/2004	0.00
CD	11/11/2003	7.35	CD	3/30/2004	7.36	CD	7/13/2004	0.00
ST	11/11/2003	7.17	ST	3/30/2004	7.31	ST	7/13/2004	0.00
10	11/11/2003	7.31	10	3/16/2004	7.75	10	7/20/2004	0.00
11	11/11/2003	7.46	11	3/16/2004	7.60	11	7/20/2004	0.00
12	11/11/2003	7.36	12	3/16/2004	7.50	12	7/20/2004	0.00
13B	11/11/2003	7.21	13B	3/16/2004	7.35	13B	7/20/2004	0.00
13C	11/11/2003	7.18	13C	3/16/2004	7.24	13C	7/20/2004	0.00
14A	11/11/2003	7.22	14A	3/16/2004	7.42	14A	7/20/2004	0.00
14B	11/11/2003	7.23	14B	3/16/2004	7.44	14B	7/20/2004	0.00
14C	11/11/2003	7.24	14C	3/16/2004	7.44	14C	7/20/2004	0.00
14D	11/11/2003	7.21	14D	3/16/2004	7.44	14D	7/20/2004	0.00
15	11/11/2003	6.87	15	3/16/2004	7.04	15	7/20/2004	0.00
16	11/11/2003	6.63	16	3/16/2004	6.76	16	7/20/2004	0.00
18	11/11/2003	was this dry? 7.72 dry	18	3/16/2004	8.09	18	7/20/2004	0.00
19	11/11/2003		19	3/16/2004	7.85	19	7/20/2004	0.00
20	11/11/2003		20	3/16/2004	7.10	20	7/20/2004	0.00
23	11/11/2003		23	3/16/2004	7.39	23	7/20/2004	0.00
23A	11/11/2003	7.15	23A	3/16/2004	7.40	23A	7/20/2004	0.00
23B	11/11/2003	7.16	23B	3/16/2004	7.38	23B	7/20/2004	0.00
24	11/11/2003	7.21	24	3/16/2004	7.39	24	7/20/2004	0.00
24A	11/11/2003	7.21	24A	3/16/2004	7.40	24A	7/20/2004	0.00
24B	11/11/2003	7.17	24B	3/16/2004	7.38	24B	7/20/2004	0.00

APPENDIX G
Hindcasted Specific Conductivity and Ion Data

Row	Well	days	Travel time	win	pos	origins date	Origin
20	BCd	40	6	1	0	6/3/2004	effective basin
20	BCe	40	6	1	0	6/3/2004	effective basin
20	BTg	70	10	2	0	6/3/2004	effective basin
20	BTd	70	10	2	0	6/3/2004	effective basin
20	BCb	17	2	1	0	6/3/2004	effective basin
20	BMa	17	2	1	0	6/3/2004	effective basin
20	BTf	68	10	2	0	6/3/2004	effective basin
20	BCf	15	5	1	0	6/3/2004	effective basin
21	BE	15	5	1	0	6/3/2004	effective basin
21	BTa	65	9	2	0	6/3/2004	effective basin
21	BTb	65	9	2	0	6/3/2004	effective basin
21	BTc	65	9	2	0	6/3/2004	effective basin
21	BTg	65	9	2	0	6/3/2004	effective basin
21	BTd	65	9	2	0	6/3/2004	effective basin
12	AJ	11	2	0	0	6/11/2004	crest of basin, across down slope
20	BMa	11	2	0	0	6/11/2004	effective basin
19	BMd	10	1	0	0	6/12/2004	effective basin
19	BN	10	1	0	0	6/12/2004	effective basin
20	BMb	9	1	0	0	6/13/2004	effective basin
19	BMa	7	1	0	0	6/13/2004	effective basin
20	BCg	25	4	1	0	6/13/2004	effective basin
20	AT	2	0	0	0	6/20/2004	effective basin
15	AO	50	7	2	0	6/23/2004	near BO cluster, not "effective" area
19	BCb	20	3	1	0	6/23/2004	effective basin
19	BCb	20	3	1	0	6/23/2004	effective basin
20	BCc	20	3	1	0	6/23/2004	effective basin
20	BTk	50	7	2	0	6/23/2004	effective basin
13	AH	90	13	3	0	6/25/2004	area 12 (south shoulder of EB line)
19	BTj	90	13	3	0	6/25/2004	effective basin
20	BMa	17	2	1	0	6/26/2004	effective basin
21	BCj	42	6	1	0	7/12/2004	effective basin
12	AJ	11	2	0	0	7/2/2004	crest of basin, across down slope
19	BMd	10	1	0	0	7/2/2004	effective basin
20	BCd	40	6	1	0	7/2/2004	effective basin
20	BCe	40	6	1	0	7/2/2004	effective basin
19	BMd	10	1	0	0	7/2/2004	effective basin
19	BN	10	1	0	0	7/2/2004	effective basin
19	BMa	9	1	0	0	7/2/2004	effective basin
19	BMa	7	1	0	0	7/2/2004	effective basin
8	AB	35	5	1	0	7/2/2004	west of rest area, across slope
21	BE	35	5	1	0	7/2/2004	effective basin
21	AT	2	0	0	0	7/13/2004	effective basin
8	AP	50	4	1	0	7/13/2004	effective basin
20	BCi	30	4	1	0	7/13/2004	effective basin
22	BO	50	4	1	0	7/13/2004	N of WB line, near 4 UO wells across rd
20	BTg	70	10	2	0	7/15/2004	effective basin
20	BTg	70	10	2	0	7/15/2004	effective basin
20	BTf	68	10	2	0	7/17/2004	effective basin
20	BCj	25	4	1	0	7/18/2004	effective basin
21	BTa	65	9	2	0	7/20/2004	effective basin
21	BTb	65	9	2	0	7/20/2004	effective basin
21	BTf	65	9	2	0	7/20/2004	effective basin
20	BTa	65	9	2	0	7/20/2004	effective basin
19	BCa	20	3	1	0	7/23/2004	effective basin
19	BCb	20	3	1	0	7/23/2004	effective basin
20	BCc	20	3	1	0	7/23/2004	effective basin
21	BD	20	3	1	0	7/13/2004	effective basin
20	BCk	17	2	1	0	7/25/2004	effective basin
20	BMa	17	2	1	0	7/25/2004	effective basin
20	SCF	15	2	1	0	7/28/2004	effective basin
12	AJ	11	2	0	0	8/1/2004	crest of basin, across down slope
20	BMa	11	2	0	0	8/1/2004	effective basin
19	BMd	10	1	0	0	8/2/2004	effective basin
19	BN	10	1	0	0	8/2/2004	effective basin
20	BMb	9	1	0	0	8/3/2004	effective basin
19	BMa	7	1	0	0	8/3/2004	effective basin
20	BTj	2	0	0	0	8/15/2004	effective basin
21	BCj	42	6	1	0	8/12/2004	effective basin
20	BCd	40	6	1	0	8/14/2004	effective basin
21	BE	35	5	1	0	8/19/2004	effective basin
20	BCi	30	4	1	0	8/24/2004	effective basin
22	BO	50	4	1	0	8/24/2004	N of WB line, near 4 UO wells across rd
20	BCg	25	4	1	0	8/29/2004	effective basin
19	BCa	20	3	1	0	9/3/2004	effective basin
19	BCb	20	3	1	0	9/3/2004	effective basin
21	BD	20	3	1	0	9/3/2004	effective basin
20	BMb	17	2	1	0	9/3/2004	effective basin
20	BCf	15	2	1	0	9/3/2004	effective basin
20	BMa	11	2	0	0	9/12/2004	effective basin
19	BMd	10	1	0	0	9/13/2004	effective basin
20	BMb	9	1	0	0	9/14/2004	effective basin
19	BMa	7	1	0	0	9/15/2004	effective basin
20	AT	2	0	0	0	9/17/2004	effective basin

CS- Cont.	Yw (mg/L)	CS- Cont.	Mg+1 (mg/L)
394.3	244.4	25.1	20.5
227.2	148.5	13.9	11.5
75.9	51.1	8.6	10.1
149.2	14.0	7.7	2.9
204.5	175.7	2.5	2.1
34.7	42.1	1.5	1.3
148.7	93.0	7.1	9.4
279.6	159.5	9.8	8.8
21.2	23.6	3.9	4.9
112.4	110.9	2.0	1.5
83.7	85.9	0.6	0.4
39.2	69.0	0.2	0.2
29.5	45.6	0.1	0.0
32.5	49.1	0.1	0.1
167.5	110.2	4.8	3.7
21.1	25.0	2.2	1.8
179.1	141.8	6.9	5.7
631.2	351.3	32.1	23.5
454.7	250.2	15.9	15.9
454.3	339.0	14.9	12.5
235.0	191.6	24.9	27.1
327.1	202.9	17.3	17.0
221.2	139.8	4.7	4.7
208.8	149.9	6.0	5.7
311.2	249.2	5.7	4.8
109.5	37.5	10.4	12.7
209.5	134.6	15.7	8.3
60.5	58.2	3.3	2.9
63.5	55.9	3.1	2.8
13.5	14.9	1.5	1.2
19.0	20.9	3.4	4.3
249.7	159.9	6.1	4.8
21.1	17.4	1.4	1.0
28.1	23.1	3.3	3.1
18.5	20.0	1.6	1.4
58.9	56.4	3.7	2.9
50.4	67.4	5.6	4.1
291.8	109.7	9.3	10.1
264.2	161.8	11.9	16.6
50.5	17.5	2.2	4.1
20.9	18.3	6.0	6.3
212.9	144.4	10.8	11.2
152.8	119.9	1.5	1.0
65.7	51.6	7.7	4.8
123.9	82.1	6.9	6.6
256.9	172.7	16.0	15.7
71.1	77.8	3.5	3.5
118.2	142.9	9.8	10.2
120.5	72.1	12.2	14.5
158.2	149.0	1.8	1.1
144.3	131.8	3.4	2.6
144.9	107.1	7.5	7.8
110.9	95.9	5.0	5.1
157.1	123.8	7.0	6.6
82.8	72.9	5.5	5.0
34.1	41.2	3.9	3.6
149.8	99.7	10.1	12.4
211.1	114.0	21.6	22.5
81.2	34.2	5.7	4.2
142.6	95.8	7.1	7.7
158.5	106.1	4.0	3.3
19.9	16.5	0.8	0.6
76.8	34.6	5.6	3.7
14.0	15.4	2.0	1.4
147.6	70.9	9.4	10.4
109.9	83.5	9.0	11.1
164.6	87.2	12.3	14.4
28.0	42.0	1.3	0.9
94.6	63.2	7.1	4.7
31.1	28.3	3.0	1.6
109.1	114.3	7.6	5.3
112.7	98.1	6.1	5.3
117.1	85.7	5.5	6.2
10.2	24.6	0.6	0.5
78.1	64.4	4.1	4.4
18.3	25.1	0.7	0.6
218.6	114.5	12.3	11.2
19.8	28.6	0.5	0.4
91.0	64.1	3.9	4.2
185.4	103.2	5.9	6.6
114.6	75.4	7.7	7.3
189.9	112.8	15.1	13.5
206.5	131.5	13.4	13.0

Travel time						Origin	Cr. Conc. (mg/L)	Na+ Conc. (mg/L)	Ca+2 Conc. (mg/L)	Mg+2 Conc. (mg/L)
Row	Well	days	hrs	mins	origins date					

Travel time						Origin	Cr. Conc. (mg/L)	Na+ Conc. (mg/L)	Ca+2 Conc. (mg/L)	Mg+2 Conc. (mg/L)
Row	Well	days	hrs	mins	origins date					

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msf	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msf	SpecCond uS/cm
20	BTe	65.0	9.3	2.2	2/17/2003	effective basin	2	1.7	760.0	20	BTcpB	50	7	2	3/1/2004	effective ba	2	5.0	840.1
20	AT	2.0	0.3	0.1	2/18/2003	effective basin	1	7.3	799.0	20	BTcpC	60.0	8.6	2.0	3/1/2004	effective ba	2	3.5	3000.7
20	BMcpA	1.0	0.1	0.0	2/19/2003	effective basin	1	6.9	1690.0	20	BYcpJ	140.0	18.7	4.7	3/1/2004	effective ba	2	-1.8	565.6
14	AN	210.0	30.0	7.0	2/20/2003	area 12 (south shoulder of EB lane)	1	8.0	170.0	20	ATcpB	5	1	0	3/2/2004	effective ba	1	5.3	2800.2
20	BMcpJ	18.0	2.6	0.6	2/20/2003	effective basin	2	0.8	1045.0	20	BMcpC	5	1	0	3/2/2004	effective ba	1	5.4	2321.1
20	BYcpJ	140.0	18.7	4.7	2/20/2003	effective basin	2	-1.8	227.0	20	BTcpJ	75.0	10.7	2.5	3/2/2004	effective ba	2	-2.6	6963.7
20	BYcpJ	150.0	20.0	5.0	2/20/2003	effective basin	2	-3.3	277.0	20	BMcpF	9.0	1.3	0.3	3/3/2004	effective ba	2	3.6	1223.8
24	AR	300	43	10	2/21/2003	N of WB lane, N of median 8	1	8.1	84.0	20	BMcpJ	18.0	2.6	0.6	3/3/2004	effective ba	2	0.8	464.2
21	BCcpA	25.0	3.6	0.8	2/21/2003	effective basin	1	7.1	9248.1	20	ATcpA	3	0	0	3/4/2004	effective ba	1	6.8	2359.8
21	BCcpB	25.0	3.6	0.8	2/21/2003	effective basin	1	5.6	5945.0	20	BMcpB	3	0	0	3/4/2004	effective ba	1	6.0	1434.8
20	BMcpK	25.0	3.6	0.8	2/21/2003	effective basin	2	-0.7	630.0	20	BMcpE	8.0	1.1	0.3	3/4/2004	effective ba	2	4.2	2658.7
20	BCg	25.0	3.6	0.8	2/22/2003	effective basin	2	2.9	1957.0	21	BUcpA	110.0	14.7	3.7	3/4/2004	effective ba	1	6.0	1483.4
20	BTJ	90.0	12.9	3.0	2/22/2003	effective basin	2	-3.7	488.8	21	BUcpB	110.0	14.7	3.7	3/4/2004	effective ba	2	4.5	1057.1
20	BTcpC	60.0	8.6	2.0	2/22/2003	effective basin	2	3.5	1119.0	21	BUcpC	110.0	14.7	3.7	3/4/2004	effective ba	2	3.0	429.5
20	BMcpI	15.0	2.1	0.5	2/23/2003	effective basin	2	1.7	922.0	21	BUcpD	110.0	14.7	3.7	3/4/2004	effective ba	2	1.5	278.0
22	AQ	330.0	47.1	11.0	2/24/2003	N of WB lane, near 4 UG wells across rd	1	8.2	179.0	21	BUcpE	110.0	14.7	3.7	3/4/2004	effective ba	2	0.9	248.8
22	BMcpA	420	56	14	2/25/2003	by back fence area, runoff b/w BK/BS	1	6.0	1444.9	21	BUcpF	110.0	14.7	3.7	3/4/2004	effective ba	2	0.2	239.4
20	BMcpH	13.0	1.9	0.4	2/25/2003	effective basin	2	2.3	736.0	21	BUcpG	110.0	14.7	3.7	3/4/2004	effective ba	2	-0.4	224.9
21	BUcpA	110.0	14.7	3.7	2/25/2003	effective basin	1	6.0	521.0	21	BUcpH	110.0	14.7	3.7	3/4/2004	effective ba	2	-1.0	201.7
21	BUcpB	110.0	14.7	3.7	2/25/2003	effective basin	2	4.5	213.0	12	AG	130.0	18.6	4.3	3/5/2004	area 12 (soi	1	7.3	345.0
21	BUcpC	110.0	14.7	3.7	2/25/2003	effective basin	2	3.0	3009.0	20	BCg	25.0	3.6	0.8	3/5/2004	effective ba	2	2.9	1296.0
21	BUcpD	110.0	14.7	3.7	2/25/2003	effective basin	2	1.5	6239.0	21	BCcpA	25.0	3.6	0.8	3/5/2004	effective ba	1	7.1	897.2
21	BUcpE	110.0	14.7	3.7	2/25/2003	effective basin	2	0.9	2927.0	21	BCcpB	25.0	3.6	0.8	3/5/2004	effective ba	1	5.6	33120.5
21	BUcpF	110.0	14.7	3.7	2/25/2003	effective basin	2	0.2	4335.0	21	BCcpC	30.0	4.3	1.0	3/5/2004	effective ba	2	4.1	1554.1
21	BUcpG	110.0	14.7	3.7	2/25/2003	effective basin	2	-0.4	4653.0	20	BMcpK	25.0	3.6	0.8	3/5/2004	effective ba	2	-0.7	202.6
21	BUcpH	110.0	14.7	3.7	2/25/2003	effective basin	2	-1.0	1757.0	20	BYcpD	130.0	17.3	4.3	3/5/2004	effective ba	2	1.3	289.0
20	BYcpI	140.0	18.7	4.7	2/26/2003	effective basin	2	-1.8	247.0	20	BYcpE	130.0	17.3	4.3	3/5/2004	effective ba	2	0.7	244.9
19	BCa	20.0	2.9	0.7	2/27/2003	effective basin	1	6.0	3469.0	20	BYcpF	130.0	17.3	4.3	3/5/2004	effective ba	2	0.0	505.5
19	BCb	20.0	2.9	0.7	2/27/2003	effective basin	2	3.6	5030.0	20	BYcpG	130.0	17.3	4.3	3/5/2004	effective ba	2	-0.6	44.9
20	BCc	20.0	2.9	0.7	2/27/2003	effective basin	2	2.0	1620.0	20	BYcpH	130.0	17.3	4.3	3/5/2004	effective ba	2	-1.2	1028.4
21	BD	20.0	2.9	0.7	2/27/2003	effective basin	1	5.6	3222.0	20	CA	160.0	22.9	5.3	3/5/2004	rest area, n	1	6.1	320.0
20	BMcpG	11.0	1.6	0.4	2/27/2003	effective basin	2	2.9	549.0	16	AS	80.0	11.4	2.7	3/6/2004	area 12 (soi	1	7.4	735.0
20	BMcpJ	18.0	2.6	0.6	2/28/2003	effective basin	2	0.8	1512.0	20	ATcpC	6.0	0.9	0.2	3/6/2004	effective ba	2	4.7	347.4
20	BMcpF	9.0	1.3	0.3	3/1/2003	effective basin	2	3.6	487.0	20	BMcpA	1	0	0	3/6/2004	effective ba	1	6.9	3038.5
20	BYcpJ	150.0	20.0	5.0	3/1/2003	effective basin	2	-3.3	274.0	20	BMcpD	6.0	0.9	0.2	3/6/2004	effective ba	2	4.8	5908.1
10	AI	200.0	28.6	6.7	3/2/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	229.0	20	BMcpI	15.0	2.1	0.5	3/6/2004	effective ba	2	1.7	1139.4
20	BCb	17.0	2.4	0.6	3/2/2003	effective basin	1	5.0	717.0	20	BTcpK	80.0	11.4	2.7	3/6/2004	effective ba	2	-4.2	6913.5
20	BMc	17.0	2.4	0.6	3/2/2003	effective basin	2	1.5	689.0	20	BYcpJ	150.0	20.0	5.0	3/6/2004	effective ba	2	-3.3	581.4
20	BMcpE	8.0	1.1	0.3	3/2/2003	effective basin	2	4.2	567.0	20	ATcpB	5.0	0.7	0.2	3/7/2004	effective ba	1	5.3	2723.7
20	BTcpK	80.0	11.4	2.7	3/2/2003	effective basin	2	-4.2	3427.0	20	BMcpC	5.0	0.7	0.2	3/7/2004	effective ba	1	5.4	2447.7
20	BYcpD	130.0	17.3	4.3	3/2/2003	effective basin	2	1.3	698.0	20	BTcpD	70.0	10.0	2.3	3/7/2004	effective ba	2	1.9	5302.8
20	BYcpE	130.0	17.3	4.3	3/2/2003	effective basin	2	0.7	731.0	20	BTcpE	70.0	10.0	2.3	3/7/2004	effective ba	2	1.3	3888.7
20	BYcpF	130.0	17.3	4.3	3/2/2003	effective basin	2	0.0	1083.0	20	BTcpF	70.0	10.0	2.3	3/7/2004	effective ba	2	0.7	4293.4
20	BYcpG	130.0	17.3	4.3	3/2/2003	effective basin	2	-0.6	419.0	20	BTcpG	70.0	10.0	2.3	3/7/2004	effective ba	2	0.1	4368.3
20	BYcpH	130.0	17.3	4.3	3/2/2003	effective basin	2	-1.2	289.0	20	BTcpH	70.0	10.0	2.3	3/7/2004	effective ba	2	-0.5	4128.4
20	BYcpI	140.0	18.7	4.7	3/2/2003	effective basin	2	-1.8	270.0	20	BTcpI	70.0	10.0	2.3	3/7/2004	effective ba	2	-1.1	4845.4
20	BMcpI	15.0	2.1	0.5	3/3/2003	effective basin	2	1.7	872.0	20	BMcpH	13.0	1.9	0.4	3/8/2004	effective ba	2	2.3	590.8
21	BUcpI	120.0	16.0	4.0	3/3/2003	effective basin	2	-1.6	982.0	20	ATcpA	3.0	0.4	0.1	3/9/2004	effective ba	1	6.8	3181.7
11	AK	240.0	34.3	8.0	3/4/2003	@ E BC, east of median 13 area	1	7.4	421.0	21	BCJ	42.0	6.0	1.4	3/9/2004	effective ba	2	-0.2	3573.0
20	ATcpC	6.0	0.9	0.2	3/4/2003	effective basin	2	4.7	11968.0	20	BMcpB	3.0	0.4	0.1	3/9/2004	effective ba	1	6.0	3587.1
20	BCF	15.0	2.1	0.5	3/4/2003	effective basin	1	6.8	2299.0	21	BUcpI	120	16	4	3/9/2004	effective ba	2	-1.6	157.2
21	BCcpH	50.0	7.1	1.7	3/4/2003	effective basin	2	-0.8	1022.0	20	BYcpA	120	16	4	3/9/2004	effective ba	1	5.8	1525.3
21	BCcpI	50.0	7.1	1.7	3/4/2003	effective basin	2	-1.4	853.0	20	BYcpB	120	16	4	3/9/2004	effective ba	2	4.3	601.3
21	BCcpJ	50.0	7.1	1.7	3/4/2003	effective basin	2	-2.0	1239.0	20	BYcpC	120	16	4	3/9/2004	effective ba	2	2.8	352.4
20	BMcpD	6.0	0.9	0.2	3/4/2003	effective basin	2	4.8	756.0	19	BCa	20.0	2.9	0.7	3/10/2004	effective ba	1	6.0	4294.0
20	BTk	50.0	7.1	1.7	3/4/2003	effective basin	1	7.3	1484.0	19	BCb	20.0	2.9	0.7	3/10/2004	effective ba	2	3.6	4747.0
20	BTcpA	50.0	7.1	1.7	3/4/2003	effective basin	1	6.5	1587.3	20	BCc	20.0	2.9	0.7	3/10/2004	effective ba	2	2.0	5460.0
20	BTcpB	50.0	7.1	1.7	3/4/2003	effective basin	2	5.0	1583.0	21	BCcpA	25.0	3.6	0.8	3/10/2004	effective ba	1	7.1	653.0
21	CB	240.0	34.3	8.0	3/4/2003	N of WB lane, near 4 UG wells across rd	1	8.6	3359.0	21	BCcpB	25.0	3.6	0.8	3/10/2004	effective ba	1	5.6	3696.3
20	ATcpB	5.0	0.7	0.2	3/5/2003	effective basin	1	5.3	3220.0	21	BD	20.0	2.9	0.7	3/10/2004	effective ba	1	5.6	1979.0
20	BMcpC	5.0	0.7	0.2	3/5/2003	effective basin	1	5.4	882.0	20	BMcpG	11.0	1.6	0.4	3/10/2004	effective ba	2	2.9	970.6
20	BMcpH	13.0	1.9	0.4	3/5/2003	effective basin	2	2.3	810.0	20	BMcpK	25.0	3.6	0.8	3/10/2004	effective ba	2	-0.7	227.9
20	ATcpA	3.0	0.4	0.1	3/7/2003	effective basin	1	6.8	698.5	20	BTcpC	60	9	2	3/10/2004	effective ba	2	3.5	2683.5
22	BMcpA	420.0	56.0	14.0	3/7/2003	by back fence area, runoff b/w BK/BS	1	6.0	1403.1	20	BYcpI	140.0	18.7	4.7	3/10/2004	effective ba	2	-1.8	410.4
20	BMcpB	3.0	0.4	0.1	3/7/2003	effective basin	1	6.0	386.0	20	BCd	40.0	5.7	1.3	3/11/2004	effective ba	2	0.2	6040.0
20	BMcpG	11.0	1.6	0.4	3/7/2003	effective basin	2	2.9	587.0	20	BCe	40.0	5.7	1.3	3/11/2004	effective ba	2	-1.6	4840.0
20	BTcpJ	75.0	10.7	2.5	3/7/2003	effective basin	2	-2.6	3316.0	21	BCcpC	30.0	4.3	1.0	3/11/2004	effective ba	2	4.1	1706.4
20	BMc	11.0	1.6	0.4	3/8/2003	effective basin	2	3.0	114.0	21	BCcpD	40	6	1	3/11/2004	effective ba	2	2.6	4185.6
20	BYcpD	130.0	17.3	4.3	3/8/2003	effective basin	2	1.3	292.0										

Row	Well	days	hrs	mins	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	hrs	mins	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
20	BYpppE	130.0	17.3	4.3	3/8/2003	effective basin	2	0.7	265.0	21	BCpppG	40	6	1	3/11/2004	effective ba	2	-0.2	3769.0
20	BYpppF	130.0	17.3	4.3	3/8/2003	effective basin	2	0.0	288.0	21	BCpppH	50.0	7.1	1.7	3/11/2004	effective ba	2	-0.8	1172.2
20	BYpppG	130.0	17.3	4.3	3/8/2003	effective basin	2	-0.6	27.0	21	BCpppI	50.0	7.1	1.7	3/11/2004	effective ba	2	-1.4	1444.9
20	BYpppH	130.0	17.3	4.3	3/8/2003	effective basin	2	-1.2	295.0	21	BCpppJ	50.0	7.1	1.7	3/11/2004	effective ba	2	-2.0	1333.1
19	BMd	10.0	1.4	0.3	3/9/2003	effective basin	2	2.1	264.0	20	BMpppA	1.0	0.1	0.0	3/11/2004	effective ba	1	6.9	19412.4
20	BMpppA	1.0	0.1	0.0	3/9/2003	effective basin	2	6.9	1327.1	20	BTpppA	50.0	7.1	1.7	3/11/2004	effective ba	1	6.5	127.0
20	BMpppB	9.0	1.3	0.3	3/9/2003	effective basin	2	3.6	461.0	20	BTpppB	50.0	7.1	1.7	3/11/2004	effective ba	2	5.0	884.0
19	BN	10.0	1.4	0.3	3/9/2003	effective basin	2	1.8	561.0	20	BTpppC	50.0	10.7	2.5	3/11/2004	effective ba	2	-2.6	5423.8
20	BMpppF	9.0	1.3	0.3	3/9/2003	effective basin	2	3.9	316.0	20	BTpppD	130.0	17.3	4.3	3/11/2004	effective ba	2	-4.2	5238.6
20	BMpppE	8.0	1.1	0.3	3/10/2003	effective basin	2	4.2	632.0	20	BTpppK	80.0	11.4	2.7	3/11/2004	effective ba	2	1.3	275.7
20	BYpppI	140.0	18.7	4.7	3/11/2003	effective basin	2	-1.8	253.0	20	BYpppD	130.0	17.3	4.3	3/11/2004	effective ba	2	0.7	254.5
9	AC	190.0	27.1	6.3	3/12/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.2	197.0	20	BYpppE	130.0	17.3	4.3	3/11/2004	effective ba	2	-0.6	291.5
20	ATpppC	6.0	0.9	0.2	3/12/2003	effective basin	2	4.7	1107.0	20	BYpppF	130.0	17.3	4.3	3/11/2004	effective ba	2	-1.2	630.5
21	BCJ	42.0	6.0	1.4	3/12/2003	effective basin	1	-0.2	1711.0	20	BYpppG	130.0	17.3	4.3	3/11/2004	effective ba	2	3.6	12680.3
19	BMa	7.0	1.0	0.2	3/12/2003	effective basin	2	4.8	293.0	20	BYpppH	130.0	17.3	4.3	3/11/2004	effective ba	2	0.8	261.6
20	BMpppD	6.0	0.9	0.2	3/12/2003	effective basin	2	4.8	832.0	20	BMpppJ	18.0	2.6	0.6	3/12/2004	effective ba	2	5.0	3676.0
20	BTpppD	70.0	10.0	2.3	3/12/2003	effective basin	2	1.9	2264.0	20	BCh	17.0	2.4	0.6	3/13/2004	effective ba	1	1.5	147.0
20	BTpppE	70.0	10.0	2.3	3/12/2003	effective basin	2	1.3	2159.0	20	BMe	17.0	2.4	0.6	3/13/2004	effective ba	2	4.2	13926.3
20	BTpppF	70.0	10.0	2.3	3/12/2003	effective basin	2	0.7	999.0	20	BMpppE	8.0	1.1	0.3	3/15/2004	effective ba	1	8.1	363.0
20	BTpppG	70.0	10.0	2.3	3/12/2003	effective basin	2	0.1	1350.0	9	AD	150.0	21.4	5.0	3/15/2004	area 12 (sou	1	7.3	477.0
20	BTpppH	70.0	10.0	2.3	3/12/2003	effective basin	2	-0.5	1698.0	14	AF	120.0	17.1	4.0	3/15/2004	area 12 (sou	1	4.7	259.0
20	BTpppI	70.0	10.0	2.3	3/12/2003	effective basin	2	-1.1	3001.0	20	ATpppC	6.0	0.9	0.2	3/15/2004	effective ba	2	6.8	1944.0
21	BUpppI	120.0	16.0	4.0	3/12/2003	effective basin	2	-1.6	217.0	20	BCF	15.0	2.1	0.5	3/15/2004	effective ba	1	4.8	15192.3
20	BYpppA	120.0	17.1	4.0	3/12/2003	effective basin	2	5.8	912.5	20	BMpppD	6.0	0.9	0.2	3/15/2004	effective ba	2	1.7	1012.8
20	BYpppB	120.0	16.0	4.0	3/12/2003	effective basin	2	4.3	2394.0	20	BMpppI	15.0	2.1	0.5	3/15/2004	effective ba	2	-1.6	171.8
20	BYpppC	120.0	16.0	4.0	3/12/2003	effective basin	2	2.8	703.0	21	BUpppI	120.0	16.0	4.0	3/15/2004	effective ba	2	5.8	920.9
20	BYpppD	130.0	17.3	4.3	3/12/2003	effective basin	2	1.3	542.0	20	BYpppA	120.0	17.1	4.0	3/15/2004	effective ba	1	4.3	473.2
20	BYpppE	130.0	17.3	4.3	3/12/2003	effective basin	2	0.7	1949.0	20	BYpppB	120.0	16.0	4.0	3/15/2004	effective ba	2	2.8	307.1
20	BYpppF	130.0	17.3	4.3	3/12/2003	effective basin	2	0.0	2363.0	20	BYpppC	120.0	16.0	4.0	3/15/2004	effective ba	2	-3.3	331.2
20	BYpppG	130.0	17.3	4.3	3/12/2003	effective basin	2	-0.6	39.0	20	BYpppJ	150.0	20.0	5.0	3/15/2004	effective ba	2	6.7	320.0
20	BYpppH	130.0	17.3	4.3	3/12/2003	effective basin	2	-1.2	80.0	20	BZ	120.0	17.1	4.0	3/15/2004	effective ba	1	8.0	112.0
21	BZ	120.0	17.1	4.0	3/12/2003	effective basin	1	6.7	1019.0	8	AB	35.0	5.0	1.2	3/16/2004	west of rest	1	7.4	202.0
20	ATpppB	5.0	0.7	0.2	3/13/2003	effective basin	1	5.3	2708.0	11	AK	240.0	34.3	8.0	3/16/2004	@ E BC, east	1	5.3	2774.2
20	BMpppC	5.0	0.7	0.2	3/13/2003	effective basin	1	5.4	847.0	20	ATpppB	5.0	0.7	0.2	3/16/2004	effective ba	1	7.1	818.4
21	BUpppA	110.0	14.7	3.7	3/13/2003	effective basin	2	6.0	802.7	21	BCpppA	25.0	3.6	0.8	3/16/2004	effective ba	1	5.6	2325.1
21	BUpppB	110.0	14.7	3.7	3/13/2003	effective basin	2	4.5	2980.0	21	BCpppB	25.0	3.6	0.8	3/16/2004	effective ba	1	-0.5	5760.0
21	BUpppC	110.0	14.7	3.7	3/13/2003	effective basin	2	3.0	852.0	21	BE	35.0	5.0	1.2	3/16/2004	effective ba	2	5.4	15192.3
21	BUpppD	110.0	14.7	3.7	3/13/2003	effective basin	2	1.5	2216.0	20	BMpppC	5.0	0.7	0.2	3/16/2004	effective ba	2	-0.7	2869.7
21	BUpppE	110.0	14.7	3.7	3/13/2003	effective basin	2	0.9	2955.0	20	BMpppK	25.0	3.6	0.8	3/16/2004	effective ba	2	-0.1	2939.0
21	BUpppF	110.0	14.7	3.7	3/13/2003	effective basin	2	0.2	1933.0	20	BTg	70.0	10.0	2.3	3/16/2004	effective ba	2	-1.0	3196.0
21	BUpppG	110.0	14.7	3.7	3/13/2003	effective basin	2	-0.4	2038.0	20	BTh	70.0	10.0	2.3	3/16/2004	effective ba	2	1.9	3546.0
21	BUpppH	110.0	14.7	3.7	3/13/2003	effective basin	2	-1.0	988.0	20	BTpppD	70.0	10.0	2.3	3/16/2004	effective ba	2	1.3	3040.3
21	BUpppI	110.0	14.7	3.7	3/13/2003	effective basin	2	0.2	491.0	20	BTpppE	70.0	10.0	2.3	3/16/2004	effective ba	2	0.7	4229.3
20	BCd	40.0	5.7	1.3	3/14/2003	effective basin	2	0.2	957.0	20	BTpppF	70.0	10.0	2.3	3/16/2004	effective ba	2	0.1	4567.8
20	BCE	40.0	5.7	1.3	3/14/2003	effective basin	2	-1.6	892.0	20	BTpppG	70.0	10.0	2.3	3/16/2004	effective ba	2	-0.5	3133.7
21	BCpppD	40.0	5.7	1.3	3/14/2003	effective basin	2	2.6	5239.0	20	BTpppH	70.0	10.0	2.3	3/16/2004	effective ba	2	-1.1	3461.0
21	BCpppE	40.0	5.7	1.3	3/14/2003	effective basin	2	1.0	2922.0	20	BTpppI	70.0	10.0	2.3	3/16/2004	effective ba	2	-2.6	5222.8
21	BCpppF	40.0	5.7	1.3	3/14/2003	effective basin	2	0.4	1522.0	20	BTpppJ	75.0	10.7	2.5	3/16/2004	effective ba	2	-4.2	2029.8
21	BCpppG	40.0	5.7	1.3	3/14/2003	effective basin	2	-0.2	1163.0	20	BTpppK	80.0	11.4	2.7	3/16/2004	effective ba	2	-1.8	244.1
20	BTg	70.0	10.0	2.3	3/14/2003	effective basin	2	-0.1	938.0	20	BYpppI	140.0	18.7	4.7	3/16/2004	effective ba	2	8.6	174.0
20	BTh	70.0	10.0	2.3	3/14/2003	effective basin	2	-1.0	320.1	19	CB	240.0	34.3	8.0	3/16/2004	N of WB la	1	2.3	548.6
20	ATpppA	3.0	0.4	0.1	3/15/2003	effective basin	1	6.8	310.0	20	BMpppH	13.0	1.9	0.4	3/17/2004	effective ba	2	0.8	2616.5
20	BMpppB	3.0	0.4	0.1	3/15/2003	effective basin	1	6.0	2427.0	20	BMpppI	18.0	2.6	0.6	3/17/2004	effective ba	2	3.5	3222.8
20	BTpppK	80.0	11.4	2.7	3/15/2003	effective basin	2	-4.2	383.0	20	BTpppC	60.0	8.6	2.0	3/18/2004	effective ba	1	6.8	2305.0
11	AK	240.0	34.3	8.0	3/16/2003	@ E BC, east of median 13 area	1	7.4	2590.2	20	ATpppA	3.0	0.4	0.1	3/18/2004	effective ba	1	6.0	23210.5
22	BTpppA	420	56	14	3/16/2003	by back fence area, runoff b/w BK/BS	1	0.7	996.0	20	BMpppB	3.0	0.4	0.1	3/18/2004	effective ba	2	0.7	2139.0
20	BTf	68.0	9.7	2.3	3/16/2003	effective basin	1	8.6	283.0	20	BTf	68.0	9.7	2.3	3/19/2004	rest of bas	1	8.0	247.0
21	CB	240.0	34.3	8.0	3/16/2003	N of WB lane, near 4 UG wells across rd	1	7.3	1227.0	12	AJ	11.0	1.6	0.4	3/19/2004	effective ba	2	3.0	811.0
20	AT	2.0	0.3	0.1	3/17/2003	effective basin	1	6.9	1102.7	20	BMc	11.0	1.6	0.4	3/19/2004	effective ba	2	2.9	8440.2
20	BMpppA	1.0	0.1	0.0	3/17/2003	effective basin	2	-3.7	2016.0	20	BMpppG	11.0	1.5	4	3/19/2004	effective ba	1	6.0	704.0
20	BTj	90.0	12.9	3.0	3/17/2003	effective basin	2	-1.6	196.0	21	BUpppA	110	15	4	3/19/2004	effective ba	2	4.5	601.3
21	BUpppI	120.0	16.0	4.0	3/18/2003	effective basin	1	5.8	782.6	21	BUpppB	110	15	4	3/19/2004	effective ba	2	3.0	458.2
20	BYpppA	120.0	17.1	4.0	3/18/2003	effective basin	2	4.3	472.0	21	BUpppC	110	15	4	3/19/2004	effective ba	2	1.5	214.7
20	BYpppB	120.0	16.0	4.0	3/18/2003	effective basin	2	2.8	1273.0	21	BUpppD	110	15	4	3/19/2004	effective ba	2	0.9	216.1
20	BYpppC	120.0	16.0	4.0	3/18/2003	effective basin	2	8.4	341.0	21	BUpppE	110	15	4	3/19/2004	effective ba	2	0.2	2173.5
7	AA	160	23	5	3/19/2003	rest area	1	-0.5	3179.0	21	BUpppF	110	15	4	3/19/2004	effective ba	2	-0.4	195.5
21	BE	35.0	5.0	1.2	3/19/2003	effective basin	1	5.4	875.0	21	BUpppG	110	15	4	3/19/2004	effective ba	2	-1.0	162.7
21	BTa	65.0	9.3	2.2	3/19/2003	effective basin													

Travel time										Sampling d		SpecCond	Travel time										Sampling d		SpecCond
Row	Well	days	wks	mos	origin date	Origin	Layer #			m above msl	uS/cm	Row	Well	days	wks	mos	origin date	Origin	Layer #			m above msl	uS/cm		
20	BYppA	120.0	17.1	4.0	7/2/2003	effective basin	1			5.8	471.1	19	BCJ	42.0	6.0	1.4	6/1/2004	effective ba	2			-0.2	508.0		
20	BYppB	120.0	16.0	4.0	7/2/2003	effective basin	2			4.3	806.3	20	BMppB	3.0	0.4	0.1	6/1/2004	effective ba	1			6.0	1603.6		
20	BYppC	120.0	16.0	4.0	7/2/2003	effective basin	2			2.8	321.0	20	BMppH	13.0	1.9	0.4	6/1/2004	effective ba	2			2.3	3122.9		
21	BZ	120.0	17.1	4.0	7/2/2003	effective basin	1			6.7	631.0	20	BTppK	80.0	11.4	2.7	6/1/2004	effective ba	2			-4.2	162.3		
19	BMa	7.0	1.0	0.2	7/3/2003	effective basin	1			4.8	938.0	21	BUppA	110.0	14.7	3.7	6/1/2004	effective ba	1			6.0	335.0		
20	BMppH	13.0	1.9	0.4	7/3/2003	effective basin	2			2.3	583.0	21	BUppB	110.0	14.7	3.7	6/1/2004	effective ba	2			4.5	799.0		
12	AG	130.0	18.6	4.3	7/4/2003	area 12 (south shoulder of EB lane)	1			7.3	266.0	21	BUppC	110.0	14.7	3.7	6/1/2004	effective ba	2			3.0	970.2		
10	AI	200.0	28.6	6.7	7/4/2003	b/w areas 6/16, N of ramp, S of shoulder	1			8.1	290.0	21	BUppD	110.0	14.7	3.7	6/1/2004	effective ba	2			1.5	1309.4		
20	ATppC	6.0	0.9	0.2	7/4/2003	effective basin	2			4.7	949.0	21	BUppE	110.0	14.7	3.7	6/1/2004	effective ba	2			0.9	1076.4		
21	BCppA	25.0	3.6	0.8	7/4/2003	effective basin	1			7.1	298.4	21	BUppF	110.0	14.7	3.7	6/1/2004	effective ba	2			0.2	1520.8		
21	BCppB	25	4	1	7/4/2003	effective basin	1			5.6	965.0	21	BUppG	110.0	14.7	3.7	6/1/2004	effective ba	2			-0.4	872.9		
20	BMppD	6.0	0.9	0.2	7/4/2003	effective basin	2			4.8	3842.0	21	BUppH	110.0	14.7	3.7	6/1/2004	effective ba	2			-1.0	359.2		
20	BMppK	25.0	3.6	0.8	7/4/2003	effective basin	2			-0.7	118.0	20	BYppD	130.0	17.3	4.3	6/1/2004	effective ba	2			1.3	1526.3		
20	BTppC	60.0	8.6	2.0	7/4/2003	effective basin	2			3.5	1337.0	20	BYppE	130.0	17.3	4.3	6/1/2004	effective ba	2			0.7	1647.0		
20	BYppD	130.0	17.3	4.3	7/4/2003	effective basin	2			1.3	492.9	20	BYppF	130.0	17.3	4.3	6/1/2004	effective ba	2			0.0	1655.4		
20	BYppE	130.0	17.3	4.3	7/4/2003	effective basin	2			0.7	517.7	20	BYppG	130.0	17.3	4.3	6/1/2004	effective ba	2			-0.6	47.7		
20	BYppF	130.0	17.3	4.3	7/4/2003	effective basin	2			0.0	530.5	20	BYppH	130.0	17.3	4.3	6/1/2004	effective ba	2			-1.2	837.9		
20	BYppG	130.0	17.3	4.3	7/4/2003	effective basin	2			-0.6	20.1	19	BCa	20.0	2.9	0.7	6/2/2004	effective ba	1			6.0	939.0		
20	BYppH	130.0	17.3	4.3	7/4/2003	effective basin	2			-1.2	530.7	19	BCb	20.0	2.9	0.7	6/2/2004	effective ba	2			3.6	1217.0		
20	ATppB	5.0	0.7	0.2	7/5/2003	effective basin	1			5.3	5472.0	20	BCc	20.0	2.9	0.7	6/2/2004	effective ba	2			2.0	802.0		
20	BMppC	5.0	0.7	0.2	7/5/2003	effective basin	1			5.4	2284.0	21	BD	20.0	2.9	0.7	6/2/2004	effective ba	1			5.6	563.0		
20	BMppG	11.0	1.6	0.4	7/5/2003	effective basin	2			2.9	1129.0	10	AI	200.0	28.6	6.7	6/3/2004	b/w areas t	1			8.1	234.0		
20	BMppI	15.0	2.1	0.5	7/5/2003	effective basin	2			1.7	674.0	9	BCd	40.0	5.7	1.3	6/3/2004	effective ba	2			0.2	1548.0		
20	BTppJ	75.0	10.7	2.5	7/5/2003	effective basin	2			-2.6	196.7	9	BCe	40.0	5.7	1.3	6/3/2004	effective ba	2			-1.6	928.0		
15	AO	50	7	2	7/7/2003	near BO cluster, not "effective" area	1			8.2	175.0	21	BCppD	40.0	5.7	1.3	6/3/2004	effective ba	2			2.6	867.0		
20	ATppA	3.0	0.4	0.1	7/7/2003	effective basin	1			6.8	1186.2	21	BCppE	40.0	5.7	1.3	6/3/2004	effective ba	2			1.0	2448.9		
21	BCppH	50.0	7.1	1.7	7/7/2003	effective basin	2			-0.8	129.5	21	BCppF	40.0	5.7	1.3	6/3/2004	effective ba	2			0.4	1954.6		
21	BCppI	50.0	7.1	1.7	7/7/2003	effective basin	2			-1.4	97.9	21	BCppG	40.0	5.7	1.3	6/3/2004	effective ba	2			-0.2	2553.5		
21	BCppJ	50.0	7.1	1.7	7/7/2003	effective basin	2			-2.0	104.5	20	BMppA	1.0	0.1	0.0	6/3/2004	effective ba	1			6.9	1181.6		
20	BMppB	3.0	0.4	0.1	7/7/2003	effective basin	1			6.0	1231.0	20	BMppG	11.0	1.6	0.4	6/3/2004	effective ba	2			2.9	3376.1		
20	BMppF	9.0	1.3	0.3	7/7/2003	effective basin	2			3.6	1878.0	9	BTg	70.0	10.0	2.3	6/3/2004	effective ba	2			-0.1	422.0		
20	BMppH	13.0	1.9	0.4	7/7/2003	effective basin	2			2.3	369.0	21	BTh	70.0	10.0	2.3	6/3/2004	effective ba	2			-1.0	565.0		
20	BTk	50	7	2	7/7/2003	effective basin	1			7.3	483.0	20	BTppD	70.0	10.0	2.3	6/3/2004	effective ba	2			1.9	1357.9		
20	BTppA	50.0	7.1	1.7	7/7/2003	effective basin	1			6.5	378.9	20	BTppE	70.0	10.0	2.3	6/3/2004	effective ba	2			1.3	1594.4		
20	BTppB	50.0	7.1	1.7	7/7/2003	effective basin	2			5.0	642.1	20	BTppF	70.0	10.0	2.3	6/3/2004	effective ba	2			0.7	670.5		
20	BYppJ	150.0	20.0	5.0	7/7/2003	effective basin	2			-3.3	183.5	20	BTppG	70.0	10.0	2.3	6/3/2004	effective ba	2			0.1	484.3		
20	AT	2.0	0.3	0.1	7/8/2003	effective basin	1			7.3	1117.0	20	BTppH	70.0	10.0	2.3	6/3/2004	effective ba	2			-0.5	658.6		
20	BMppE	8.0	1.1	0.3	7/8/2003	effective basin	2			4.2	3264.0	20	BTppI	70.0	10.0	2.3	6/3/2004	effective ba	2			-1.1	858.7		
20	BMppA	1.0	0.1	0.0	7/9/2003	effective basin	1			6.9	790.8	7	AA	160.0	22.9	5.3	6/4/2004	rest area	1			8.4	NM		
20	BMppG	11.0	1.6	0.4	7/9/2003	effective basin	2			2.9	1273.0	20	BMppJ	18.0	2.6	0.6	6/4/2004	effective ba	2			0.8	362.9		
20	ATppC	6.0	0.9	0.2	7/10/2003	effective basin	2			4.7	536.0	20	BTppC	60.0	8.6	2.0	6/4/2004	effective ba	2			3.5	714.0		
20	BMppD	6.0	0.9	0.2	7/10/2003	effective basin	2			4.8	3298.0	20	CA	160.0	22.9	5.3	6/4/2004	rest area, r	1			6.1	327.0		
20	BTg	70.0	10.0	2.3	7/10/2003	effective basin	2			-0.1	160.0	20	BCh	17.0	2.4	0.6	6/5/2004	effective ba	1			5.0	883.0		
20	BTh	70.0	10.0	2.3	7/10/2003	effective basin	2			-1.0	142.0	20	BMe	17.0	2.4	0.6	6/5/2004	effective ba	2			1.5	220.0		
20	BTppD	70.0	10.0	2.3	7/10/2003	effective basin	2			1.9	877.8	20	BMppF	9.0	1.3	0.3	6/5/2004	effective ba	2			3.6	2658.7		
20	BTppE	70.0	10.0	2.3	7/10/2003	effective basin	2			1.3	294.1	22	BTf	68.0	9.7	2.3	6/5/2004	effective ba	2			0.7	641.0		
20	BTppF	70.0	10.0	2.3	7/10/2003	effective basin	2			0.7	192.1	20	BMppE	8.0	1.1	0.3	6/6/2004	effective ba	2			4.2	5908.1		
20	BTppG	70.0	10.0	2.3	7/10/2003	effective basin	2			0.1	301.0	20	BTppJ	75.0	10.7	2.5	6/6/2004	effective ba	2			-2.6	214.3		
20	BTppH	70.0	10.0	2.3	7/10/2003	effective basin	2			-0.5	175.5	20	BCf	15.0	2.1	0.5	6/7/2004	effective ba	1			6.8	1075.0		
20	BTppI	70.0	10.0	2.3	7/10/2003	effective basin	2			-1.1	206.8	21	BCppC	30	4	1	6/7/2004	effective ba	2			4.1	916.3		
7	AA	160	23	5	7/11/2003	rest area	1			8.4	NS	20	BMppI	15.0	2.1	0.5	6/7/2004	effective ba	2			1.7	2194.4		
20	ATppB	5.0	0.7	0.2	7/11/2003	effective basin	1			5.3	5392.0	8	AB	35.0	5.0	1.2	6/8/2004	west of rest	1			8.0	316.0		
22	BTppA	420.0	56.0	14.0	7/11/2003	by back fence area, runoff b/w BK/BS	1			6.0	2431.6	20	ATppC	6.0	0.9	0.2	6/8/2004	effective ba	2			4.7	570.9		
20	BMppC	5.0	0.7	0.2	7/11/2003	effective basin	1			5.4	2915.														

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
14	AF	120.0	17.1	4.0	7/14/2003	area 12 (south shoulder of EB lane)	1	7.3	100.0	21	BCpppG	40.0	5.7	1.3	6/9/2004	effective ba	2	-0.2	2243.9
20	ATpppC	6.0	0.9	0.2	7/14/2003	effective basin	2	4.7	441.0	20	BMpppC	5.0	0.7	0.2	6/9/2004	effective ba	1	5.4	5908.1
21	BCpppH	50.0	7.1	1.7	7/14/2003	effective basin	2	-0.8	308.2	20	BMpppH	13.0	1.9	0.4	6/9/2004	effective ba	2	2.3	1814.6
21	BCpppI	50.0	7.1	1.7	7/14/2003	effective basin	2	-1.4	108.2	20	BYpppI	150.0	20.0	5.0	6/9/2004	effective ba	2	-3.3	906.4
21	BCpppJ	50.0	7.1	1.7	7/14/2003	effective basin	2	-2.0	102.3	12	AI	11.0	1.6	0.4	6/11/2004	crest of bas	1	8.0	639.0
20	BMpppD	6.0	0.9	0.2	7/14/2003	effective basin	2	4.8	3051.0	20	ATpppA	3.0	0.4	0.1	6/11/2004	effective ba	1	6.8	1926.4
20	BMpppI	15.0	2.1	0.5	7/14/2003	effective basin	2	1.7	519.0	20	BMc	11.0	1.6	0.4	6/11/2004	effective ba	2	3.0	162.0
20	BTpppA	50.0	7.1	1.7	7/14/2003	effective basin	1	6.5	327.1	20	BMpppB	3.0	0.4	0.1	6/11/2004	effective ba	1	6.0	2321.1
20	BTpppB	50.0	7.1	1.7	7/14/2003	effective basin	2	5.0	582.2	20	BMpppD	11.0	1.6	0.4	6/11/2004	effective ba	2	2.9	1983.4
21	BUpppI	120.0	16.0	4.0	7/14/2003	effective basin	1	-1.6	260.8	20	BTpppD	70.0	10.0	2.3	6/11/2004	effective ba	2	1.9	1461.1
20	BYpppA	120.0	17.1	4.0	7/14/2003	effective basin	2	5.8	833.4	20	BTpppE	70.0	10.0	2.3	6/11/2004	effective ba	2	1.3	1688.4
20	BYpppB	120.0	16.0	4.0	7/14/2003	effective basin	2	4.3	541.3	20	BTpppF	70.0	10.0	2.3	6/11/2004	effective ba	2	0.7	698.6
20	BYpppC	120.0	16.0	4.0	7/14/2003	effective basin	2	2.8	489.5	20	BTpppG	70.0	10.0	2.3	6/11/2004	effective ba	2	0.1	574.7
21	BZ	120.0	17.1	4.0	7/14/2003	effective basin	1	6.7	626.0	20	BTpppH	70.0	10.0	2.3	6/11/2004	effective ba	2	-0.5	419.7
20	ATpppB	5.0	0.7	0.2	7/15/2003	effective basin	1	5.3	563.0	20	BTpppI	70.0	10.0	2.3	6/11/2004	effective ba	2	-1.1	941.6
21	BCJ	42	6	1	7/15/2003	effective basin	2	-0.2	108.0	21	BUpppI	120.0	16.0	4.0	6/11/2004	effective ba	2	-1.6	1141.4
20	BMpppA	1.0	0.1	0.0	7/15/2003	effective basin	1	6.9	842.8	20	BYpppA	120.0	17.1	4.0	6/11/2004	effective ba	1	5.8	404.1
20	BMpppC	5.0	0.7	0.2	7/15/2003	effective basin	1	5.4	3186.0	20	BYpppB	120.0	16.0	4.0	6/11/2004	effective ba	2	4.3	547.7
21	BTa	65.0	9.3	2.2	7/15/2003	effective basin	1	5.4	234.0	21	BYpppC	120.0	16.0	4.0	6/11/2004	effective ba	2	2.8	1464.9
21	BTb	65.0	9.3	2.2	7/15/2003	effective basin	2	4.4	205.0	21	BCpppB	25	4	1	6/12/2004	effective ba	1	7.1	880.0
21	BTc	65.0	9.3	2.2	7/15/2003	effective basin	2	3.6	205.0	21	BCpppB	25	4	1	6/12/2004	effective ba	1	5.6	1470.0
21	BTd	65.0	9.3	2.2	7/15/2003	effective basin	2	2.7	206.0	19	BMd	10.0	1.4	0.3	6/12/2004	effective ba	2	2.1	770.0
20	BTf	65.0	9.3	2.2	7/15/2003	effective basin	2	1.7	137.0	20	BMpppK	25	4	1	6/12/2004	effective ba	2	-0.7	151.9
20	BMpppH	13	2	0	7/16/2003	effective basin	2	2.3	1107.0	19	BN	10.0	1.4	0.3	6/12/2004	effective ba	2	1.8	2231.0
20	ATpppA	3.0	0.4	0.1	7/17/2003	effective basin	1	6.8	988.1	9	AC	190.0	27.1	6.3	6/13/2004	b/w areas t	1	8.2	106.0
20	BCd	40	6	1	7/17/2003	effective basin	2	0.2	194.0	18	AP	30.0	4.3	1.0	6/13/2004	effective ba	1	8.0	950.0
20	BCe	40	6	1	7/17/2003	effective basin	2	-1.6	135.0	22	BCI	30.0	4.3	1.0	6/13/2004	effective ba	2	1.1	653.0
21	BCpppD	40.0	5.7	1.3	7/17/2003	effective basin	2	2.6	1140.8	21	BCpppC	30.0	4.3	1.0	6/13/2004	effective ba	2	4.1	1256.1
21	BCpppE	40.0	5.7	1.3	7/17/2003	effective basin	2	1.0	259.5	20	BG	30.0	4.3	1.0	6/13/2004	effective ba	1	7.6	576.0
21	BCpppF	40.0	5.7	1.3	7/17/2003	effective basin	2	0.4	245.3	20	BMb	9.0	1.3	0.3	6/13/2004	effective ba	2	3.9	1521.0
21	BCpppG	40.0	5.7	1.3	7/17/2003	effective basin	2	-0.2	245.9	20	BMpppA	1.0	0.1	0.0	6/13/2004	effective ba	1	6.9	1772.4
20	BMpppB	3.0	0.4	0.1	7/17/2003	effective basin	1	6.0	1759.0	20	BMpppF	9.0	1.3	0.3	6/13/2004	effective ba	2	3.6	1266.0
20	BYpppI	140.0	18.7	4.7	7/17/2003	effective basin	2	-1.8	237.7	20	BTpppC	60.0	8.6	2.0	6/13/2004	effective ba	2	3.5	825.6
20	BMpppG	11.0	1.6	0.4	7/18/2003	effective basin	2	2.9	480.0	9	AD	150.0	21.4	5.0	6/14/2004	b/w areas t	1	8.1	NM
20	BMpppA	1.0	0.1	0.0	7/19/2003	effective basin	1	6.9	1077.9	21	BCpppH	50.0	7.1	1.7	6/14/2004	effective ba	2	-0.8	211.7
20	BMpppF	9.0	1.3	0.3	7/20/2003	effective basin	2	3.6	817.0	21	BCpppI	50.0	7.1	1.7	6/14/2004	effective ba	2	-1.4	233.9
20	BTpppC	60.0	8.6	2.0	7/20/2003	effective basin	2	3.5	1150.0	21	BCpppJ	50.0	7.1	1.7	6/14/2004	effective ba	2	-2.0	208.6
9	AD	150	21	5	7/21/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	NM	20	BMpppE	8.0	1.1	0.3	6/14/2004	effective ba	2	4.2	3460.5
20	BMpppE	8.0	1.1	0.3	7/21/2003	effective basin	1	4.2	2030.0	20	BTpppA	50.0	7.1	1.7	6/14/2004	effective ba	1	6.5	975.9
20	BYpppI	150.0	20.0	5.0	7/21/2003	effective basin	2	-3.3	149.3	20	BTpppB	50.0	7.1	1.7	6/14/2004	effective ba	2	5.0	1107.0
8	AB	35	5	1	7/22/2003	west of rest area, runoff slope	1	8.0	450.0	20	BYpppJ	150.0	20.0	5.0	6/15/2004	effective ba	2	-3.3	1120.4
21	BE	35	5	1	7/22/2003	effective basin	2	-0.5	213.0	19	BMa	7.0	1.0	0.2	6/15/2004	effective ba	1	4.8	1724.0
20	ATpppC	6.0	0.9	0.2	7/23/2003	effective basin	2	4.7	683.0	20	BTpppK	80.0	11.4	2.7	6/15/2004	effective ba	2	-4.2	364.0
20	BMpppD	6.0	0.9	0.2	7/24/2003	effective basin	2	4.8	2358.0	20	ATpppC	6.0	0.9	0.2	6/16/2004	effective ba	2	4.7	715.8
20	ATpppB	5	1	0	7/24/2003	effective basin	1	5.3	2784.0	20	BMpppD	6.0	0.9	0.2	6/16/2004	effective ba	2	4.8	5064.1
21	BCpppD	40.0	5.7	1.3	7/24/2003	effective basin	2	2.6	389.2	20	ATpppB	5.0	0.7	0.2	6/17/2004	effective ba	1	5.3	5455.8
21	BCpppE	40.0	5.7	1.3	7/24/2003	effective basin	2	1.0	270.2	20	ATpppC	5.0	0.7	0.2	6/17/2004	effective ba	1	5.4	5064.1
21	BCpppF	40.0	5.7	1.3	7/24/2003	effective basin	2	0.4	232.4	12	AG	130.0	18.6	4.3	6/18/2004	area 12 (sou	1	7.3	617.0
21	BCpppG	40.0	5.7	1.3	7/24/2003	effective basin	2	-0.2	429.2	18	BCg	25.0	3.6	0.8	6/18/2004	effective ba	2	2.9	112.0
20	BMpppC	5.0	0.7	0.2	7/24/2003	effective basin	1	5.4	2963.0	21	BCpppA	25.0	3.6	0.8	6/18/2004	effective ba	1	7.1	1111.4
21	BUpppA	110.0	14.7	3.7	7/24/2003	effective basin	1	6.0	611.2	21	BCpppB	25.0	3.6	0.8	6/18/2004	effective ba	1	5.6	1521.0
21	BUpppB	110.0	14.7	3.7	7/24/2003	effective basin	2	4.5	703.7	21	BCpppD	40.0	5.7	1.3	6/18/2004	effective ba	2	2.6	2484.5
21	BUpppC	110.0	14.7	3.7	7/24/2003	effective basin	2	3.0	842.9	21	BCpppE	40.0	5.7	1.3	6/18/2004	effective ba	2	1.0	1656.3
21	BUpppD	110.0	14.7	3.7	7/24/2003	effective basin	2	1.5	356.0	21	BCpppF	40.0	5.7	1.3	6/18/2004	effective ba	2	0.4	1356.0
21	BUpppE	110.0	14.7	3.7	7/24/2003	effective basin	2	0.9	335.8	21	BCpppG	40.0	5.7	1.3	6/18/2004	effective ba	2	-0.2	924.7
21	BUpppF	110.0	14.7	3.7	7/24/2003	effective basin	2	0.2	344.1	20	BMpppK	25.0	3.6	0.8	6/18/2004	effective ba	2	-0.7	169.8
21	BUpppG	110.0	14.7	3.7	7/24/2003	effective basin	2	-0.4	175.4	20	BMpppD	130.0	17.3	4.3	6/18/2004	effective ba	2	1.3	1182.5
21	BUpppH	110.0	14.7	3.7	7/24/2003	effective basin	2	-1.0	144.5	20	BYpppE	130.0	17.3	4.3	6/18/2004	effective ba	2	0.7	1359.6
20	ATpppA	3.0	0.4	0.1	7/26/2003	effective basin	1	6.8	713.9	20	BYpppF	130.0	17.3	4.3	6/18/2004	effective ba	2	0.0	1522.7
20	BMpppB	3.0	0.4	0.1	7/26/2003	effective basin	1	6.0	1619.0	20	BYpppG	130.0	17.3	4.3	6/18/2004	effective ba	2	-0.6	111.1
18	AP	30	4	1	7/27/2003	effective basin	1	8.0	345.0	20	BYpppH	130.0	17.3	4.3	6/18/2004	effective ba	2	-1.2	1113.9
20	BCI	30	4	1	7/27/2003	effective basin	2	1.1	183.0	20	ATpppA	3.0	0.4	0.1	6/19/2004	effective ba	1	6.8	1792.4
21	BCpppC	30.0	4.3	1.0	7/27/2003	effective basin	2	4.1	465.9	20	BCpppC	30.0	4.3	1.0	6/19/2004	effective ba	2	4.1	1397.0
22	BG	30	4	1	7/27/2003	N of WB lane, near 4 UG wells across rd	1	7.6	595.0	20	BMpppB	3.0	0.4	0.1	6/19/2004	effective ba	1	6.0	2363.3
22	BlpppA	420.0	56.0	14.0	7/27/2003	by back fence area, runoff b/w BK/BS	1	6.0	2177.4	20	BMpppC	18	3	1	6/19/2004	effective ba	2	0.8	244.8
20	BYpppD	130.0	17.3	4.3	7/27/2003	effective basin	2	1.3	241.2	20	BYpppI	140.0	18.7	4.7	6/19/2004	effective ba	2	-1.8	774.3
20	BYpppE	130.0	17.3	4.3	7/27/2003	effective basin	2	0.7	238.5	20	AT	2.0	0.3	0.1	6/20/2004	effective ba	1	7.3	1254.0
20	BYpppF	130.0	17.3	4.3	7/27/2003	effective basin	-2	0.0	235.2	20	BTpppI	75.0	10.7	2.5	6/20/2004	effective ba	2	-2.6	336.3
20	BYppp																		

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
24	AR	300.0	42.9	10.0	8/27/2003	N of WB lane, N of median 8	1	8.1	902.0	20	BTpppG	70.0	10.0	2.3	7/11/2004	effective ba	2	0.1	1555.1
21	BCpppH	50.0	7.1	1.7	8/27/2003	effective basin	2	-0.8	165.1	20	BTpppH	70.0	10.0	2.3	7/11/2004	effective ba	2	-0.5	1195.6
21	BCpppI	50.0	7.1	1.7	8/27/2003	effective basin	2	-1.4	122.9	20	BTpppI	70.0	10.0	2.3	7/11/2004	effective ba	2	-1.1	987.3
21	BCpppJ	50.0	7.1	1.7	8/27/2003	effective basin	2	-2.0	138.1	20	BMpppA	1.0	0.1	0.0	7/12/2004	effective ba	1	6.9	2110.0
20	BMpppD	6.0	0.9	0.2	8/27/2003	effective basin	2	4.8	2067.8	18	AP	30.0	4.3	1.0	7/13/2004	effective ba	1	8.0	609.0
20	BTpppA	50.0	7.1	1.7	8/27/2003	effective basin	1	6.5	355.2	20	ATpppC	6.0	0.9	0.2	7/13/2004	effective ba	2	4.7	349.2
20	BTpppB	50.0	7.1	1.7	8/27/2003	effective basin	2	5.0	545.1	22	BCI	30.0	4.3	1.0	7/13/2004	effective ba	2	1.1	353.0
20	BMpppC	5.0	0.7	0.2	8/28/2003	effective basin	1	5.4	2743.1	21	BCpppC	30.0	4.3	1.0	7/13/2004	effective ba	2	4.1	1155.9
20	BTpppJ	75.0	10.7	2.5	8/28/2003	effective basin	2	-2.6	177.3	20	BG	30.0	4.3	1.0	7/13/2004	N of WB la	1	7.6	525.0
19	BCa	20.0	2.9	0.7	8/29/2003	effective basin	1	6.0	674.0	20	BMpppD	6.0	0.9	0.2	7/13/2004	effective ba	2	4.8	1688.0
19	BCb	20.0	2.9	0.7	8/29/2003	effective basin	2	3.6	702.0	20	BMpppI	15.0	2.1	0.5	7/13/2004	effective ba	2	1.7	1265.0
20	BCc	20.0	2.9	0.7	8/29/2003	effective basin	2	2.0	128.0	20	CA	160.0	22.9	5.3	7/13/2004	rest area, N	1	6.1	315.0
21	BD	20.0	2.9	0.7	8/29/2003	effective basin	1	5.6	410.0	14	AF	120.0	17.1	4.0	7/14/2004	area 12 (son	1	7.3	130.0
20	BYpppD	130.0	17.3	4.3	8/29/2003	effective basin	2	1.3	209.1	20	ATpppB	5.0	0.7	0.2	7/14/2004	effective ba	1	5.3	2856.6
20	BYpppE	130.0	17.3	4.3	8/29/2003	effective basin	2	0.7	181.3	20	BMpppC	5.0	0.7	0.2	7/14/2004	effective ba	1	5.4	1941.2
20	BYpppF	130.0	17.3	4.3	8/29/2003	effective basin	2	0.0	221.2	21	BUpppI	120.0	16.0	4.0	7/14/2004	effective ba	2	-1.6	339.1
20	BYpppG	130.0	17.3	4.3	8/29/2003	effective basin	2	-0.6	11.7	20	BYpppA	120.0	17.1	4.0	7/14/2004	effective ba	1	5.8	390.8
20	BYpppH	130.0	17.3	4.3	8/29/2003	effective basin	2	-1.2	224.6	20	BYpppB	120.0	16.0	4.0	7/14/2004	effective ba	2	4.3	561.8
20	BMpppB	3.0	0.4	0.1	8/30/2003	effective basin	1	-6.0	1519.2	20	BYpppC	120.0	16.0	4.0	7/14/2004	effective ba	2	2.8	1014.2
21	BUpppA	110.0	14.7	3.7	8/30/2003	effective basin	1	-6.0	837.1	20	BYpppD	130.0	17.3	4.3	7/14/2004	effective ba	2	1.3	592.6
21	BUpppB	110.0	14.7	3.7	8/30/2003	effective basin	2	4.5	722.3	20	BYpppE	130.0	17.3	4.3	7/14/2004	effective ba	2	0.7	599.6
21	BUpppC	110.0	14.7	3.7	8/30/2003	effective basin	2	3.0	448.8	20	BYpppF	130.0	17.3	4.3	7/14/2004	effective ba	2	0.0	900.6
21	BUpppD	110.0	14.7	3.7	8/30/2003	effective basin	2	1.5	282.6	20	BYpppG	130.0	17.3	4.3	7/14/2004	effective ba	2	-0.6	32.3
21	BUpppE	110.0	14.7	3.7	8/30/2003	effective basin	2	0.9	198.8	20	BYpppH	130.0	17.3	4.3	7/14/2004	effective ba	2	-1.2	860.3
21	BUpppF	110.0	14.7	3.7	8/30/2003	effective basin	2	0.2	287.5	20	BYpppI	150.0	20.0	5.0	7/14/2004	effective ba	2	-3.3	392.7
21	BUpppG	110.0	14.7	3.7	8/30/2003	effective basin	2	-0.4	172.9	20	BZ	120.0	17.1	4.0	7/14/2004	effective ba	1	6.7	297.0
21	BUpppH	110.0	14.7	3.7	8/30/2003	effective basin	2	-1.0	175.1	21	BCpppH	50.0	7.1	1.7	7/15/2004	effective ba	2	-0.8	937.2
20	BMpppI	18.0	2.6	0.6	8/31/2003	effective basin	2	0.8	337.6	21	BCpppI	50.0	7.1	1.7	7/15/2004	effective ba	2	-1.4	198.7
20	BTpppC	60.0	8.6	2.0	8/31/2003	effective basin	2	3.5	802.5	21	BCpppJ	50.0	7.1	1.7	7/15/2004	effective ba	2	-2.0	180.4
										20	BMpppH	13.0	1.9	0.4	7/15/2004	effective ba	2	2.3	1266.0
20	BCh	17.0	2.4	0.6	9/1/2003	effective basin	1	5.0	622.0	9	BTg	70.0	10.0	2.3	7/15/2004	effective ba	2	-1.0	1082.0
20	BMc	17.0	2.4	0.6	9/1/2003	effective basin	2	1.5	94.0	21	BTh	70.0	10.0	2.3	7/15/2004	effective ba	2	-1.0	408.0
20	BMpppA	1.0	0.1	0.0	9/1/2003	effective basin	1	6.9	928.4	20	BTpppA	50.0	7.1	1.7	7/15/2004	effective ba	1	6.5	743.8
14	AN	210.0	30.0	7.0	9/2/2003	area 12 (south shoulder of EB lane)	1	8.0	143.0	20	BTpppB	50.0	7.1	1.7	7/15/2004	effective ba	2	5.0	685.1
22	BTpppA	420.0	56.0	14.0	9/2/2003	by back fence area, runoff b/w BK/BS	1	6.0	858.2	20	ATpppA	3.0	0.4	0.1	7/16/2004	effective ba	1	6.8	1050.7
20	BTg	70.0	10.0	2.3	9/2/2003	effective basin	2	-0.1	347.0	20	BMpppB	3.0	0.4	0.1	7/16/2004	effective ba	1	6.0	1603.6
20	BTh	70.0	10.0	2.3	9/2/2003	effective basin	2	-1.0	207.0	20	BMpppI	18.0	2.6	0.6	7/16/2004	effective ba	2	0.8	212.0
20	BTpppD	70.0	10.0	2.3	9/2/2003	effective basin	2	1.9	547.7	20	BMpppG	11.0	1.6	0.4	7/17/2004	effective ba	2	2.9	590.8
20	BTpppE	70.0	10.0	2.3	9/2/2003	effective basin	2	1.3	419.7	22	BTf	65.0	9.7	2.3	7/17/2004	effective ba	2	0.7	844.0
20	BTpppF	70.0	10.0	2.3	9/2/2003	effective basin	2	0.7	315.5	18	BCg	25.0	3.6	0.8	7/18/2004	effective ba	2	2.9	549.0
20	BTpppG	70.0	10.0	2.3	9/2/2003	effective basin	2	-0.1	402.5	21	BCpppA	25.0	3.6	0.8	7/18/2004	effective ba	1	7.1	1173.3
20	BTpppH	70.0	10.0	2.3	9/2/2003	effective basin	2	-0.5	442.3	21	BCpppB	25.0	3.6	0.8	7/18/2004	effective ba	1	5.6	1079.6
20	BTpppI	70.0	10.0	2.3	9/2/2003	effective basin	2	-1.1	281.5	20	BMpppA	1.0	0.1	0.0	7/18/2004	effective ba	1	6.9	1350.4
20	BCf	15.0	2.1	0.5	9/3/2003	effective basin	1	6.8	580.0	20	BMpppK	25.0	3.6	0.8	7/18/2004	effective ba	2	-0.7	149.0
20	BMpppI	15.0	2.1	0.5	9/3/2003	effective basin	2	1.7	1097.2	20	BMpppF	9.0	1.3	0.3	7/19/2004	effective ba	2	3.6	590.8
20	BTf	68.0	9.7	2.3	9/4/2003	effective basin	2	0.7	190.0	20	BMpppI	15.0	2.1	0.5	7/19/2004	effective ba	2	1.7	1118.7
20	BYpppI	150.0	20.0	5.0	9/4/2003	effective basin	2	-3.3	198.6	21	BUpppA	110.0	14.7	3.7	7/19/2004	effective ba	1	6.0	451.5
20	BMpppH	13.0	1.9	0.4	9/5/2003	effective basin	2	2.3	1941.2	21	BUpppB	110.0	14.7	3.7	7/19/2004	effective ba	2	4.5	806.3
20	BYpppI	140.0	18.7	4.7	9/5/2003	effective basin	2	-1.8	175.7	21	BUpppC	110.0	14.7	3.7	7/19/2004	effective ba	2	3.0	481.5
21	BCpppD	40.0	5.7	1.3	9/6/2003	effective basin	2	2.6	442.4	21	BUpppD	110.0	14.7	3.7	7/19/2004	effective ba	2	1.5	806.3
21	BCpppE	40.0	5.7	1.3	9/6/2003	effective basin	2	1.0	392.7	21	BUpppE	110.0	14.7	3.7	7/19/2004	effective ba	2	0.9	954.0
21	BCpppF	40.0	5.7	1.3	9/6/2003	effective basin	2	0.4	283.3	21	BUpppF	110.0	14.7	3.7	7/19/2004	effective ba	2	0.2	877.4
21	BCpppG	40.0	5.7	1.3	9/6/2003	effective basin	2	-0.2	457.7	21	BUpppG	110.0	14.7	3.7	7/19/2004	effective ba	2	-0.4	861.6
12	AJ	11.0	1.6	0.4	9/7/2003	crest of basin, comes down slope	1	8.0	265.0	21	BUpppH	110.0	14.7	3.7	7/19/2004	effective ba	2	-1.0	346.7
20	BMc	11.0	1.6	0.4	9/7/2003	effective basin	2	3.0	538.0	20	BMpppE	8.0	1.1	0.3	7/20/2004	effective ba	2	4.2	928.4
20	BMpppG	11.0	1.6	0.4	9/7/2003	effective basin	2	2.9	1434.8	21	BTa	65.0	9.3	2.2	7/20/2004	effective ba	1	5.4	654.0
21	BTa	65.0	9.3	2.2	9/7/2003	effective basin	1	5.4	840.0	21	BTb	65.0	9.3	2.2	7/20/2004	effective ba	2	4.4	679.0
21	BTb	65.0	9.3	2.2	9/7/2003	effective basin	2	4.4	634.0	21	BTc	65.0	9.3	2.2	7/20/2004	effective ba	2	3.6	678.0
21	BTc	65.0	9.3	2.2	9/7/2003	effective basin	2	3.6	436.0	22	BTd	65.0	9.3	2.2	7/20/2004	effective ba	2	2.7	63.2
21	BTd	65.0	9.3	2.2	9/7/2003	effective basin	2	2.7	391.0	22	BTe	65.0	9.3	2.2	7/20/2004	effective ba	2	1.7	532.0
20	BTe	65.0	9.3	2.2	9/7/2003	effective basin	2	1.7	299.0	21	BCpppC	30.0	4.3	1.0	7/21/2004	effective ba	2	4.1	1259.2
19	BMd	10.0	1.4	0.3	9/8/2003	effective basin	2	2.1	364.0	20	BMpppH	13.0	1.9	0.4	7/21/2004	effective ba	2	2.3	336.0
19	BN	10.0	1.4	0.3	9/8/2003	effective basin	2	1.8	193.0	20	BTpppC	60.0	8.6	2.0	7/21/2004	effective ba	2	3.5	799.0
21	BUpppI	120.0	16.0	4.0	9/8/2003	effective basin	2	-1.6	160.9	20	BTpppK	80.0	11.4	2.7	7/21/2004	effective ba	2	-4.2	211.4
20	BYpppA	120.0	17.1	4.0	9/8/2003	effective basin	1	5.8	292.1	20	ATpppC	6.0	0.9	0.2	7/22/2004	effective ba	2	4.7	478.8
20	BYpppB	120.0	16.0	4.0	9/8/2003	effective basin	2	4.3	202.3	20	BMpppD	6.0	0.9	0.2	7/22/2004	effective ba	2	4.8	1772.4
20	BYpppC	120.0	16.0	4.0	9/8/2003	effective basin	2	2.8	196.8	9	AD	150.0	21.4	5.0	7/23/2004	b/w areas t	1	8.1	353.0
20	BMb	9.0	1.3	0.3	9/9/2003	effective basin	2	3.9	369.0	20	ATpppB	5.0	0.7	0.2	7/23/2004	effective ba	1	5.3	2783.3
20	BMpppF	9																	

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
21	BCppH	50.0	7.1	1.7	9/10/2003	effective basin	2	-0.8	196.5	18	BCC	20.0	2.9	0.7	7/23/2004	effective ba	2	2.0	256.0
21	BCppI	50.0	7.1	1.7	9/10/2003	effective basin	2	-1.4	122.9	19	BD	20.0	2.9	0.7	7/23/2004	effective ba	1	5.6	658.0
21	BCppJ	50.0	7.1	1.7	9/10/2003	effective basin	2	-2.0	135.4	20	BMppC	5.0	0.7	0.2	7/23/2004	effective ba	2	5.4	1434.8
20	BMppE	8.0	1.1	0.3	9/10/2003	effective basin	2	4.2	2447.7	20	BMppG	11.0	1.6	0.4	7/23/2004	effective ba	2	2.9	494.0
20	BTk	50.0	7.1	1.7	9/10/2003	effective basin	1	7.3	491.0	20	BYppJ	150.0	20.0	5.0	7/23/2004	effective ba	2	-3.3	302.6
20	BTppA	50.0	7.1	1.7	9/10/2003	effective basin	1	6.5	554.3	21	BUppA	110.0	14.7	3.7	7/24/2004	effective ba	1	6.0	362.9
20	BTppB	50.0	7.1	1.7	9/10/2003	effective basin	2	5.0	537.5	21	BUppB	110.0	14.7	3.7	7/24/2004	effective ba	2	4.5	454.8
19	BMA	7.0	1.0	0.2	9/11/2003	effective basin	1	4.8	603.0	21	BUppC	110.0	14.7	3.7	7/24/2004	effective ba	2	3.0	480.4
20	BYppJ	150.0	20.0	5.0	9/11/2003	effective basin	2	-3.3	172.6	21	BUppD	110.0	14.7	3.7	7/24/2004	effective ba	2	1.5	1087.7
12	AG	130.0	18.6	4.3	9/12/2003	area 12 (south shoulder of EB lane)	1	7.3	1260.0	21	BUppE	110.0	14.7	3.7	7/24/2004	effective ba	2	0.9	487.2
10	AI	200.0	28.6	6.7	9/12/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	367.0	21	BUppF	110.0	14.7	3.7	7/24/2004	effective ba	2	0.2	466.7
20	ATppC	6.0	0.9	0.2	9/12/2003	effective basin	2	4.7	517.5	21	BUppG	110.0	14.7	3.7	7/24/2004	effective ba	2	-0.4	386.1
20	BMppD	6.0	0.9	0.2	9/12/2003	effective basin	2	4.8	2152.2	21	BUppH	110.0	14.7	3.7	7/24/2004	effective ba	2	-1.0	501.3
20	BTppC	60.0	8.6	2.0	9/12/2003	effective basin	2	3.5	652.6	21	BUppI	120.0	16.0	4.0	7/24/2004	effective ba	2	-1.6	266.9
20	ATppB	5.0	0.7	0.2	9/13/2003	effective basin	1	5.3	3100.6	20	BYppA	120.0	17.1	4.0	7/24/2004	effective ba	1	5.8	400.5
22	BlppA	420.0	56.0	14.0	9/13/2003	by back fence area, runoff b/w BK/BS	1	6.0	1504.9	20	BYppB	120.0	16.0	4.0	7/24/2004	effective ba	2	4.3	528.0
20	BMppC	5.0	0.7	0.2	9/13/2003	effective basin	1	5.4	1941.2	20	BYppC	120.0	16.0	4.0	7/24/2004	effective ba	2	2.8	430.0
20	BYppI	140.0	18.7	4.7	9/14/2003	effective basin	2	-1.8	172.8	20	ATppA	3.0	0.4	0.1	7/25/2004	effective ba	2	-1.8	512.4
20	ATppA	3.0	0.4	0.1	9/15/2003	effective basin	1	6.8	815.8	20	ATppB	40.0	5.7	1.3	7/25/2004	effective ba	1	6.8	845.7
20	BMppB	3.0	0.4	0.1	9/15/2003	effective basin	1	6.0	633.0	21	BCppD	40.0	5.7	1.3	7/25/2004	effective ba	2	2.6	882.0
20	BYppK	80.0	11.4	2.7	9/15/2003	effective basin	2	-4.2	123.0	21	BCppE	40.0	5.7	1.3	7/25/2004	effective ba	2	1.0	912.5
20	BYppD	130.0	17.3	4.3	9/15/2003	effective basin	2	1.3	251.0	21	BCppF	40.0	5.7	1.3	7/25/2004	effective ba	2	0.4	1121.6
20	BYppE	130.0	17.3	4.3	9/15/2003	effective basin	2	0.7	215.4	21	BCppG	40.0	5.7	1.3	7/25/2004	effective ba	2	-0.2	1561.9
20	BYppF	130.0	17.3	4.3	9/15/2003	effective basin	2	0.0	250.1	20	BMppB	3.0	0.4	0.1	7/25/2004	effective ba	1	6.0	1434.8
20	BYppG	130.0	17.3	4.3	9/15/2003	effective basin	2	-0.6	15.1	20	BMppF	9.0	1.3	0.3	7/25/2004	effective ba	2	3.6	521.0
20	BTppH	130.0	17.3	4.3	9/15/2003	effective basin	2	-1.2	215.0	20	BMppI	18.0	2.6	0.6	7/25/2004	effective ba	2	0.8	192.1
20	AT	2.0	0.3	0.1	9/16/2003	effective basin	1	7.3	524.0	19	BCH	17.0	2.4	0.6	7/26/2004	effective ba	1	5.0	901.0
21	BCppC	30.0	4.3	1.0	9/16/2003	effective basin	2	4.1	1087.7	21	BCppA	25.0	3.6	0.8	7/26/2004	effective ba	1	7.1	1114.7
7	AA	160.0	22.9	5.3	9/17/2003	rest area	1	8.4	NS	21	BCppB	25.0	3.6	0.8	7/26/2004	effective ba	1	5.6	1121.6
22	AQ	330.0	47.1	11.0	9/17/2003	N of WB lane, near 4 UG wells across rd	1	8.2	380.0	20	BME	17.0	2.4	0.6	7/26/2004	effective ba	2	1.5	296.0
24	AR	300.0	42.9	10.0	9/17/2003	N of WB lane, N of median 8	1	8.1	983.0	20	BMppE	8.0	1.1	0.3	7/26/2004	effective ba	2	4.2	754.6
20	BMppA	1.0	0.1	0.0	9/17/2003	effective basin	1	6.9	1012.8	20	BMppK	25.0	3.6	0.8	7/26/2004	effective ba	2	-0.7	116.9
8	CA	160.0	22.9	5.3	9/17/2003	rest area, near EBC	1	6.1	412.0	20	BTppJ	75.0	10.7	2.5	7/26/2004	effective ba	2	-2.6	312.4
21	BCJ	42.0	6.0	1.4	9/18/2003	effective basin	2	-0.2	131.0	20	BMppA	1.0	0.1	0.0	7/27/2004	effective ba	1	6.9	1941.2
22	BTppA	420.0	56.0	14.0	9/18/2003	by back fence area, runoff b/w BK/BS	1	6.0	1228.3	13	AH	90.0	12.9	3.0	7/28/2004	area 12 (sou	1	7.4	348.0
21	BUppA	110.0	14.7	3.7	9/18/2003	effective basin	1	6.0	714.6	20	ATppC	6.0	0.9	0.2	7/28/2004	effective ba	1	4.7	612.0
21	BUppB	110.0	14.7	3.7	9/18/2003	effective basin	2	4.5	722.3	18	BCI	15.0	2.1	0.5	7/28/2004	effective ba	1	6.8	588.0
21	BUppC	110.0	14.7	3.7	9/18/2003	effective basin	2	3.0	393.7	20	BMppD	6.0	0.9	0.2	7/28/2004	effective ba	2	4.8	1509.3
21	BUppD	110.0	14.7	3.7	9/18/2003	effective basin	2	1.5	395.6	20	BMppI	15.0	2.1	0.5	7/28/2004	effective ba	2	1.7	990.8
21	BUppE	110.0	14.7	3.7	9/18/2003	effective basin	2	0.9	232.3	10	BTJ	90.0	12.9	3.0	7/28/2004	effective ba	2	-3.7	271.0
21	BUppF	110.0	14.7	3.7	9/18/2003	effective basin	2	0.2	180.5	20	ATppB	5.0	0.7	0.2	7/29/2004	effective ba	1	5.3	2865.3
21	BUppG	110.0	14.7	3.7	9/18/2003	effective basin	2	-0.4	158.4	20	BMppC	5.0	0.7	0.2	7/29/2004	effective ba	1	5.4	1461.9
21	BUppH	110.0	14.7	3.7	9/18/2003	effective basin	2	-1.0	136.0	20	BMppI	13.0	1.9	0.4	7/30/2004	effective ba	2	2.3	316.1
13	AH	90	13	3	9/19/2003	area 12 (south shoulder of EB lane)	1	7.4	2425.0	20	ATppA	3.0	0.4	0.1	7/31/2004	effective ba	1	6.8	1036.9
20	BTJ	90	13	3	9/19/2003	effective basin	2	-3.7	151.0	21	BCppH	50.0	7.1	1.7	7/31/2004	effective ba	2	-0.8	338.5
20	BYppJ	150.0	20.0	5.0	9/20/2003	effective basin	2	-3.3	173.8	21	BCppI	50.0	7.1	1.7	7/31/2004	effective ba	2	-1.4	226.5
20	BCd	40.0	5.7	1.3	9/20/2003	effective basin	2	0.2	346.0	21	BCppJ	50.0	7.1	1.7	7/31/2004	effective ba	2	-2.0	264.5
20	BCe	40.0	5.7	1.3	9/20/2003	effective basin	2	-1.6	198.0	20	BMppB	3.0	0.4	0.1	7/31/2004	effective ba	1	6.0	586.1
21	BCppD	40.0	5.7	1.3	9/20/2003	effective basin	2	2.6	626.9	20	BTppA	50.0	7.1	1.7	7/31/2004	effective ba	1	6.5	614.1
21	BCppE	40.0	5.7	1.3	9/20/2003	effective basin	2	1.0	608.2	20	BTppB	50.0	7.1	1.7	7/31/2004	effective ba	2	5.0	741.9
21	BCppF	40.0	5.7	1.3	9/20/2003	effective basin	2	0.4	562.4	20	BTppD	70.0	10.0	2.3	7/31/2004	effective ba	2	1.9	817.7
21	BCppG	40.0	5.7	1.3	9/20/2003	effective basin	2	-0.2	572.1	20	BTppE	70.0	10.0	2.3	7/31/2004	effective ba	2	1.3	741.2
20	BTppJ	75.0	10.7	2.5	9/20/2003	effective basin	2	-2.6	244.6	20	BTppF	70.0	10.0	2.3	7/31/2004	effective ba	2	0.7	963.1
21	BCppA	25.0	3.6	0.8	9/21/2003	effective basin	1	7.1	798.0	20	BTppG	70.0	10.0	2.3	7/31/2004	effective ba	2	0.1	11.9
21	BCppB	25.0	3.6	0.8	9/21/2003	effective basin	1	5.6	1253.8	20	BTppH	70.0	10.0	2.3	7/31/2004	effective ba	2	-0.5	693.4
20	BMppK	25.0	3.6	0.8	9/21/2003	effective basin	2	-0.7	253.2	20	BTppI	70.0	10.0	2.3	7/31/2004	effective ba	2	-1.1	856.1
20	BYppI	140.0	18.7	4.7	9/21/2003	effective basin	2	-1.8	158.8										
9	AC	190.0	27.1	6.3	9/22/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.2	247.0	12	AJ	11.0	1.6	0.4	8/1/2004	crest of bas	1	8.0	612.0
14	AF	120.0	17.1	4.0	9/22/2003	area 12 (south shoulder of EB lane)	1	7.3	269.0	20	BMc	11.0	1.6	0.4	8/1/2004	effective ba	2	3.0	114.0
15	AO	50.0	7.1	1.7	9/22/2003	near BO cluster, not "effective" area	1	8.2	195.0	20	BMppG	11.0	1.6	0.4	8/2/2004	effective ba	2	2.9	516.6
21	BCppH	50.0	7.1	1.7	9/22/2003	effective basin	2	-0.8	174.0	20	BMD	10.0	1.4	0.3	8/2/2004	effective ba	2	2.1	303.0
21	BCppI	50.0	7.1	1.7	9/22/2003	effective basin	2	-1.4	142.2	20	BMppA	1.0	0.1	0.0	8/2/2004	effective ba	1	6.9	1097.8
21	BCppJ	50.0	7.1	1.7	9/22/2003	effective basin	2	-2.0	122.3	20	BMppJ	18.0	2.6	0.6	8/2/2004	effective ba	2	0.8	207.8
20	BTk	50.0	7.1	1.7	9/22/2003	effective basin	1	7.3	841.0	21	BN	10.0	1.4	0.3	8/2/2004	effective ba	2	1.8	108.0
20	BTppA	50.0	7.1	1.7	9/22/2003	effective basin	1	6.5	416.7	20	BYppI	140.0	18.7	4.7	8/2/2004	effective ba	2	-1.8	543.2
20	BTppB	50.0	7.1	1.7	9/22/2003	effective basin	2	5.0	568.3	20	BMb	9.0	1.3	0.3	8/3/2004	effective ba	2	3.9	567.0
21	BZ	120.0	17.1	4.0	9/22/2003	effective basin	1	6.7	204.0	20	BMppF	9.0	1.3	0.3	8/3/2004	effective ba	2	3.6	542.8
14	AN	210.0	30.0	7.0	9/23/2003	area 12 (south shoulder of EB lane)	1	8.0	164.0	21	BUppA	110.0	14.7	3.7	8/3/2004	effective ba	1	6.0	406.2
20	BYppD	130.0	17.3	4.3	9/24/2003	effective basin	2	1.3	224.7	21	BUppB								

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
20	BYpppF	130.0	17.3	4.3	9/24/2003	effective basin	2	0.0	230.6	21	BUPppD	110.0	14.7	3.7	8/3/2004	effective ba	2	1.5	754.3
20	BYpppG	130.0	17.3	4.3	9/24/2003	effective basin	2	-0.6	15.1	21	BUPppE	110.0	14.7	3.7	8/3/2004	effective ba	2	0.9	872.2
20	BYpppH	130.0	17.3	4.3	9/24/2003	effective basin	2	-1.2	209.1	21	BUPppF	110.0	14.7	3.7	8/3/2004	effective ba	2	0.2	900.6
8	AB	35.0	5.0	1.2	9/25/2003	west of rest area, runoff slope	1	8.0	419.0	21	BUPppG	110.0	14.7	3.7	8/3/2004	effective ba	2	-0.4	529.3
21	BE	35.0	5.0	1.2	9/25/2003	effective basin	2	-0.5	116.0	21	BUPppH	110.0	14.7	3.7	8/3/2004	effective ba	2	-1.0	516.2
20	BTpppD	70.0	10.0	2.3	9/25/2003	effective basin	2	1.9	617.1	20	BYpppD	130.0	17.3	4.3	8/3/2004	effective ba	2	1.3	707.9
20	BTpppE	70.0	10.0	2.3	9/25/2003	effective basin	2	1.3	653.1	20	BYpppE	130.0	17.3	4.3	8/3/2004	effective ba	2	0.7	713.7
20	BTpppF	70.0	10.0	2.3	9/25/2003	effective basin	2	0.7	372.8	20	BYpppF	130.0	17.3	4.3	8/3/2004	effective ba	2	0.0	993.2
20	BTpppG	70.0	10.0	2.3	9/25/2003	effective basin	2	0.1	292.6	20	BYpppG	130.0	17.3	4.3	8/3/2004	effective ba	2	-0.6	32.8
20	BTpppH	70.0	10.0	2.3	9/25/2003	effective basin	2	-0.5	177.8	20	BYpppH	130.0	17.3	4.3	8/3/2004	effective ba	2	-1.2	780.1
20	BTpppI	70.0	10.0	2.3	9/25/2003	effective basin	2	-1.1	237.7	21	BCpppC	30.0	4.3	1.0	8/4/2004	effective ba	2	4.1	819.1
21	BUPppI	120.0	16.0	4.0	9/25/2003	effective basin	2	-1.6	148.9	20	BMpppE	8.0	1.1	0.3	8/4/2004	effective ba	2	4.2	797.2
20	BYpppA	120.0	17.1	4.0	9/25/2003	effective basin	1	5.8	253.2	20	BMA	7.0	1.0	0.2	8/5/2004	effective ba	1	4.8	434.0
20	BYpppB	120.0	16.0	4.0	9/25/2003	effective basin	2	4.3	240.8	20	BMpppI	15.0	2.1	0.5	8/5/2004	effective ba	2	1.7	974.1
20	BYpppC	120.0	16.0	4.0	9/25/2003	effective basin	2	2.8	227.1	20	ATpppC	6.0	0.9	0.2	8/6/2004	effective ba	2	4.7	462.4
9	AD	150.0	21.4	5.0	9/27/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	462.0	20	BMpppD	6.0	0.9	0.2	8/6/2004	effective ba	2	4.8	1523.5
11	AK	240.0	34.3	8.0	9/28/2003	@ E BC, east of median I3 area	1	7.4	614.0	16	AS	80.0	11.4	2.7	8/7/2004	area 12 (so	1	7.4	123.0
22	BlpppA	420.0	56.0	14.0	9/28/2003	by back fence area, runoff b/tw BK/BS	1	6.0	1430.3	20	ATpppB	5.0	0.7	0.2	8/7/2004	effective ba	1	5.3	2699.1
20	BMpppJ	18.0	2.6	0.6	9/28/2003	effective basin	2	0.8	422.0	20	BMpppC	5.0	0.7	0.2	8/7/2004	effective ba	1	5.4	1255.0
21	CB	240.0	34.3	8.0	9/28/2003	N of WB lane, near 4 UG wells across rd	1	8.6	810.0	20	BMpppH	13.0	1.9	0.4	8/7/2004	effective ba	2	2.3	581.2
16	AS	80	11	3	9/29/2003	area 12 (south shoulder of EB lane)	1	7.4	1413.0	20	BTpppK	80.0	11.4	2.7	8/7/2004	effective ba	2	-4.2	357.5
20	BTpppK	80.0	11.4	2.7	9/29/2003	effective basin	2	-4.2	181.1	20	ATpppA	3.0	0.4	0.1	8/9/2004	effective ba	1	6.8	1173.3
20	BYpppI	140.0	18.7	4.7	9/29/2003	effective basin	2	-1.8	182.9	21	BCpppA	25.0	3.6	0.8	8/9/2004	effective ba	1	7.1	183.1
18	AP	30.0	4.3	1.0	9/30/2003	effective basin	1	8.0	245.0	21	BCpppB	25.0	3.6	0.8	8/9/2004	effective ba	1	5.6	536.2
20	BCI	30.0	4.3	1.0	9/30/2003	effective basin	2	1.1	439.0	20	BMpppB	3.0	0.4	0.1	8/9/2004	effective ba	1	6.0	1143.1
21	BCJ	42.0	6.0	1.4	9/30/2003	effective basin	2	-0.2	144.0	20	BMpppG	11.0	1.6	0.4	8/9/2004	effective ba	2	2.9	1021.7
21	BCpppC	30.0	4.3	1.0	9/30/2003	effective basin	2	4.1	802.5	20	BMpppK	25.0	3.6	0.8	8/9/2004	effective ba	2	-0.7	115.3
22	BG	30.0	4.3	1.0	9/30/2003	effective basin	1	7.6	478.0	20	AT	2.0	0.3	0.1	8/10/2004	effective ba	1	7.3	630.0
20	BMpppI	15.0	2.1	0.5	10/1/2003	effective basin	2	1.7	675.2	21	BCpppD	40.0	5.7	1.3	8/10/2004	effective ba	2	2.6	341.6
20	BYpppD	130.0	17.3	4.3	10/1/2003	effective basin	2	1.3	201.7	21	BCpppE	40.0	5.7	1.3	8/10/2004	effective ba	2	1.0	1133.0
20	BYpppE	130.0	17.3	4.3	10/1/2003	effective basin	2	0.7	178.7	21	BCpppF	40.0	5.7	1.3	8/10/2004	effective ba	2	0.4	1137.5
20	BYpppF	130.0	17.3	4.3	10/1/2003	effective basin	2	0.0	225.7	21	HCpppG	40.0	5.7	1.3	8/10/2004	effective ba	2	-0.2	1143.7
20	BYpppG	130.0	17.3	4.3	10/1/2003	effective basin	2	-0.6	15.0	20	BTpppC	60.0	8.6	2.0	8/10/2004	effective ba	2	3.5	542.6
20	BYpppH	130.0	17.3	4.3	10/1/2003	effective basin	2	-1.2	206.9	20	BMpppA	1.0	0.1	0.0	8/11/2004	effective ba	1	6.9	616.0
20	BCd	40.0	5.7	1.3	10/2/2003	effective basin	2	0.2	324.0	20	BMpppF	9.0	1.3	0.3	8/11/2004	effective ba	2	3.6	1174.9
20	BCe	40.0	5.7	1.3	10/2/2003	effective basin	2	-1.6	168.0	12	AG	130.0	18.6	4.3	8/12/2004	area 12 (so	1	7.3	505.0
21	BCpppD	40.0	5.7	1.3	10/2/2003	effective basin	2	2.6	766.8	19	BCJ	42.0	6.0	1.4	8/12/2004	effective ba	2	-0.2	218.0
21	BCpppE	40.0	5.7	1.3	10/2/2003	effective basin	2	1.0	447.7	20	BMpppE	8.0	1.1	0.3	8/12/2004	effective ba	2	4.2	1168.9
21	BCpppF	40.0	5.7	1.3	10/2/2003	effective basin	2	0.4	372.8	20	BTpppJ	75.0	10.7	2.5	8/12/2004	effective ba	2	-2.6	608.2
21	BCpppG	40.0	5.7	1.3	10/2/2003	effective basin	2	-0.2	862.5	20	BYpppD	130.0	17.3	4.3	8/12/2004	effective ba	2	1.3	557.0
20	BYpppJ	150	20	5	10/2/2003	effective basin	2	-3.3	183.6	20	BYpppE	130.0	17.3	4.3	8/12/2004	effective ba	2	0.7	674.9
10	AI	200.0	28.6	6.7	10/3/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	421.0	20	BYpppF	130.0	17.3	4.3	8/12/2004	effective ba	2	0.0	906.4
20	BMpppH	13.0	1.9	0.4	10/3/2003	effective basin	2	2.3	1434.8	20	BYpppG	130.0	17.3	4.3	8/12/2004	effective ba	2	-0.6	174.7
20	BTpppJ	75.0	10.7	2.5	10/4/2003	effective basin	2	-2.6	238.9	20	BYpppH	130.0	17.3	4.3	8/12/2004	effective ba	2	-1.2	860.3
21	BUPppI	120.0	16.0	4.0	10/4/2003	effective basin	2	-1.6	125.1	13	AH	90.0	12.9	3.0	8/13/2004	area 12 (so	1	7.4	397.0
20	BYpppA	120.0	17.1	4.0	10/4/2003	effective basin	1	5.8	281.3	10	BTJ	90.0	12.9	3.0	8/13/2004	effective ba	2	-3.7	252.0
20	BYpppB	120.0	16.0	4.0	10/4/2003	effective basin	2	4.3	275.9	21	BUPppI	120.0	16.0	4.0	8/13/2004	effective ba	2	-1.6	222.0
20	BYpppC	120.0	16.0	4.0	10/4/2003	effective basin	2	2.8	244.7	20	BYpppA	120.0	17.1	4.0	8/13/2004	effective ba	1	5.8	528.0
20	BCg	25.0	3.6	0.8	10/5/2003	effective basin	2	2.9	452.0	20	BYpppB	120.0	16.0	4.0	8/13/2004	effective ba	2	4.3	440.3
21	BCpppA	25.0	3.6	0.8	10/5/2003	effective basin	1	7.1	552.0	20	BYpppC	120.0	16.0	4.0	8/13/2004	effective ba	2	2.8	542.6
21	BCpppB	25.0	3.6	0.8	10/5/2003	effective basin	1	5.6	694.4	20	ATpppC	6.0	0.9	0.2	8/14/2004	effective ba	2	4.7	645.7
20	BMpppG	11.0	1.6	0.4	10/5/2003	effective basin	2	2.9	1941.2	9	BCd	40.0	5.7	1.3	8/14/2004	effective ba	2	0.2	404.0
20	BMpppK	25.0	3.6	0.8	10/5/2003	effective basin	2	-0.7	232.1	9	BCe	40.0	5.7	1.3	8/14/2004	effective ba	2	-1.6	173.0
20	BTpppC	60.0	8.6	2.0	10/5/2003	effective basin	2	3.5	639.0	20	BMpppD	6.0	0.9	0.2	8/14/2004	effective ba	2	4.8	1658.4
21	BUPppA	110.0	14.7	3.7	10/5/2003	effective basin	1	6.0	866.1	20	ATpppB	5.0	0.7	0.2	8/15/2004	effective ba	1	5.3	5919.3
21	BUPppB	110.0	14.7	3.7	10/5/2003	effective basin	2	4.5	12.0	20	BMpppC	5.0	0.7	0.2	8/15/2004	effective ba	1	5.4	1226.9
21	BUPppC	110.0	14.7	3.7	10/5/2003	effective basin	2	3.0	436.7	20	BMpppI	18.0	2.6	0.6	8/16/2004	effective ba	2	0.8	366.9
21	BUPppD	110.0	14.7	3.7	10/5/2003	effective basin	2	1.5	408.6	20	ATpppA	3.0	0.4	0.1	8/17/2004	effective ba	1	6.8	674.7
21	BUPppE	110.0	14.7	3.7	10/5/2003	effective basin	2	0.9	349.3	20	BMpppB	3.0	0.4	0.1	8/17/2004	effective ba	1	6.0	186.9
21	BUPppF	110.0	14.7	3.7	10/5/2003	effective basin	2	0.2	292.8	9	BTg	70.0	10.0	2.3	8/17/2004	effective ba	2	-0.1	263.0
21	BUPppG	110.0	14.7	3.7	10/5/2003	effective basin	2	-0.4	223.9	21	BTh	70.0	10.0	2.3	8/17/2004	effective ba	2	-1.0	213.0
21	BUPppH	110.0	14.7	3.7	10/5/2003	effective basin	2	-1.0	197.1	20	BTpppD	70.0	10.0	2.3	8/17/2004	effective ba	2	1.9	860.0
8	AB	35.0	5.0	1.2	10/7/2003	west of rest area, runoff slope	1	8.0	378.0	20	BTpppE	70.0	10.0	2.3	8/17/2004	effective ba	2	1.3	870.1
21	BE	35.0	5.0	1.2	10/7/2003	effective basin	2	-0.5	160.0	20	BTpppF	70.0	10.0	2.3	8/17/2004	effective ba	2	0.7	924.5
20	BMpppF	9.0	1.3	0.3	10/7/2003	effective basin	2	3.6	1181.6	20	BTpppG	70.0	10.0	2.3	8/17/2004	effective ba	2	0.1	5.6
20	BMpppE	8.0	1.1	0.3	10/8/2003	effective basin	2	4.2	1658.0	20	BTpppH	70.0	10.0	2.3	8/17/2004	effective ba	2	-0.5	334.2
20	BTg	70	10	2	10/9/2003	effective basin	2	-0.1	174.0	20	BTpppI	70.0	10.0	2.3	8/17/2004	effective ba	2	-1.1	449.9
20	BTh	70	10	2	10/9/2003	effective basin	2	-1.0	158.0	20	BTpppK	80.0	11.4	2.7	8/18/2004	effective ba	2	-4.2	251.8

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
20	BTppE	70.0	10.0	2.3	10/9/2003	effective basin	2	1.3	340.7	20	BMppE	15.0	2.1	0.5	8/19/2004	effective ba	2	1.7	1106.6
20	BTppF	70.0	10.0	2.3	10/9/2003	effective basin	2	0.7	345.0	22	BTf	68.0	9.7	2.3	8/19/2004	effective ba	2	0.7	376.0
20	BTppG	70.0	10.0	2.3	10/9/2003	effective basin	2	0.1	345.9	21	BCppC	30.0	4.3	1.0	8/20/2004	effective ba	2	4.1	371.0
20	BTppH	70.0	10.0	2.3	10/9/2003	effective basin	2	-0.5	233.5	21	BCppH	50.0	7.1	1.7	8/20/2004	effective ba	2	-0.8	866.8
20	BTppI	70.0	10.0	2.3	10/9/2003	effective basin	2	-1.1	236.5	21	BCppI	50.0	7.1	1.7	8/20/2004	effective ba	2	-1.4	570.7
20	BYppD	130.0	17.3	4.3	10/9/2003	effective basin	2	1.3	278.1	21	BCppJ	50.0	7.1	1.7	8/20/2004	effective ba	2	-2.0	454.3
20	BYppE	130.0	17.3	4.3	10/9/2003	effective basin	2	0.7	249.1	20	BTppA	50.0	7.1	1.7	8/20/2004	effective ba	1	6.5	129.3
20	BYppF	130.0	17.3	4.3	10/9/2003	effective basin	2	0.0	248.9	20	BTppB	50.0	7.1	1.7	8/20/2004	effective ba	2	5.0	257.4
20	BYppG	130.0	17.3	4.3	10/9/2003	effective basin	2	-0.6	17.6	20	BMppH	13.0	1.9	0.4	8/21/2004	effective ba	2	2.3	968.4
20	BYppH	130.0	17.3	4.3	10/9/2003	effective basin	2	-1.2	204.8	14	AF	120.0	17.1	4.0	8/22/2004	effective ba	1	7.1	198.0
20	BYppI	150	20	5	10/9/2003	effective basin	2	-3.3	197.2	21	BTa	65.0	9.3	2.2	8/22/2004	effective ba	1	5.4	200.0
20	ATppC	6.0	0.9	0.2	10/10/2003	effective basin	2	4.7	435.1	21	BTb	65.0	9.3	2.2	8/22/2004	effective ba	2	4.4	600.0
19	BCa	20.0	2.9	0.7	10/10/2003	effective basin	1	6.0	508.0	21	BTc	65.0	9.3	2.2	8/22/2004	effective ba	2	3.6	607.0
19	BCb	20.0	2.9	0.7	10/10/2003	effective basin	2	3.6	673.0	22	BTd	65.0	9.3	2.2	8/22/2004	effective ba	2	2.7	712.0
20	BCc	20.0	2.9	0.7	10/10/2003	effective basin	2	2.0	493.0	22	BTf	65.0	9.3	2.2	8/22/2004	effective ba	2	1.7	506.0
21	BD	20.0	2.9	0.7	10/10/2003	effective basin	1	5.6	635.0	21	BUppI	120.0	16.0	4.0	8/22/2004	effective ba	2	-1.6	241.4
20	BMppD	6.0	0.9	0.2	10/10/2003	effective basin	2	4.8	2363.3	20	BYppA	120.0	17.1	4.0	8/22/2004	effective ba	1	5.8	587.2
20	ATppB	5.0	0.7	0.2	10/11/2003	effective basin	1	5.3	2725.6	20	BYppB	120.0	16.0	4.0	8/22/2004	effective ba	2	4.3	454.3
20	BMppC	5.0	0.7	0.2	10/11/2003	effective basin	1	5.4	2278.9	20	BYppC	120.0	16.0	4.0	8/22/2004	effective ba	2	2.8	527.8
20	BTf	68	10	2	10/11/2003	effective basin	2	0.7	203.0	20	BZ	120.0	17.1	4.0	8/22/2004	effective ba	1	6.7	338.0
21	BUppI	120.0	16.0	4.0	10/11/2003	effective basin	2	-1.6	102.9	16	AS	80.0	11.4	2.7	8/23/2004	effective ba	1	7.4	141.0
20	BYppA	120.0	17.1	4.0	10/11/2003	effective basin	1	5.8	282.1	20	BMppG	11.0	1.6	0.4	8/23/2004	effective ba	2	2.9	1030.9
20	BYppB	120.0	16.0	4.0	10/11/2003	effective basin	2	4.3	242.8	20	BTppK	75.0	10.7	2.5	8/23/2004	effective ba	2	-2.6	396.6
20	BYppC	120.0	16.0	4.0	10/11/2003	effective basin	2	2.8	186.3	20	BTppL	80.0	11.4	2.7	8/23/2004	effective ba	2	-4.2	240.2
18	AP	30.0	4.3	1.0	10/12/2003	effective basin	1	8.0	288.0	21	BUppA	110.0	14.7	3.7	8/23/2004	effective ba	1	6.0	410.7
20	BCi	30.0	4.3	1.0	10/12/2003	effective basin	2	1.1	420.0	21	BUppB	110.0	14.7	3.7	8/23/2004	effective ba	2	4.5	330.2
21	BCppC	30.0	4.3	1.0	10/12/2003	effective basin	2	4.1	761.4	21	BUppC	110.0	14.7	3.7	8/23/2004	effective ba	2	3.0	352.7
22	BQ	30.0	4.3	1.0	10/12/2003	effective basin	2	7.6	654.0	21	BUppD	110.0	14.7	3.7	8/23/2004	effective ba	2	1.5	870.1
20	BMppI	18.0	2.6	0.6	10/12/2003	effective basin	2	0.8	422.0	21	BUppE	110.0	14.7	3.7	8/23/2004	effective ba	2	0.9	658.8
20	BYppJ	140	19	5	10/12/2003	effective basin	2	-1.8	216.7	21	BUppF	110.0	14.7	3.7	8/23/2004	effective ba	2	0.2	541.8
9	AC	190.0	27.1	6.3	10/13/2003	b/tw areas 6/16, N of ramp, S of shoulder	2	8.2	187.0	21	BUppG	110.0	14.7	3.7	8/23/2004	effective ba	2	-0.4	566.0
20	ATppA	3.0	0.4	0.1	10/13/2003	effective basin	1	6.8	440.3	21	BUppH	110.0	14.7	3.7	8/23/2004	effective ba	2	-1.0	346.7
20	BCh	17.0	2.4	0.6	10/13/2003	effective basin	1	5.0	-521.0	22	BCi	30.0	4.3	1.0	8/24/2004	effective ba	2	1.1	693.0
20	BMe	17.0	2.4	0.6	10/13/2003	effective basin	2	1.5	243.0	20	BG	30.0	4.3	1.0	8/24/2004	N of WB ls	1	7.6	522.0
20	BMppB	3.0	0.4	0.1	10/13/2003	effective basin	1	6.0	928.4	21	BCppA	25.0	3.6	0.8	8/25/2004	effective ba	1	7.1	335.0
21	BTa	65	9	2	10/14/2003	effective basin	1	5.4	475.0	21	BCppB	25.0	3.6	0.8	8/25/2004	effective ba	1	5.6	176.9
21	BTb	65	9	2	10/14/2003	effective basin	2	4.4	472.0	20	BMppF	9.0	1.3	0.3	8/25/2004	effective ba	-2	3.6	1557.7
21	BTc	65	9	2	10/14/2003	effective basin	2	3.6	392.0	20	BMppK	25.0	3.6	0.8	8/25/2004	effective ba	2	-0.7	227.7
21	BTd	65	9	2	10/14/2003	effective basin	2	2.7	406.0	20	BMppE	8.0	1.1	0.3	8/26/2004	effective ba	2	4.2	1247.0
20	BTf	65	9	2	10/14/2003	effective basin	2	1.7	274.0	20	BTppC	60.0	8.6	2.0	8/27/2004	effective ba	2	3.5	323.3
21	BUppA	110.0	14.7	3.7	10/14/2003	effective basin	1	6.0	960.4	20	ATppC	6.0	0.9	0.2	8/28/2004	effective ba	2	4.7	606.7
21	BUppB	110.0	14.7	3.7	10/14/2003	effective basin	2	4.5	735.8	20	BMppD	6.0	0.9	0.2	8/28/2004	effective ba	2	4.8	699.6
21	BUppC	110.0	14.7	3.7	10/14/2003	effective basin	2	3.0	560.2	20	BTppD	70.0	10.0	2.3	8/28/2004	effective ba	2	1.9	752.5
21	BUppD	110.0	14.7	3.7	10/14/2003	effective basin	2	1.5	525.3	20	BTppE	70.0	10.0	2.3	8/28/2004	effective ba	2	1.3	708.7
21	BUppE	110.0	14.7	3.7	10/14/2003	effective basin	2	0.9	209.6	20	BTppF	70.0	10.0	2.3	8/28/2004	effective ba	2	0.7	726.1
21	BUppF	110.0	14.7	3.7	10/14/2003	effective basin	2	0.2	203.2	20	BTppG	70.0	10.0	2.3	8/28/2004	effective ba	2	0.1	683.4
21	BUppG	110.0	14.7	3.7	10/14/2003	effective basin	2	-0.4	193.6	20	BTppH	70.0	10.0	2.3	8/28/2004	effective ba	2	-0.5	404.5
21	BUppH	110.0	14.7	3.7	10/14/2003	effective basin	2	-1.0	149.3	20	BTppI	70.0	10.0	2.3	8/28/2004	effective ba	2	-1.1	315.5
21	BUppI	110.0	14.7	3.7	10/14/2003	effective basin	2	-3.3	197.7	20	BTppJ	70.0	10.0	2.3	8/28/2004	effective ba	2	-2.6	442.3
20	BYppJ	150.0	20.0	5.0	10/14/2003	effective basin	2	6.8	403.0	20	BTppK	70.0	10.0	2.3	8/28/2004	effective ba	2	5.3	3574.5
20	BCf	15.0	2.1	0.5	10/15/2003	effective basin	1	-0.8	168.9	18	BCg	25.0	3.6	0.8	8/29/2004	effective ba	2	2.9	478.0
21	BCppH	50.0	7.1	1.7	10/15/2003	effective basin	2	-1.4	148.6	20	BMppC	5.0	0.7	0.2	8/29/2004	effective ba	1	5.4	394.4
21	BCppI	50.0	7.1	1.7	10/15/2003	effective basin	2	-2.0	134.5	21	BCppD	40.0	5.7	1.3	8/30/2004	effective ba	2	2.6	1090.2
21	BCppJ	50.0	7.1	1.7	10/15/2003	effective basin	2	6.9	168.8	21	BCppE	40.0	5.7	1.3	8/30/2004	effective ba	2	1.0	686.3
20	BMppA	1.0	0.1	0.0	10/15/2003	effective basin	1	1.7	1053.0	21	BCppF	40.0	5.7	1.3	8/30/2004	effective ba	2	0.4	1053.4
20	BMppI	15.0	2.1	0.5	10/15/2003	effective basin	2	6.5	264.0	21	BCppG	40.0	5.7	1.3	8/30/2004	effective ba	2	-0.2	1638.3
20	BTppA	50.0	7.1	1.7	10/15/2003	effective basin	1	5.0	222.8	21	ATppA	3.0	0.4	0.1	8/31/2004	effective ba	1	6.8	972.6
20	BTppB	50.0	7.1	1.7	10/15/2003	effective basin	2	7.3	NS	20	BMppB	3.0	0.4	0.1	8/31/2004	effective ba	1	6.0	357.5
12	AG	130.0	18.6	4.3	10/17/2003	area 12 (south shoulder of EB lane)	1	8.1	1332.0	20	BMppJ	18.0	2.6	0.6	9/1/2004	effective ba	2	0.8	546.2
24	AR	300.0	42.9	10.0	10/17/2003	N of WB lane, N of median S	2	2.9	461.0	21	BUppA	110.0	14.7	3.7	9/1/2004	effective ba	1	6.0	556.3
20	BCg	25.0	3.6	0.8	10/17/2003	effective basin	1	7.1	444.5	21	BUppB	110.0	14.7	3.7	9/1/2004	effective ba	2	4.5	397.5
21	BCppA	25.0	3.6	0.8	10/17/2003	effective basin	1	5.6	811.9	21	BUppC	110.0	14.7	3.7	9/1/2004	effective ba	2	3.0	666.7
21	BCppB	25.0	3.6	0.8	10/17/2003	effective basin	2	2.3	1941.2	21	BUppD	110.0	14.7	3.7	9/1/2004	effective ba	2	1.5	668.3
20	BMppH	13.0	1.9	0.4	10/17/2003	effective basin	2	-0.7	219.4	21	BUppE	110.0	14.7	3.7	9/1/2004	effective ba	2	0.9	449.9
20	BMppK	25.0	3.6	0.8	10/17/2003	effective basin	1	6.0	2669.3	21	BUppF	110.0	14.7	3.7	9/1/2004	effective ba	2	0.2	396.6
22	BTppA	420.0	56.0	14.0	10/18/2003	by back fence area, runoff b/tw BK/BS	2	-4.2	151.7	21	BUppG	110.0	14.7	3.7	9/1/2004	effective ba	2	-0.4	407.6
20	BTppK	80.0	11.4	2.7	10/19/2003	crest of basin, comes down slope	1	8.0	202.0	21	BUppH	110.0	14.7	3.7	9/1/2004	effective ba	2	-1.0	286.8
12	AJ	11.0	1.6	0.4	10/19/2003	effective basin	2	3.0	440.0	21	BUppI	110.0	14.7	3.7	9/2/2004	effective ba	1	6.9	343.3
20	BMc	11.0	1.6	0.4	10/19/2003	effective basin	2	2.9	151										

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msf	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msf	SpecCond uS/cm
21	BUpcl	120.0	16.0	4.0	10/19/2003	effective basin	2	-1.5	130.7	21	BTH	70.0	10.0	2.3	9/2/2004	effective ba	2	-1.0	182.0
20	BYppA	120.0	17.1	4.0	10/19/2003	effective basin	1	5.8	456.8	20	BTppD	70.0	10.0	2.3	9/2/2004	effective ba	2	1.9	1033.3
20	BYppB	120.0	16.0	4.0	10/19/2003	effective basin	2	4.3	289.0	20	BTppE	70.0	10.0	2.3	9/2/2004	effective ba	2	1.3	811.9
20	BYppC	120.0	16.0	4.0	10/19/2003	effective basin	2	2.8	271.2	20	BTppF	70.0	10.0	2.3	9/2/2004	effective ba	2	0.7	631.4
20	BYppcl	140	19	5	10/19/2003	effective basin	2	-1.8	205.7	20	BTppG	70.0	10.0	2.3	9/2/2004	effective ba	2	0.1	5.5
19	BMd	10.0	1.4	0.3	10/20/2003	effective basin	2	2.1	327.0	20	BTppH	70.0	10.0	2.3	9/2/2004	effective ba	2	-0.5	367.0
19	BN	10.0	1.4	0.3	10/20/2003	effective basin	2	1.8	430.0	20	BTppI	70.0	10.0	2.3	9/2/2004	effective ba	2	-1.1	339.1
20	BMB	9.0	1.3	0.3	10/21/2003	effective basin	2	3.9	438.0	20	BTppK	80.0	11.4	2.7	9/2/2004	effective ba	2	-4.2	184.4
20	BMppF	9.0	1.3	0.3	10/21/2003	effective basin	2	3.6	1688.0	21	BCa	20.0	2.9	0.7	9/3/2004	effective ba	1	6.0	122.0
21	BUpclA	110.0	14.7	3.7	10/21/2003	effective basin	1	6.0	1032.1	9	BCb	20.0	2.9	0.7	9/3/2004	effective ba	2	3.6	372.0
21	BUpclB	110.0	14.7	3.7	10/21/2003	effective basin	2	4.5	645.5	18	BCc	20.0	2.9	0.7	9/3/2004	effective ba	2	2.0	651.0
21	BUpclC	110.0	14.7	3.7	10/21/2003	effective basin	2	3.0	465.8	19	BD	20.0	2.9	0.7	9/3/2004	effective ba	1	5.6	143.0
21	BUpclD	110.0	14.7	3.7	10/21/2003	effective basin	2	1.5	216.2	20	BMppcl	15.0	2.1	0.5	9/4/2004	effective ba	2	1.7	929.2
21	BUpclE	110.0	14.7	3.7	10/21/2003	effective basin	2	0.9	184.5	22	BTf	68.0	9.7	2.3	9/4/2004	effective ba	2	0.7	404.0
21	BUpclF	110.0	14.7	3.7	10/21/2003	effective basin	2	0.2	174.6	19	BCh	17.0	2.4	0.6	9/6/2004	effective ba	1	5.0	208.0
21	BUpclG	110.0	14.7	3.7	10/21/2003	effective basin	2	-0.4	153.1	21	BCppH	50.0	7.1	1.7	9/6/2004	effective ba	2	-0.8	334.2
21	BUpclH	110.0	14.7	3.7	10/21/2003	effective basin	2	-1.0	121.2	21	BCppI	50.0	7.1	1.7	9/6/2004	effective ba	2	-1.4	449.9
7	AA	160.0	22.9	5.3	10/22/2003	rest area	1	8.4	NS	21	BCppJ	50.0	7.1	1.7	9/6/2004	effective ba	2	-2.0	608.2
13	AH	90.0	12.9	3.0	10/22/2003	area 12 (south shoulder of EB lane)	1	7.4	517.0	20	BMe	17.0	2.4	0.6	9/6/2004	effective ba	2	1.5	810.0
19	BCa	20.0	2.9	0.7	10/22/2003	effective basin	1	6.0	421.0	20	BMppH	13.0	1.9	0.4	9/6/2004	effective ba	2	2.3	1284.1
19	BCb	20.0	2.9	0.7	10/22/2003	effective basin	2	3.6	477.0	19	BTk	50.0	7.1	1.7	9/6/2004	effective ba	1	7.3	602.0
20	BCc	20.0	2.9	0.7	10/22/2003	effective basin	2	2.0	521.0	20	BTppA	50.0	7.1	1.7	9/6/2004	effective ba	1	6.5	514.9
21	BD	20.0	2.9	0.7	10/22/2003	effective basin	1	5.6	613.0	20	BTppB	50.0	7.1	1.7	9/6/2004	effective ba	2	5.0	269.4
20	BMppE	8.0	1.1	0.3	10/22/2003	effective basin	2	4.2	759.6	21	BTa	65.0	9.3	2.2	9/7/2004	effective ba	1	5.4	142.0
20	BTJ	90.0	12.9	3.0	10/22/2003	effective basin	2	-3.7	186.0	21	BTb	65.0	9.3	2.2	9/7/2004	effective ba	2	4.4	518.0
20	BYppD	130	17	4	10/22/2003	effective basin	2	1.3	334.6	21	BTc	65.0	9.3	2.2	9/7/2004	effective ba	2	3.6	494.0
20	BYppE	130	17	4	10/22/2003	effective basin	2	0.7	277.6	22	BTd	65.0	9.3	2.2	9/7/2004	effective ba	2	2.7	509.0
20	BYppF	130	17	4	10/22/2003	effective basin	2	0.0	334.6	22	BTe	65.0	9.3	2.2	9/7/2004	effective ba	2	1.7	471.0
20	BYppG	130	17	4	10/22/2003	effective basin	2	-0.6	18.1	20	BTppC	60.0	8.6	2.0	9/7/2004	effective ba	2	3.5	668.8
20	BYppH	130	17	4	10/22/2003	effective basin	2	-1.2	249.8	20	BTppI	75.0	10.7	2.5	9/7/2004	effective ba	2	-2.6	583.4
8	CA	160.0	22.9	5.3	10/22/2003	rest area, near E BC	1	6.1	434.0	18	BCf	15.0	2.1	0.5	9/8/2004	effective ba	1	6.8	145.0
19	BMA	7.0	1.0	0.2	10/23/2003	effective basin	1	4.8	496.0	20	BMppQ	11.0	1.6	0.4	9/8/2004	effective ba	2	2.9	1083.5
20	BTppJ	75.0	10.7	2.5	10/23/2003	effective basin	2	-2.6	276.2	21	BCppA	30.0	4.3	1.0	9/9/2004	effective ba	2	4.1	379.8
20	BYppJ	150.0	20.0	5.0	10/23/2003	effective basin	2	-3.3	181.5	20	BMppF	9.0	1.3	0.3	9/10/2004	effective ba	2	3.6	973.3
20	ATppC	6.0	0.9	0.2	10/24/2003	effective basin	2	4.7	695.5	20	BMppE	8.0	1.1	0.3	9/11/2004	effective ba	2	4.2	679.8
20	BMppD	6.0	0.9	0.2	10/24/2003	effective basin	2	4.8	844.0	20	BMc	11.0	1.6	0.4	9/12/2004	effective ba	2	3.0	388.0
20	BMppJ	18.0	2.6	0.6	10/24/2003	effective basin	2	0.8	337.6	20	BTppC	60.0	8.6	2.0	9/12/2004	effective ba	2	3.5	427.0
20	BYppI	140.0	18.7	4.7	10/24/2003	effective basin	2	-1.8	200.7	20	BTppD	70.0	10.0	2.3	9/12/2004	effective ba	2	1.9	339.4
20	ATppB	5.0	0.7	0.2	10/25/2003	effective basin	1	5.3	2687.5	20	BTppE	70.0	10.0	2.3	9/12/2004	effective ba	2	1.3	697.8
20	BCh	17.0	2.4	0.6	10/25/2003	effective basin	1	5.0	624.0	20	BTppF	70.0	10.0	2.3	9/12/2004	effective ba	2	0.7	780.5
21	BCppD	40.0	5.7	1.3	10/25/2003	effective basin	2	2.6	448.8	20	BTppG	70.0	10.0	2.3	9/12/2004	effective ba	2	0.1	8.8
21	BCppE	40.0	5.7	1.3	10/25/2003	effective basin	2	1.0	454.3	20	BTppH	70.0	10.0	2.3	9/12/2004	effective ba	2	-0.5	516.2
21	BCppF	40.0	5.7	1.3	10/25/2003	effective basin	2	0.4	344.1	20	BTppI	70.0	10.0	2.3	9/12/2004	effective ba	2	-1.1	511.1
21	BCppG	40.0	5.7	1.3	10/25/2003	effective basin	2	-0.2	936.3	20	ATppC	6.0	0.9	0.2	9/13/2004	effective ba	2	4.7	656.3
20	BMe	17.0	2.4	0.6	10/25/2003	effective basin	2	1.5	202.0	20	BMD	10.0	1.4	0.3	9/13/2004	effective ba	2	2.1	683.0
20	BMppC	5.0	0.7	0.2	10/25/2003	effective basin	1	5.4	928.4	20	BMppD	6.0	0.9	0.2	9/13/2004	effective ba	2	4.8	683.2
11	AK	240.0	34.3	8.0	10/26/2003	@ E BC, east of median 13 area	1	7.4	481.0	21	BN	10.0	1.4	0.3	9/13/2004	effective ba	2	1.8	446.0
21	CB	240.0	34.3	8.0	10/26/2003	N of WB lane, near 4 UG wells across rd	1	8.6	1138.0	20	ATppB	5.0	0.7	0.2	9/14/2004	effective ba	1	5.3	3139.0
14	AF	120.0	17.1	4.0	10/27/2003	area 12 (south shoulder of EB lane)	1	7.3	1403.0	19	BCJ	42.0	6.0	1.4	9/14/2004	effective ba	2	-0.2	467.0
20	ATppA	3.0	0.4	0.1	10/27/2003	effective basin	1	6.8	249.4	21	BCppA	25.0	3.6	0.8	9/14/2004	effective ba	1	7.1	32.3
20	BCf	15.0	2.1	0.5	10/27/2003	effective basin	1	6.8	292.0	21	BCppB	25.0	3.6	0.8	9/14/2004	effective ba	1	5.6	230.0
22	BTppA	420.0	56.0	14.0	10/27/2003	by back fence area, runoff b/w BK/BS	1	6.0	2595.9	20	BMB	9.0	1.3	0.3	9/14/2004	effective ba	2	3.9	458.0
20	BMppB	3.0	0.4	0.1	10/27/2003	effective basin	1	6.0	151.9	20	BMppC	5.0	0.7	0.2	9/14/2004	effective ba	1	5.4	1198.5
20	BMppJ	15.0	2.1	0.5	10/27/2003	effective basin	2	1.7	928.4	20	BMppK	25.0	3.6	0.8	9/14/2004	effective ba	2	-0.7	242.4
21	BZ	120.0	17.1	4.0	10/27/2003	effective basin	1	6.7	184.0	20	ATppA	3.0	0.4	0.1	9/16/2004	effective ba	1	6.8	502.5
14	AN	210.0	30.0	7.0	10/28/2003	area 12 (south shoulder of EB lane)	1	8.0	687.0	9	BCd	40.0	5.7	1.3	9/16/2004	effective ba	2	0.2	542.0
20	AT	2.0	0.3	0.1	10/28/2003	effective basin	1	7.3	361.0	9	BCe	40.0	5.7	1.3	9/16/2004	effective ba	2	-1.6	495.0
20	BTppD	70.0	10.0	2.3	10/28/2003	effective basin	2	1.9	508.6	21	BCppD	40.0	5.7	1.3	9/16/2004	effective ba	2	2.6	860.0
20	BTppE	70.0	10.0	2.3	10/28/2003	effective basin	2	1.3	237.9	21	BCppE	40.0	5.7	1.3	9/16/2004	effective ba	2	1.0	870.1
20	BTppF	70.0	10.0	2.3	10/28/2003	effective basin	2	0.7	238.7	21	BCppF	40.0	5.7	1.3	9/16/2004	effective ba	2	0.4	924.5
20	BTppG	70.0	10.0	2.3	10/28/2003	effective basin	2	0.1	264.0	21	BCppG	40.0	5.7	1.3	9/16/2004	effective ba	2	-0.2	5.6
20	BTppH	70.0	10.0	2.3	10/28/2003	effective basin	2	-0.5	177.4	20	BMA	7.0	1.0	0.2	9/16/2004	effective ba	1	4.8	773.0
20	BTppI	70.0	10.0	2.3	10/28/2003	effective basin	2	-1.1	256.2	20	BMppB	3.0	-0.4	0.1	9/16/2004	effective ba	1	6.0	142.7
15	AO	50	7	2	10/29/2003	near BO cluster, not "effective" area	1	8.2	164.0	21	BCppH	50.0	7.1	1.7	9/17/2004	effective ba	2	-0.8	404.5
21	BCppH	50.0	7.1	1.7	10/29/2003	effective basin	2	-0.8	128.4	21	BCppI	50.0	7.1	1.7	9/17/2004	effective ba	2	-1.4	458.8
21	BCppJ	50.0	7.1	1.7	10/29/2003	effective basin	2	-1.4	141.9	21	BCppJ	50.0	7.1	1.7	9/17/2004	effective ba	2	-2.0	339.9
21	BCppJ	50.0	7.1	1.7	10/29/2003	effective basin	2	-2.0	137.4	20	BTppA	50.0	7.1	1.7	9/17/2004	effective ba	1	6.5	276.9
20	BMppA	1.0	0.1	0.0	10/29/2003	effective basin	1	6.9	194.1	20	BTppB	50.0	7.1	1.7	9/17/2004	effective ba	2	5.0	177.4
20	BMppH	13.0	1.9	0.4	10/29/2003	effective basin	2	2.3	168										

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
20	BTppA	50.0	7.1	1.7	10/29/2003	effective basin	1	6.5	212.5	20	AT	2.0	0.3	0.1	9/21/2004	effective ba	1	7.3	865.0
20	BTppB	50.0	7.1	1.7	10/29/2003	effective basin	2	5.0	520.1	20	BE	35.0	5.0	1.2	9/21/2004	effective ba	2	-0.5	364.0
21	BUppA	110.0	14.7	3.7	10/29/2003	effective basin	1	6.0	878.4	20	BMppJ	18.0	2.6	0.6	9/21/2004	effective ba	2	0.8	681.5
21	BUppB	110.0	14.7	3.7	10/29/2003	effective basin	2	4.5	565.4	10	BTJ	90.0	12.9	3.0	9/22/2004	near BO ch	1	8.2	NMI
21	BUppC	110.0	14.7	3.7	10/29/2003	effective basin	2	3.0	383.3	15	AO	50.0	7.1	1.7	9/22/2004	effective ba	2	-0.8	529.1
21	BUppD	110.0	14.7	3.7	10/29/2003	effective basin	2	1.5	147.6	21	BCppH	50.0	7.1	1.7	9/22/2004	effective ba	2	-1.4	367.3
21	BUppE	110.0	14.7	3.7	10/29/2003	effective basin	2	0.9	202.8	21	BCppI	50.0	7.1	1.7	9/22/2004	effective ba	2	-2.0	294.8
21	BUppF	110.0	14.7	3.7	10/29/2003	effective basin	2	0.2	266.7	19	BCppJ	50.0	7.1	1.7	9/22/2004	effective ba	1	7.3	337.0
21	BUppG	110.0	14.7	3.7	10/29/2003	effective basin	2	-0.4	196.5	20	BTppA	50.0	7.1	1.7	9/22/2004	effective ba	2	5.0	187.3
21	BUppH	110.0	14.7	3.7	10/29/2003	effective basin	2	-1.0	175.6	20	BTppB	50.0	7.1	1.7	9/22/2004	effective ba	2	3.5	376.3
20	BYppD	130	17	4	10/29/2003	effective basin	2	1.3	271.6	20	BTppC	60.0	8.6	2.0	9/22/2004	effective ba	2	-4.2	233.9
20	BYppE	130	17	4	10/29/2003	effective basin	2	0.7	266.3	20	BTppK	80.0	11.4	2.7	9/24/2004	effective ba	2	1.7	141.4
20	BYppF	130	17	4	10/29/2003	effective basin	2	0.0	455.0	20	BMppI	15.0	2.1	0.5	9/26/2004	effective ba	1	8.0	306.0
20	BYppG	130	17	4	10/29/2003	effective basin	2	-0.6	18.2	18	AP	30.0	4.3	1.0	9/26/2004	effective ba	2	1.1	563.0
20	BYppH	130	17	4	10/29/2003	effective basin	2	-1.2	242.0	22	BCi	30.0	4.3	1.0	9/26/2004	effective ba	2	4.1	323.3
12	AJ	11.0	1.6	0.4	10/31/2003	crest of basin, comes down slope	1	8.0	247.0	21	BCppC	30.0	4.3	1.0	9/26/2004	N of WB ls	1	7.6	252.0
20	BMc	11.0	1.6	0.4	10/31/2003	effective basin	2	3.0	575.0	20	BG	30.0	4.3	1.0	9/26/2004	effective ba	2	2.3	577.9
20	BMppG	11.0	1.6	0.4	10/31/2003	effective basin	2	2.9	1097.2	20	BMppH	13.0	1.9	0.4	9/27/2004	effective ba	2	2.6	430.0
9	AD	150.0	21.4	5.0	11/1/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	381.0	21	BCppD	40.0	5.7	1.3	9/27/2004	effective ba	2	1.0	654.1
16	AS	80.0	11.4	2.7	11/1/2003	area 12 (south shoulder of EB lane)	1	7.4	1377.0	21	BCppE	40.0	5.7	1.3	9/27/2004	effective ba	2	0.4	484.1
19	BMD	10.0	1.4	0.3	11/1/2003	effective basin	2	2.1	319.0	21	BCppF	40.0	5.7	1.3	9/27/2004	effective ba	2	-0.2	713.1
19	BN	10.0	1.4	0.3	11/1/2003	effective basin	2	1.8	497.0	21	BCppG	40.0	5.7	1.3	9/27/2004	effective ba	2	-2.6	420.8
21	BUppI	120	16	4	11/1/2003	effective basin	2	-1.6	147.5	20	BTppJ	75.0	10.7	2.5	9/28/2004	effective ba	2	2.9	1072.4
20	BYppA	120	17	4	11/1/2003	effective basin	1	5.8	323.6	20	BMppG	-11.0	1.6	0.4	9/30/2004	effective ba	2	-0.2	282.0
20	BYppB	120	16	4	11/1/2003	effective basin	2	4.3	280.8	19	BCJ	42.0	6.0	1.4	9/30/2004	effective ba	2	3.6	1023.3
20	BYppC	120	16	4	11/1/2003	effective basin	2	2.8	255.8	20	BMppF	9.0	1.3	0.3					
20	BYppD	150.0	20.0	5.0	11/1/2003	effective basin	2	-3.3	139.9	16	AS	80.0	11.4	2.7	10/1/2004	area 12 (sou	1	7.4	80.0
20	BMB	9.0	1.3	0.3	11/2/2003	effective basin	2	3.9	340.0	18	BCg	25.0	3.6	0.8	10/1/2004	effective ba	2	2.9	214.0
20	BMppF	9.0	1.3	0.3	11/2/2003	effective basin	2	3.6	1139.4	21	BCppA	25.0	3.6	0.8	10/1/2004	effective ba	1	7.1	743.8
20	BYppI	140.0	18.7	4.7	11/2/2003	effective basin	2	-1.8	178.0	21	BCppB	25.0	3.6	0.8	10/1/2004	effective ba	1	5.6	161.6
20	BMppE	8.0	1.1	0.3	11/3/2003	effective basin	2	4.2	1519.2	20	BMppE	8.0	1.1	0.3	10/1/2004	effective ba	2	4.2	658.8
20	BYppD	130.0	17.3	4.3	11/3/2003	effective basin	2	1.3	267.4	20	BMppC	25.0	3.6	0.8	10/1/2004	effective ba	2	-0.7	184.7
20	BYppE	130.0	17.3	4.3	11/3/2003	effective basin	2	0.7	257.5	20	BMppK	80.0	11.4	2.7	10/1/2004	effective ba	2	-4.2	245.9
20	BYppF	130.0	17.3	4.3	11/3/2003	effective basin	2	0.0	429.2	20	BTppK	80.0	11.4	2.7	10/2/2004	effective ba	2	0.2	405.0
20	BYppG	130.0	17.3	4.3	11/3/2003	effective basin	2	-0.6	18.3	9	BCd	40.0	5.7	1.3	10/2/2004	effective ba	2	-1.6	210.0
20	BYppH	130.0	17.3	4.3	11/3/2003	effective basin	2	-1.2	262.3	9	BCe	40.0	5.7	1.3	10/2/2004	effective ba	2	2.6	734.2
21	BCppC	30.0	4.3	1.0	11/4/2003	effective basin	2	4.1	277.8	21	BCppD	40.0	5.7	1.3	10/2/2004	effective ba	2	1.0	676.6
19	BMA	7.0	1.0	0.2	11/4/2003	effective basin	1	4.8	380.0	21	BCppE	40.0	5.7	1.3	10/2/2004	effective ba	2	0.4	494.1
20	BTppK	80.0	11.4	2.7	11/4/2003	effective basin	2	-4.2	141.9	21	BCppF	40.0	5.7	1.3	10/2/2004	effective ba	2	-0.2	717.1
20	ATppC	6.0	0.9	0.2	11/5/2003	effective basin	2	4.7	271.9	21	BCppG	40.0	5.7	1.3	10/2/2004	effective ba	2	-0.8	458.8
20	BMppD	6.0	0.9	0.2	11/5/2003	effective basin	2	4.8	1012.8	21	BCppH	50.0	7.1	1.7	10/2/2004	effective ba	2	-1.4	391.9
20	ATppB	5.0	0.7	0.2	11/6/2003	effective basin	1	5.3	1840.4	21	BCppI	50.0	7.1	1.7	10/2/2004	effective ba	2	-2.0	333.4
21	BCJ	42	6	1	11/6/2003	effective basin	1	-0.2	126.0	21	BCppJ	50.0	7.1	1.7	10/2/2004	effective ba	1	6.5	343.3
20	BMppC	5.0	0.7	0.2	11/6/2003	effective basin	1	5.4	844.0	20	BTppB	50.0	7.1	1.7	10/2/2004	effective ba	2	5.0	215.5
20	BYppJ	150.0	20.0	5.0	11/6/2003	effective basin	2	-3.3	193.2	20	BTppC	70.0	10.0	2.3	10/2/2004	effective ba	2	1.9	707.0
10	AI	200.0	28.6	6.7	11/7/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	579.0	20	BTppD	70.0	10.0	2.3	10/2/2004	effective ba	2	1.3	658.8
20	BTppC	60.0	8.6	2.0	11/7/2003	effective basin	2	3.5	309.3	20	BTppE	70.0	10.0	2.3	10/2/2004	effective ba	2	0.7	541.8
20	ATppA	3.0	0.4	0.1	11/8/2003	effective basin	1	6.8	333.4	20	BTppF	70.0	10.0	2.3	10/2/2004	effective ba	2	0.1	297.9
20	BCd	40	6	1	11/8/2003	effective basin	2	0.2	239.0	20	BTppG	70.0	10.0	2.3	10/2/2004	effective ba	2	-0.5	404.5
20	BCe	40	6	1	11/8/2003	effective basin	2	-1.6	144.0	20	BTppH	70.0	10.0	2.3	10/2/2004	effective ba	2	-1.1	512.4
21	BCppD	40.0	5.7	1.3	11/8/2003	effective basin	2	2.6	339.1	20	BTppI	70.0	10.0	2.3	10/3/2004	effective ba	2	4.7	5154.3
21	BCppE	40.0	5.7	1.3	11/8/2003	effective basin	2	1.0	511.1	20	ATppC	6.0	0.9	0.2	10/3/2004	effective ba	2	4.8	954.0
21	BCppF	40.0	5.7	1.3	11/8/2003	effective basin	2	0.4	345.0	20	BMppD	6.0	0.9	0.2	10/4/2004	effective ba	1	5.3	3012.4
21	BCppG	40.0	5.7	1.3	11/8/2003	effective basin	2	-0.2	979.9	20	ATppB	5.0	0.7	0.2	10/4/2004	effective ba	1	5.4	705.3
21	BMppB	3.0	0.4	0.1	11/8/2003	effective basin	1	6.0	1772.4	20	BMppC	5.0	0.7	0.2	10/6/2004	effective ba	1	6.8	1077.5
21	BUppI	120	16	4	11/8/2003	effective basin	2	-1.6	332.8	20	ATppA	3.0	0.4	0.1	10/6/2004	effective ba	1	6.0	96.0
20	BYppA	120	17	4	11/8/2003	effective basin	1	5.8	294.1	21	BCa	20.0	2.9	0.7	10/6/2004	effective ba	2	3.6	222.0
20	BYppB	120	16	4	11/8/2003	effective basin	2	4.3	276.8	9	BCb	20.0	2.9	0.7	10/6/2004	effective ba	2	2.0	387.0
20	BYppC	120	16	4	11/8/2003	effective basin	2	2.8	229.3	18	BCc	20.0	2.9	0.7	10/6/2004	effective ba	1	5.6	127.0
20	AT	2.0	0.3	0.1	11/9/2003	effective basin	1	7.3	319.0	19	BD	20.0	2.9	0.7	10/6/2004	effective ba	1	6.0	104.1
21	BCppA	25.0	3.6	0.8	11/9/2003	effective basin	1	7.1	528.0	20	BMppB	3.0	0.4	0.1	10/6/2004	effective ba	2	-2.6	484.1
21	BCppB	25.0	3.6	0.8	11/9/2003	effective basin	1	5.6	501.3	20	BTppJ	70.0	10.7	2.5	10/6/2004	effective ba	2	4.1	374.5
21	BMppK	25.0	3.6	0.8	11/9/2003	effective basin	2	-0.7	236.3	8	AB	35.0	5.0	1.2	10/7/2004	west of rest	1	8.0	250.0
20	BTppJ	75.0	10.7	2.5	11/9/2003	effective basin	2	-2.6	290.4	21	BCppC	30.0	4.3	1.0	10/7/2004	effective ba	2	-0.5	105.1
20	BMppA	1.0	0.1	0.0	11/10/2003	effective basin	1	6.9	270.1	20	BE	35.0	5.0	1.2	10/8/2004	effective ba	1	6.9	359.4
20	BTg	70.0	10.0	2.3	11/11/2003	effective basin	2	-0.1	231.0	20	BMppJ	18.0	2.6	0.6	10/9/2004	effective ba	1	5.0	159.0
20	BTh	70.0	10.0	2.3	11/11/2003	effective basin	2	-1.0	208.0	19	BCh	17.0	2.4	0.6	10/9/2004	effective ba	2	1.5	159.0
21	BUppA	110	15	4	11/11/2003	effective basin	1	6.0	947.0	20	BMc	17.0	2.4	0.6					
21	BUppB	110	15	4	11/11/2003	effective basin	2	4.5	555.1										

Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above mal	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above mal	SpecCond uS/cm
21	BUppC	110	15	4	11/11/2003	effective basin	2	3.0	493.1	18	BCF	15.0	2.1	0.5	10/11/2004	effective ba	1	6.8	91.0
21	BUppD	110	15	4	11/11/2003	effective basin	2	1.5	228.1	20	BMppI	15.0	2.1	0.5	10/11/2004	effective ba	2	1.7	1349.7
21	BUppE	110	15	4	11/11/2003	effective basin	2	0.9	181.1	9	BTg	70.0	10.0	2.3	10/11/2004	effective ba	2	-0.1	297.0
21	BUppF	110	15	4	11/11/2003	effective basin	2	0.2	173.4	21	BTH	70.0	10.0	2.3	10/11/2004	effective ba	2	-1.0	306.0
21	BUppG	110	15	4	11/11/2003	effective basin	2	-0.4	172.0	20	BTppD	70.0	10.0	2.3	10/11/2004	effective ba	2	1.9	612.6
21	BUppH	110	15	4	11/11/2003	effective basin	2	-1.0	451.5	20	BTppE	70.0	10.0	2.3	10/11/2004	effective ba	2	1.3	449.9
20	BYppI	140.0	18.7	4.7	11/11/2003	effective basin	2	-1.8	133.5	20	BTppF	70.0	10.0	2.3	10/11/2004	effective ba	2	0.7	509.9
7	AA	160.0	22.9	5.3	11/12/2003	rest area	1	8.4	192.0	20	BTppG	70.0	10.0	2.3	10/11/2004	effective ba	2	-0.5	344.1
20	BYppD	130.0	17.3	4.3	11/12/2003	effective basin	2	1.3	255.1	20	BTppH	70.0	10.0	2.3	10/11/2004	effective ba	2	-1.1	482.8
20	BYppE	130.0	17.3	4.3	11/12/2003	effective basin	2	0.7	205.4	18	AP	30.0	4.3	1.0	10/12/2004	effective ba	1	8.0	197.0
20	BYppF	130.0	17.3	4.3	11/12/2003	effective basin	2	0.0	224.5	22	BCi	30.0	4.3	1.0	10/12/2004	effective ba	2	1.1	230.0
20	BYppG	130.0	17.3	4.3	11/12/2003	effective basin	2	-0.6	15.1	21	BCppA	25.0	3.6	0.8	10/12/2004	effective ba	1	7.1	782.6
20	BYppH	130.0	17.3	4.3	11/12/2003	effective basin	2	-1.2	211.8	21	BCppB	25.0	3.6	0.8	10/12/2004	effective ba	1	5.6	145.1
20	BYppI	150.0	20.0	5.0	11/12/2003	effective basin	2	-3.3	234.9	21	BCppC	30.0	4.3	1.0	10/12/2004	effective ba	2	4.1	560.5
8	CA	160.0	22.9	5.3	11/12/2003	rest area, near E BC	1	6.1	511.0	21	BCppD	40.0	5.7	1.3	10/12/2004	effective ba	2	2.6	754.3
8	AB	35	5	1	11/13/2003	west of rest area, runoff slope	1	8.0	305.0	21	BCppE	40.0	5.7	1.3	10/12/2004	effective ba	2	1.0	599.6
21	BE	35	5	1	11/13/2003	effective basin	2	-0.5	114.0	21	BCppF	40.0	5.7	1.3	10/12/2004	effective ba	2	0.4	570.4
20	BTf	68.0	9.7	2.3	11/13/2003	effective basin	2	0.7	205.0	21	BCppG	40.0	5.7	1.3	10/12/2004	effective ba	2	-0.2	999.9
20	BTppK	80.0	11.4	2.7	11/13/2003	effective basin	2	-4.2	117.9	20	BQ	30.0	4.3	1.0	10/12/2004	N of WB la	1	7.6	243.0
21	BUppI	120.0	16.0	4.0	11/13/2003	effective basin	2	-1.6	200.7	20	BMppK	25.0	3.6	0.8	10/12/2004	effective ba	2	-0.7	307.8
20	BYppA	120.0	17.1	4.0	11/13/2003	effective basin	1	5.8	254.5	20	BTppC	60.0	8.6	2.0	10/12/2004	effective ba	2	3.5	233.3
20	BYppB	120.0	16.0	4.0	11/13/2003	effective basin	2	4.3	199.3	20	BMppH	13.0	1.9	0.4	10/13/2004	effective ba	2	2.3	835.4
20	BYppC	120.0	16.0	4.0	11/13/2003	effective basin	2	2.8	202.1	22	BTf	68.0	9.7	2.3	10/13/2004	effective ba	2	0.7	280.0
20	BTppD	70.0	10.0	2.3	11/14/2003	effective basin	2	1.9	700.4	20	BMc	11.0	1.6	0.4	10/15/2004	effective ba	2	3.0	352.0
20	BTppE	70.0	10.0	2.3	11/14/2003	effective basin	2	1.3	524.0	20	BMppG	11.0	1.6	0.4	10/15/2004	effective ba	2	2.9	1166.8
20	BTppF	70.0	10.0	2.3	11/14/2003	effective basin	2	0.7	262.3	20	BMD	10.0	1.4	0.3	10/16/2004	effective ba	2	2.1	185.0
20	BTppG	70.0	10.0	2.3	11/14/2003	effective basin	2	0.1	296.5	21	BN	10.0	1.4	0.3	10/16/2004	effective ba	2	1.8	308.0
20	BTppH	70.0	10.0	2.3	11/14/2003	effective basin	2	-0.5	215.0	21	BTa	65.0	9.3	2.2	10/16/2004	effective ba	1	5.4	187.0
20	BTppI	70.0	10.0	2.3	11/14/2003	effective basin	2	-1.1	1429.8	21	BTb	65.0	9.3	2.2	10/16/2004	effective ba	2	4.4	509.0
11	AK	240.0	34.3	8.0	11/16/2003	@ E BC, east of median 13 area	1	7.4	365.0	21	BTc	65.0	9.3	2.2	10/16/2004	effective ba	2	3.6	533.0
20	BMppJ	18.0	2.6	0.6	11/16/2003	effective basin	2	0.8	185.7	22	BTd	65.0	9.3	2.2	10/16/2004	effective ba	2	2.7	513.0
21	BTa	65.0	9.3	2.2	11/16/2003	effective basin	1	5.4	292.0	22	BTc	65.0	9.3	2.2	10/16/2004	effective ba	2	1.7	249.0
21	BTb	65.0	9.3	2.2	11/16/2003	effective basin	2	4.4	361.0	18	BCg	25.0	3.6	0.8	10/17/2004	effective ba	2	2.9	287.0
21	BTc	65.0	9.3	2.2	11/16/2003	effective basin	2	3.6	389.0	21	BCppA	25.0	3.6	0.8	10/17/2004	effective ba	1	7.1	697.9
21	BTd	65.0	9.3	2.2	11/16/2003	effective basin	2	2.7	296.0	21	BCppB	25.0	3.6	0.8	10/17/2004	effective ba	1	5.6	131.1
20	BTc	65.0	9.3	2.2	11/16/2003	effective basin	2	1.7	241.0	20	BMB	9.0	1.3	0.3	10/17/2004	effective ba	2	3.9	244.0
20	BYppI	140.0	18.7	4.7	11/16/2003	effective basin	2	-1.8	167.3	20	BMppF	9.0	1.3	0.3	10/17/2004	effective ba	2	3.6	978.9
19	CB	240.0	34.3	8.0	11/16/2003	N of WB lane, near 4 UG wells across rd	1	8.6	500.0	20	BMppK	25.0	3.6	0.8	10/17/2004	effective ba	2	-0.7	480.3
9	AC	190.0	27.1	6.3	11/17/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.2	155.0	20	BMppE	8.0	1.1	0.3	10/18/2004	effective ba	2	4.2	1359.6
21	BCppH	50.0	7.1	1.7	11/17/2003	effective basin	2	-0.8	4729.4	20	BMe	7.0	1.0	0.2	10/19/2004	effective ba	1	4.8	341.0
21	BCppI	50.0	7.1	1.7	11/17/2003	effective basin	2	-1.4	1787.3	20	BMppJ	18.0	2.6	0.6	10/19/2004	effective ba	2	0.8	424.9
21	BCppJ	50.0	7.1	1.7	11/17/2003	effective basin	2	-2.0	2281.5	20	ATppC	6.0	0.9	0.2	10/20/2004	effective ba	2	4.7	592.6
20	BTppA	50.0	7.1	1.7	11/17/2003	effective basin	1	6.5	217.5	20	BMppD	6.0	0.9	0.2	10/20/2004	effective ba	2	4.8	1881.3
20	BTppB	50.0	7.1	1.7	11/17/2003	effective basin	2	5.0	260.0	20	ATppB	5.0	0.7	0.2	10/21/2004	effective ba	1	5.3	3232.5
18	AP	30	4	1	11/18/2003	effective basin	1	8.0	249.0	20	BMppC	5.0	0.7	0.2	10/21/2004	effective ba	1	5.4	808.1
20	BCi	30	4	1	11/18/2003	effective basin	2	1.1	369.0	20	BTppC	60.0	8.6	2.0	10/21/2004	effective ba	2	3.5	253.6
21	BCppC	30.0	4.3	1.0	11/18/2003	effective basin	2	4.1	163.3	21	BCa	20.0	2.9	0.7	10/22/2004	effective ba	1	6.0	63.0
22	BG	30	4	1	11/18/2003	effective basin	1	7.6	453.0	9	BCb	20.0	2.9	0.7	10/22/2004	effective ba	2	3.6	107.0
20	BTppJ	75.0	10.7	2.5	11/18/2003	effective basin	2	-2.6	533.4	18	BCc	20.0	2.9	0.7	10/22/2004	effective ba	2	2.0	316.0
21	BUppA	110	15	4	11/18/2003	effective basin	1	6.0	287.3	21	BCppC	30.0	4.3	1.0	10/22/2004	effective ba	2	4.1	752.5
21	BUppB	110	15	4	11/18/2003	effective basin	2	4.5	485.4	21	BCppH	50.0	7.1	1.7	10/22/2004	effective ba	2	-0.8	317.8
21	BUppC	110	15	4	11/18/2003	effective basin	2	3.0	402.8	21	BCppI	50.0	7.1	1.7	10/22/2004	effective ba	2	-1.4	267.6
21	BUppD	110	15	4	11/18/2003	effective basin	2	1.5	513.0	21	BCppJ	50.0	7.1	1.7	10/22/2004	effective ba	2	-2.0	196.4
21	BUppE	110	15	4	11/18/2003	effective basin	2	0.9	423.6	19	BD	20.0	2.9	0.7	10/22/2004	effective ba	1	5.6	125.0
21	BUppF	110	15	4	11/18/2003	effective basin	2	0.2	169.9	20	BMppI	15.0	2.1	0.5	10/22/2004	effective ba	2	1.7	1147.1
21	BUppG	110	15	4	11/18/2003	effective basin	2	-0.4	178.5	20	BTppA	50.0	7.1	1.7	10/22/2004	effective ba	1	6.5	258.1
21	BUppH	110	15	4	11/18/2003	effective basin	2	-1.0	168.4	20	BTppB	50.0	7.1	1.7	10/22/2004	effective ba	2	5.0	187.1
20	BMppI	15.0	2.1	0.5	11/19/2003	effective basin	2	1.7	590.8	20	ATppA	3.0	0.4	0.1	10/23/2004	effective ba	1	6.8	772.4
20	BTppK	80.0	11.4	2.7	11/20/2003	effective basin	2	-4.2	119.4	20	BMppB	3.0	0.4	0.1	10/23/2004	effective ba	1	6.0	161.6
12	AG	130.0	18.6	4.3	11/21/2003	area 12 (south shoulder of EB lane)	1	7.3	2182.0	20	AT	2.0	0.3	0.1	10/24/2004	effective ba	1	7.3	542.0
20	BMppH	13.0	1.9	0.4	11/21/2003	effective basin	2	2.3	675.2	20	BMppH	13.0	1.9	0.4	10/24/2004	effective ba	2	2.3	577.9
20	BYppD	130.0	17.3	4.3	11/21/2003	effective basin	2	1.3	309.9	20	BMppJ	18.0	2.6	0.6	10/24/2004	effective ba	2	0.8	412.8
20	BYppE	130.0	17.3	4.3	11/21/2003	effective basin	2	0.7	196.7	19	BCh	17.0	2.4	0.6	10/25/2004	effective ba	1	5.0	99.0
20	BYppF	130.0	17.3	4.3	11/21/2003	effective basin	2	0.0	223.3	20	BMe	17.0	2.4	0.6	10/25/2004	effective ba	2	1.5	263.0
20	BYppG	130.0	17.3	4.3	11/21/2003	effective basin	2	-0.6	12.1	20	BMppA	1.0	0.1	0.0	10/25/2004	effective ba	1	6.9	343.3
20	BYppH	130.0	17.3	4.3	11/21/2003	effective basin	2	-1.2	163.4	20	BMppG	11.0	1.6	0.4	10/26/2004	effective ba	2	2.9	772.5
9	AD	150.0	21.4	5.0	11/22/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	389.0	18	BCf	15.0	2.1	0.5	10/27/2004	effective ba	1	6.8	69.0
21	BUppI	120.0	16.0	4.0	11/22/2003	effective basin	2	-1.6	422.5	21	BCppA	25.0	3.6	0.8	10/27/2004	effective ba	1	7.1	915.4
20	BYppA	120.0																	

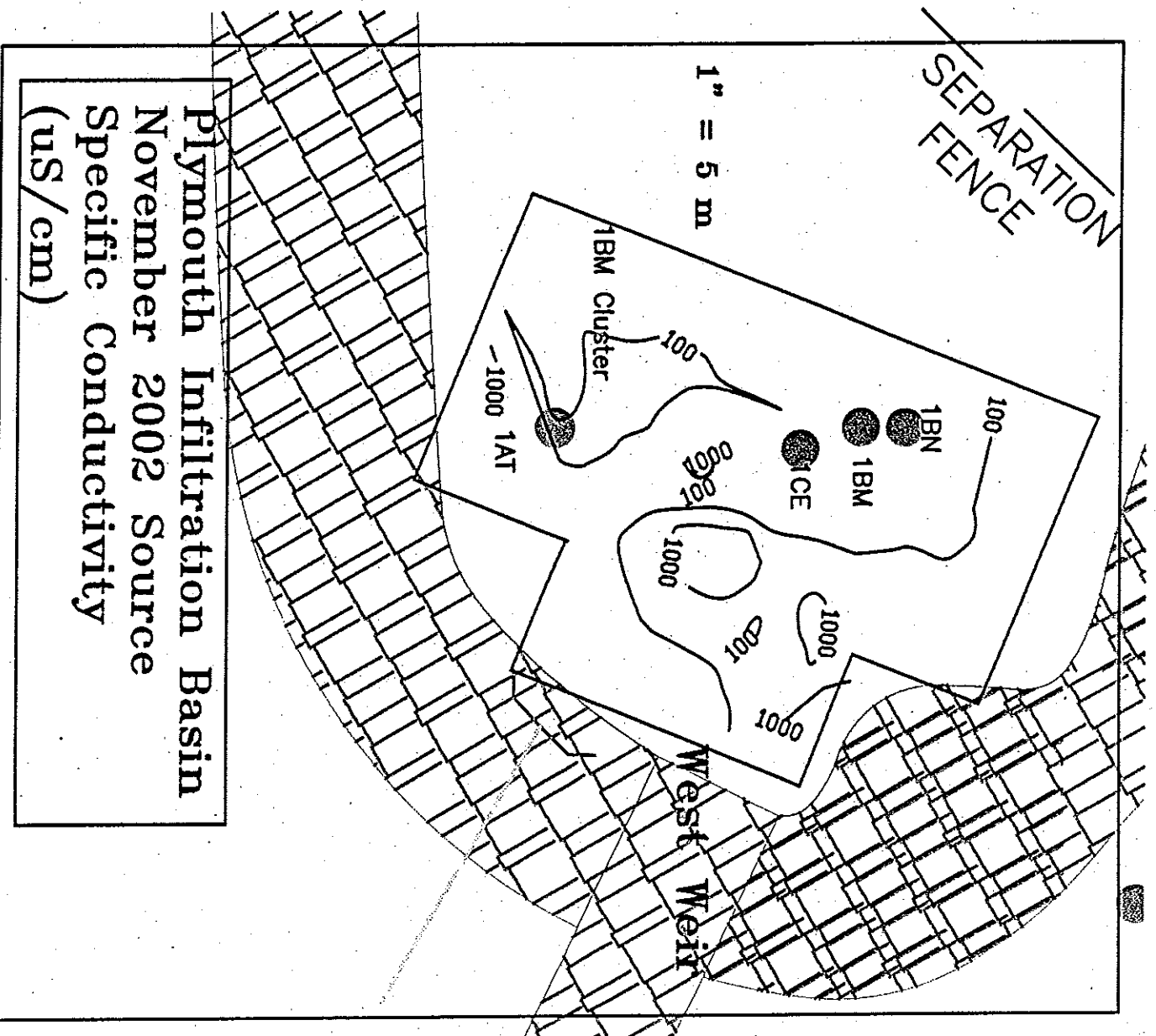
Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm	Row	Well	days	Travel time wks	mos	origin date	Origin	Layer #	Sampling d m above msl	SpecCond uS/cm
20	BYppcC	120.0	16.0	4.0	11/22/2003	effective basin	2	2.8	243.2	20	BMppcK	25.0	3.6	0.8	10/27/2004	effective ba	2	-0.7	27.5
20	BYppcI	140.0	18.7	4.7	11/22/2003	effective basin	2	-1.8	339.0	20	BMppcF	9.0	1.3	0.3	10/28/2004	effective ba	2	3.6	1028.7
20	BYppcJ	150	20	5	11/22/2003	effective basin	2	-3.3	296.4	20	BMppcE	8.0	1.1	0.3	10/29/2004	effective ba	2	4.2	1144.7
20	BCg	25	4	1	11/23/2003	effective basin	2	2.9	283.0	20	BMppcH	13.0	1.9	0.4	10/31/2004	crest of bas	1	2.3	445.6
21	BCppcA	25.0	3.6	0.8	11/23/2003	effective basin	1	7.1	965.9	12	AJ	11.0	1.6	0.4	10/31/2004	near BO ch	1	8.0	NM
21	BCppcB	25.0	3.6	0.8	11/23/2003	effective basin	1	5.6	288.9	15	AO	50.0	7.1	1.7	10/31/2004	effective ba	2	8.2	252.0
20	BMppcG	11.0	1.6	0.4	11/23/2003	effective basin	2	2.9	590.8	20	ATppcC	6.0	0.9	0.2	10/31/2004	effective ba	2	4.7	428.0
20	BMppcK	25.0	3.6	0.8	11/23/2003	effective basin	2	-0.7	211.0	21	BCppcH	50.0	7.1	1.7	10/31/2004	effective ba	2	-0.8	286.8
20	BTppcD	70.0	10.0	2.3	11/23/2003	effective basin	2	1.9	1167.4	21	BCppcI	50.0	7.1	1.7	10/31/2004	effective ba	2	-1.4	241.4
20	BTppcE	70.0	10.0	2.3	11/23/2003	effective basin	2	1.3	1717.6	21	BCppcJ	50.0	7.1	1.7	10/31/2004	effective ba	2	-2.0	181.5
20	BTppcF	70.0	10.0	2.3	11/23/2003	effective basin	2	0.7	455.0	20	BMc	11.0	1.6	0.4	10/31/2004	effective ba	2	3.0	247.0
20	BTppcG	70.0	10.0	2.3	11/23/2003	effective basin	2	0.1	937.9	20	BMppcD	6.0	0.9	0.2	10/31/2004	effective ba	2	4.8	913.8
20	BTppcH	70.0	10.0	2.3	11/23/2003	effective basin	2	-0.5	1373.8	20	BMppcG	11.0	1.6	0.4	10/31/2004	effective ba	2	2.9	606.8
20	BTppcI	70.0	10.0	2.3	11/23/2003	effective basin	2	-1.1	804.3	19	BTk	50.0	7.1	1.7	10/31/2004	effective ba	1	7.3	266.0
21	BUppcA	110.0	14.7	3.7	11/23/2003	effective basin	1	6.0	268.7	20	BTppcA	50.0	7.1	1.7	10/31/2004	effective ba	1	6.5	309.0
21	BUppcB	110.0	14.7	3.7	11/23/2003	effective basin	2	4.5	465.0	20	BTppcB	50.0	7.1	1.7	10/31/2004	effective ba	2	5.0	170.4
21	BUppcC	110.0	14.7	3.7	11/23/2003	effective basin	2	3.0	568.4	20	ATppcB	5.0	0.7	0.2	11/1/2004	effective ba	1	5.3	2633.8
21	BUppcD	110.0	14.7	3.7	11/23/2003	effective basin	2	1.5	676.3	21	BCppcD	40.0	5.7	1.3	11/1/2004	effective ba	2	2.6	761.4
21	BUppcE	110.0	14.7	3.7	11/23/2003	effective basin	2	0.9	613.2	21	BCppcE	40.0	5.7	1.3	11/1/2004	effective ba	2	1.0	3568.5
21	BUppcF	110.0	14.7	3.7	11/23/2003	effective basin	2	0.2	183.9	21	BCppcF	40.0	5.7	1.3	11/1/2004	effective ba	2	0.4	571.9
21	BUppcG	110.0	14.7	3.7	11/23/2003	effective basin	2	-0.4	183.5	21	BCppcG	40.0	5.7	1.3	11/1/2004	effective ba	2	-0.2	774.5
21	BUppcH	110.0	14.7	3.7	11/23/2003	effective basin	2	-1.0	152.5	21	BMc	10.0	1.4	0.3	11/1/2004	effective ba	2	2.1	116.0
20	BTppcC	60.0	8.6	2.0	11/24/2003	effective basin	2	3.5	209.6	20	BMd	5.0	0.7	0.2	11/1/2004	effective ba	1	5.4	802.5
14	AN	210.0	30.0	7.0	11/25/2003	area 12 (south shoulder of EB lane)	1	8.0	757.0	20	BMppcC	5.0	0.7	0.2	11/1/2004	effective ba	2	1.8	240.0
20	BMppcF	9.0	1.3	0.3	11/25/2003	effective basin	2	3.6	844.0	21	BN	10.0	1.4	0.3	11/2/2004	effective ba	2	3.9	376.0
20	BTppcJ	75.0	10.7	2.5	11/25/2003	effective basin	2	-2.6	760.7	20	BMc	9.0	1.3	0.3	11/2/2004	effective ba	2	3.6	823.5
13	AH	90.0	12.9	3.0	11/26/2003	area 12 (south shoulder of EB lane)	1	7.4	NS	20	BMppcF	9.0	1.3	0.3	11/2/2004	effective ba	1	6.8	511.7
20	BMppcE	8.0	1.1	0.3	11/26/2003	effective basin	2	4.2	1097.2	20	ATppcA	3.0	0.4	0.1	11/3/2004	effective ba	1	6.0	209.6
20	BTj	90.0	12.9	3.0	11/26/2003	effective basin	2	-3.7	124.0	20	BMppcB	3.0	0.4	0.1	11/3/2004	effective ba	2	4.2	866.1
20	BYppcD	130.0	17.3	4.3	11/26/2003	effective basin	2	1.3	541.3	20	BMppcE	8.0	1.1	0.3	11/3/2004	effective ba	2	0.8	19.4
20	BYppcE	130.0	17.3	4.3	11/26/2003	effective basin	2	0.7	601.7	20	BMA	7.0	1.0	0.2	11/4/2004	effective ba	1	4.8	284.0
20	BYppcF	130.0	17.3	4.3	11/26/2003	effective basin	2	0.0	522.6	20	ATppcC	6.0	0.9	0.2	11/5/2004	effective ba	2	4.7	266.9
20	BYppcG	130.0	17.3	4.3	11/26/2003	effective basin	2	-0.6	15.5	20	BMppcD	1.0	0.1	0.0	11/5/2004	effective ba	1	6.9	114.4
20	BYppcH	130.0	17.3	4.3	11/26/2003	effective basin	2	-1.2	265.8	20	BMppcD	6.0	0.9	0.2	11/5/2004	effective ba	2	4.8	1794.7
21	BCppcD	40.0	5.7	1.3	11/27/2003	effective basin	2	2.6	339.1	20	BMppcD	5.0	0.7	0.2	11/6/2004	effective ba	1	5.3	2514.6
21	BCppcE	40.0	5.7	1.3	11/27/2003	effective basin	2	1.0	4248.9	20	ATppcB	5.0	0.7	0.2	11/6/2004	effective ba	1	5.4	1441.2
21	BCppcF	40.0	5.7	1.3	11/27/2003	effective basin	2	0.4	5240.1	20	BMppcC	5.0	0.7	0.2	11/6/2004	effective ba	1	1.7	289.6
21	BCppcG	40.0	5.7	1.3	11/27/2003	effective basin	2	-0.2	4106.7	20	BMppcI	15.0	2.1	0.5	11/8/2004	effective ba	2	6.8	670.0
20	ATppcC	6.0	0.9	0.2	11/28/2003	effective basin	2	4.7	188.9	20	ATppcA	3.0	0.4	0.1	11/8/2004	effective ba	2	-0.2	199.0
19	BCa	20	3	1	11/28/2003	effective basin	1	6.0	185.0	19	BCj	42.0	6.0	1.4	11/8/2004	effective ba	1	6.0	198.0
19	BCb	20	3	1	11/28/2003	effective basin	2	3.6	253.0	20	BMppcB	3.0	0.4	0.1	11/8/2004	effective ba	2	2.3	17.2
19	BCc	20	3	1	11/28/2003	effective basin	2	2.0	476.0	20	BMppcH	13.0	1.9	0.4	11/8/2004	effective ba	1	7.3	315.0
20	BCd	20	3	1	11/28/2003	effective basin	1	5.6	146.0	20	AT	2.0	0.3	0.1	11/9/2004	effective ba	2	0.2	362.0
21	BD	20	3	1	11/28/2003	effective basin	2	4.8	1645.3	9	BCd	40.0	5.7	1.3	11/10/2004	effective ba	2	-1.6	304.0
20	BMppcD	6.0	0.9	0.2	11/28/2003	effective basin	2	-4.2	169.6	9	BCe	40.0	5.7	1.3	11/10/2004	effective ba	2	2.6	445.6
20	BTppcK	80.0	11.4	2.7	11/28/2003	effective basin	1	5.3	2172.1	21	BCppcD	40.0	5.7	1.3	11/10/2004	effective ba	2	1.0	731.1
20	ATppcB	5.0	0.7	0.2	11/29/2003	effective basin	1	5.4	844.0	21	BCppcE	40.0	5.7	1.3	11/10/2004	effective ba	2	0.4	566.5
20	BMppcC	5.0	0.7	0.2	11/29/2003	effective basin	2	0.8	211.0	21	BCppcF	40.0	5.7	1.3	11/10/2004	effective ba	2	-0.2	815.1
20	BMppcJ	18.0	2.6	0.6	11/30/2003	effective basin	2	1.9	1959.8	21	BCppcG	40.0	5.7	1.3	11/10/2004	effective ba	1	6.9	167.5
20	BTppcD	70.0	10.0	2.3	11/30/2003	effective basin	2	1.3	2421.0	20	BMppcA	1.0	0.1	0.0	11/10/2004	effective ba	2	2.9	82.3
20	BTppcE	70.0	10.0	2.3	11/30/2003	effective basin	2	0.7	1655.4	20	BMppcG	11.0	1.6	0.4	11/10/2004	effective ba	2	4.1	271.3
20	BTppcF	70.0	10.0	2.3	11/30/2003	effective basin	2	0.1	2851.9	21	BCppcC	30.0	4.3	1.0	11/11/2004	effective ba	2	3.6	222.1
20	BTppcG	70.0	10.0	2.3	11/30/2003	effective basin	2	-0.5	1241.5	20	BMppcF	9.0	1.3	0.3	11/12/2004	effective ba	2	4.2	190.8
20	BTppcH	70.0	10.0	2.3	11/30/2003	effective basin	2	-1.1	1264.6	20	BMppcE	8.0	1.1	0.3	11/13/2004	effective ba	1	8.0	124.0
20	BTppcI	70.0	10.0	2.3	11/30/2003	effective basin	2			8	AB	35.0	5.0	1.2	11/15/2004	west of rest	2	4.7	268.8
14	AF	120.0	17.1	4.0	12/1/2003	area 12 (south shoulder of EB lane)	1	7.3	1732.0	20	ATppcC	6.0	0.9	0.2	11/15/2004	effective ba	2	-0.5	185.0
13	AO	50.0	7.1	1.7	12/1/2003	near BO cluster, not "effective" area	1	8.2	324.0	20	BE	35.0	5.0	1.2	11/15/2004	effective ba	2	4.8	215.5
20	ATppcA	3.0	0.4	0.1	12/1/2003	effective basin	1	6.8	246.4	20	BMppcD	6.0	0.9	0.2	11/16/2004	effective ba	1	5.3	2101.2
20	BCh	17	2	1	12/1/2003	effective basin	1	5.0	209.0	20	ATppcB	5.0	0.7	0.2	11/16/2004	effective ba	1	7.1	850.7
20	BMe	17	2	1	12/1/2003	effective basin	2	1.5	139.0	21	BCppcA	25.0	3.6	0.8	11/16/2004	effective ba	1	5.6	154.1
20	BMppcB	3.0	0.4	0.1	12/1/2003	effective basin	1	6.0	211.0	21	BCppcB	25.0	3.6	0.8	11/16/2004	effective ba	1	5.4	139.8
20	BTk	50.0	7.1	1.7	12/1/2003	effective basin	1	7.3	338.0	20	BMppcC	5.0	0.7	0.2	11/16/2004	effective ba	2	-0.7	155.9
21	BUppcI	120.0	16.0	4.0	12/1/2003	effective basin	2	-1.6	157.7	20	BMppcK	25.0	3.6	0.8	11/16/2004	effective ba	1	6.8	383.3
20	BYppcA	120.0	17.1	4.0	12/1/2003	effective basin	1	5.8	262.2	20	ATppcA	3.0	0.4	0.1	11/18/2004	effective ba	1	6.0	43.1
20	BYppcB	120.0	16.0	4.0	12/1/2003	effective basin	2	4.3	324.6	20	BMppcB	3.0	0.4	0.1	11/20/2004	effective ba	1	8.0	366.0
20	BYppcC	120.0	16.0	4.0	12/1/2003	effective basin	2	2.8	254.0	18	AP	30.0	4.3	1.0	11/20/2004	effective ba	2	1.1	588.0
21	BZ	120.0	17.1	4.0	12/1/2003	effective basin	1	6.7	301.0	22	BCI	30.0	4.3	1.0	11/20/2004	effective ba	2	4.1	333.4
21	BUppcA	110.0	14.7	3.7	12/2/2003	effective basin	1	6.0	593.7	21	BCppcC	30.0	4.3	1.0	11/20/2004	N of			

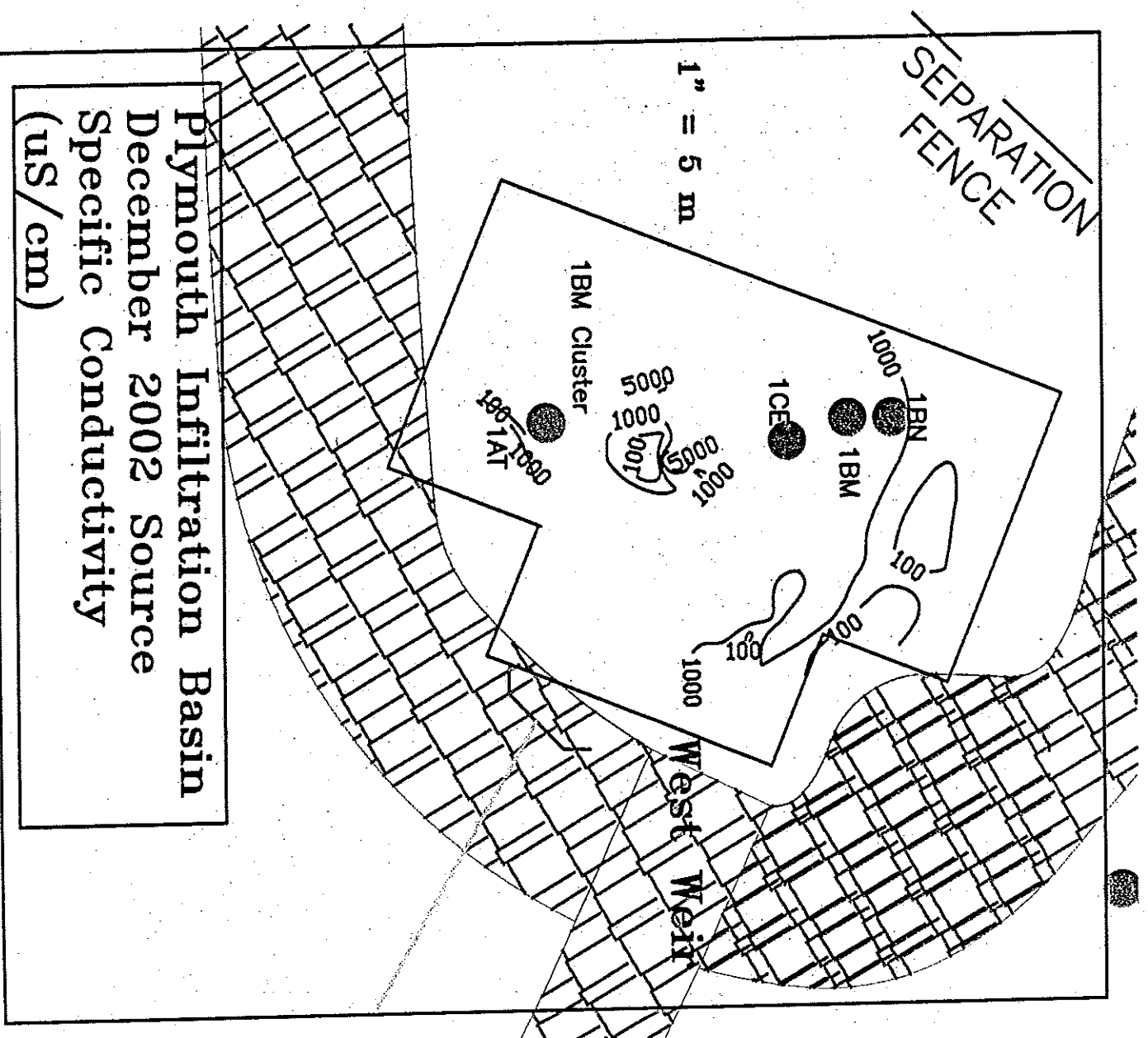
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21	BUppD	110.0	14.7	3.7	12/2/2003	effective basin	2	1.5	522.6	20	BMppJ	18.0	2.6	0.6	11/23/2004	effective ba	2	0.8	336.6
21	BUppE	110.0	14.7	3.7	12/2/2003	effective basin	2	0.9	855.4	18	BCg	25.0	3.6	0.8	11/25/2004	effective ba	2	2.9	241.0
21	BUppF	110.0	14.7	3.7	12/2/2003	effective basin	2	0.2	333.7	21	BCppA	25.0	3.6	0.8	11/25/2004	effective ba	1	7.1	679.9
21	BUppG	110.0	14.7	3.7	12/2/2003	effective basin	2	-0.4	193.6	21	BCppB	25.0	3.6	0.8	11/25/2004	effective ba	1	5.6	284.0
21	BUppH	110.0	14.7	3.7	12/2/2003	effective basin	2	-1.0	184.6	20	BMppK	25.0	3.6	0.8	11/25/2004	effective ba	2	-0.7	245.9
20	BYppD	130.0	17.3	4.3	12/2/2003	effective basin	2	1.3	228.0	20	BMppL	15.0	2.1	0.5	11/26/2004	effective ba	2	1.7	910.9
20	BYppE	130.0	17.3	4.3	12/2/2003	effective basin	2	0.7	375.9	20	BMppH	13.0	1.9	0.4	11/28/2004	effective ba	2	2.3	693.4
20	BYppF	130.0	17.3	4.3	12/2/2003	effective basin	2	0.0	428.1	21	BCa	20.0	2.9	0.7	11/30/2004	effective ba	1	6.0	128.0
20	BYppG	130.0	17.3	4.3	12/2/2003	effective basin	2	-0.6	15.3	9	BCb	20.0	2.9	0.7	11/30/2004	effective ba	2	3.6	165.0
20	BYppH	130.0	17.3	4.3	12/2/2003	effective basin	2	-1.2	368.9	18	BCc	20.0	2.9	0.7	11/30/2004	effective ba	2	2.0	205.0
20	BYppI	140	19	5	12/2/2003	effective basin	2	-1.8	203.6	19	BD	20.0	2.9	0.7	11/30/2004	effective ba	1	5.6	202.0
20	BYppJ	150.0	20.0	5.0	12/2/2003	effective basin	2	-3.3	296.4	20	BMppG	11.0	1.6	0.4	11/30/2004	effective ba	2	2.9	417.0
20	BCf	15	2	1	12/3/2003	effective basin	1	6.8	206.0										
20	BMppA	1.0	0.1	0.0	12/3/2003	effective basin	1	6.9	156.1	20	BMppF	9.0	1.3	0.3	12/2/2004	effective ba	2	3.6	421.4
20	BMppL	15.0	2.1	0.5	12/3/2003	effective basin	2	1.7	506.4	20	BMppJ	18.0	2.6	0.6	12/2/2004	effective ba	2	0.8	363.1
20	BTppC	60.0	8.6	2.0	12/3/2003	effective basin	2	3.5	241.8	19	BCh	17.0	2.4	0.6	12/3/2004	effective ba	1	5.0	216.0
20	BTppJ	75.0	10.7	2.5	12/3/2003	effective basin	2	-2.6	246.2	20	BMe	17.0	2.4	0.6	12/3/2004	effective ba	2	1.5	265.0
21	BCppH	50.0	7.1	1.7	12/4/2003	effective basin	2	-0.8	185.2	20	BMppE	8.0	1.1	0.3	12/3/2004	effective ba	2	4.2	302.0
21	BCppI	50.0	7.1	1.7	12/4/2003	effective basin	2	-1.4	172.8	20	ATppC	6.0	0.9	0.2	12/5/2004	effective ba	2	4.7	2984.1
21	BCppJ	50.0	7.1	1.7	12/4/2003	effective basin	2	-2.0	177.8	18	BCf	15.0	2.1	0.5	12/5/2004	effective ba	1	6.8	164.0
20	BTppA	50.0	7.1	1.7	12/4/2003	effective basin	1	6.5	146.6	20	BMppD	6.0	0.9	0.2	12/5/2004	effective ba	2	4.8	679.8
20	BTppB	50.0	7.1	1.7	12/4/2003	effective basin	2	5.0	153.5	20	BMppI	15.0	2.1	0.5	12/5/2004	effective ba	2	1.7	1146.7
10	AI	200.0	28.6	6.7	12/5/2003	b/w areas 6/16, N of ramp, S of shoulder	1	8.1	242.0	20	ATppB	5.0	0.7	0.2	12/6/2004	effective ba	1	5.3	2228.8
20	BMppH	13.0	1.9	0.4	12/5/2003	effective basin	2	2.3	675.2	20	BMppC	5.0	0.7	0.2	12/6/2004	effective ba	1	5.4	515.4
16	AS	80.0	11.4	2.7	12/6/2003	area 12 (south shoulder of EB lane)	1	7.4	NS	20	BMppH	13.0	1.9	0.4	12/7/2004	effective ba	2	2.3	688.3
21	BUppI	120.0	16.0	4.0	12/6/2003	effective basin	2	-1.6	136.3	20	ATppA	3.0	0.4	0.1	12/8/2004	effective ba	1	6.8	322.7
20	BYppA	120.0	17.1	4.0	12/6/2003	effective basin	1	5.8	326.5	20	BMppB	3.0	0.4	0.1	12/8/2004	effective ba	1	6.0	143.1
20	BYppB	120.0	16.0	4.0	12/6/2003	effective basin	2	4.3	403.2	12	AJ	11.0	1.6	0.4	12/9/2004	crest of bas	1	8.0	183.0
20	BYppC	120.0	16.0	4.0	12/6/2003	effective basin	2	2.8	323.8	20	BMc	11.0	1.6	0.4	12/9/2004	effective ba	2	3.0	176.0
12	AI	11	2	0	12/7/2003	crest of basin, comes down slope	1	8.0	116.0	20	BMppG	11.0	1.6	0.4	12/9/2004	effective ba	2	2.9	1106.2
21	BCppC	30.0	4.3	1.0	12/7/2003	effective basin	2	4.1	2305.8	20	BMD	10.0	1.4	0.3	12/10/2004	effective ba	2	2.1	259.0
20	BMc	11	2	0	12/7/2003	effective basin	2	3.0	267.0	20	BMppA	1.0	0.1	0.0	12/10/2004	effective ba	1	6.9	140.8
20	BMppO	11.0	1.6	0.4	12/7/2003	effective basin	2	2.9	759.6	21	BN	10.0	1.4	0.3	12/10/2004	effective ba	2	1.8	319.0
19	BMD	10	1	0	12/8/2003	effective basin	2	2.1	482.0	20	BMB	9.0	1.3	0.3	12/11/2004	effective ba	2	3.9	323.0
19	BN	10	1	0	12/8/2003	effective basin	2	1.8	232.0	20	BMppF	9.0	1.3	0.3	12/11/2004	effective ba	2	3.6	849.8
20	BTppD	70.0	10.0	2.3	12/8/2003	effective basin	2	1.9	869.0	20	BMppE	8.0	1.1	0.3	12/12/2004	effective ba	2	4.2	506.1
20	BTppE	70.0	10.0	2.3	12/8/2003	effective basin	2	1.3	926.9	20	BMA	7.0	1.0	0.2	12/13/2004	effective ba	1	4.8	286.0
20	BTppF	70.0	10.0	2.3	12/8/2003	effective basin	2	0.7	770.5	20	ATppC	6.0	0.9	0.2	12/14/2004	effective ba	2	4.7	277.8
20	BTppG	70.0	10.0	2.3	12/8/2003	effective basin	2	0.1	528.0	20	BMppD	6.0	0.9	0.2	12/14/2004	effective ba	2	4.8	835.4
20	BTppH	70.0	10.0	2.3	12/8/2003	effective basin	2	-0.5	526.7	20	ATppB	5.0	0.7	0.2	12/15/2004	effective ba	1	5.3	2328.4
20	BTppI	70.0	10.0	2.3	12/8/2003	effective basin	2	-1.1	1219.6	20	BMppC	5.0	0.7	0.2	12/15/2004	effective ba	1	5.4	666.7
21	BCJ	42.0	6.0	1.4	12/9/2003	effective basin	2	-0.2	455.0	20	ATppA	3.0	0.4	0.1	12/17/2004	effective ba	1	6.8	432.7
20	BMB	9	1	0	12/9/2003	effective basin	2	3.9	2087.0	20	BMppB	3.0	0.4	0.1	12/17/2004	effective ba	1	6.0	164.7
20	BMppF	9.0	1.3	0.3	12/9/2003	effective basin	2	3.6	2954.1	20	AT	2.0	0.3	0.1	12/18/2004	effective ba	1	7.3	339.0
20	BMppE	8.0	1.1	0.3	12/10/2003	effective basin	2	4.2	7174.2	20	BMppA	1.0	0.1	0.0	12/19/2004	effective ba	1	6.9	105.1
20	BTppC	60.0	8.6	2.0	12/10/2003	effective basin	2	3.5	902.5										
20	BCd	40.0	5.7	1.3	12/11/2003	effective basin	2	0.2	535.0										
20	BCe	40.0	5.7	1.3	12/11/2003	effective basin	2	-1.6	155.0										
19	BMA	7	1	0	12/11/2003	effective basin	1	4.8	248.0										
20	BTppK	80	11	3	12/11/2003	effective basin	2	-4.2	132.4										
21	BUppA	110.0	14.7	3.7	12/11/2003	effective basin	1	6.0	414.1										
21	BUppB	110.0	14.7	3.7	12/11/2003	effective basin	2	4.5	596.2										
21	BUppC	110.0	14.7	3.7	12/11/2003	effective basin	2	3.0	349.3										
21	BUppD	110.0	14.7	3.7	12/11/2003	effective basin	2	1.5	371.8										
21	BUppE	110.0	14.7	3.7	12/11/2003	effective basin	2	0.9	190.6										
21	BUppF	110.0	14.7	3.7	12/11/2003	effective basin	2	0.2	190.1										
21	BUppG	110.0	14.7	3.7	12/11/2003	effective basin	2	-0.4	181.5										
21	BUppH	110.0	14.7	3.7	12/11/2003	effective basin	2	-1.0	157.3										
20	BYppI	150	20	5	12/11/2003	effective basin	2	-3.3	960.4										
12	AG	130.0	18.6	4.3	12/12/2003	area 12 (south shoulder of EB lane)	1	7.3	448.0										
20	ATppC	6.0	0.9	0.2	12/12/2003	effective basin	2	4.7	280.5										
21	BCppA	25.0	3.6	0.8	12/12/2003	effective basin	1	7.1	372.8										
21	BCppB	25.0	3.6	0.8	12/12/2003	effective basin	1	5.6	190.7										
20	BMppD	6.0	0.9	0.2	12/12/2003	effective basin	2	4.8	10128.2										
20	BMppK	25.0	3.6	0.8	12/12/2003	effective basin	2	-0.7	202.6										
21	BUppI	120.0	16.0	4.0	12/12/2003	effective basin	2	-1.6	135.6										
20	BYppA	120.0	17.1	4.0	12/12/2003	effective basin	1	5.8	375.1										
20	BYppB	120.0	16.0	4.0	12/12/2003	effective basin	2	4.3	498.2										
20	BYppC	120.0	16.0	4.0	12/12/2003	effective basin	2	2.8	483.0										
20	BYppD	130	17	4	12/12/2003	effective basin	2	1.3	375.1										

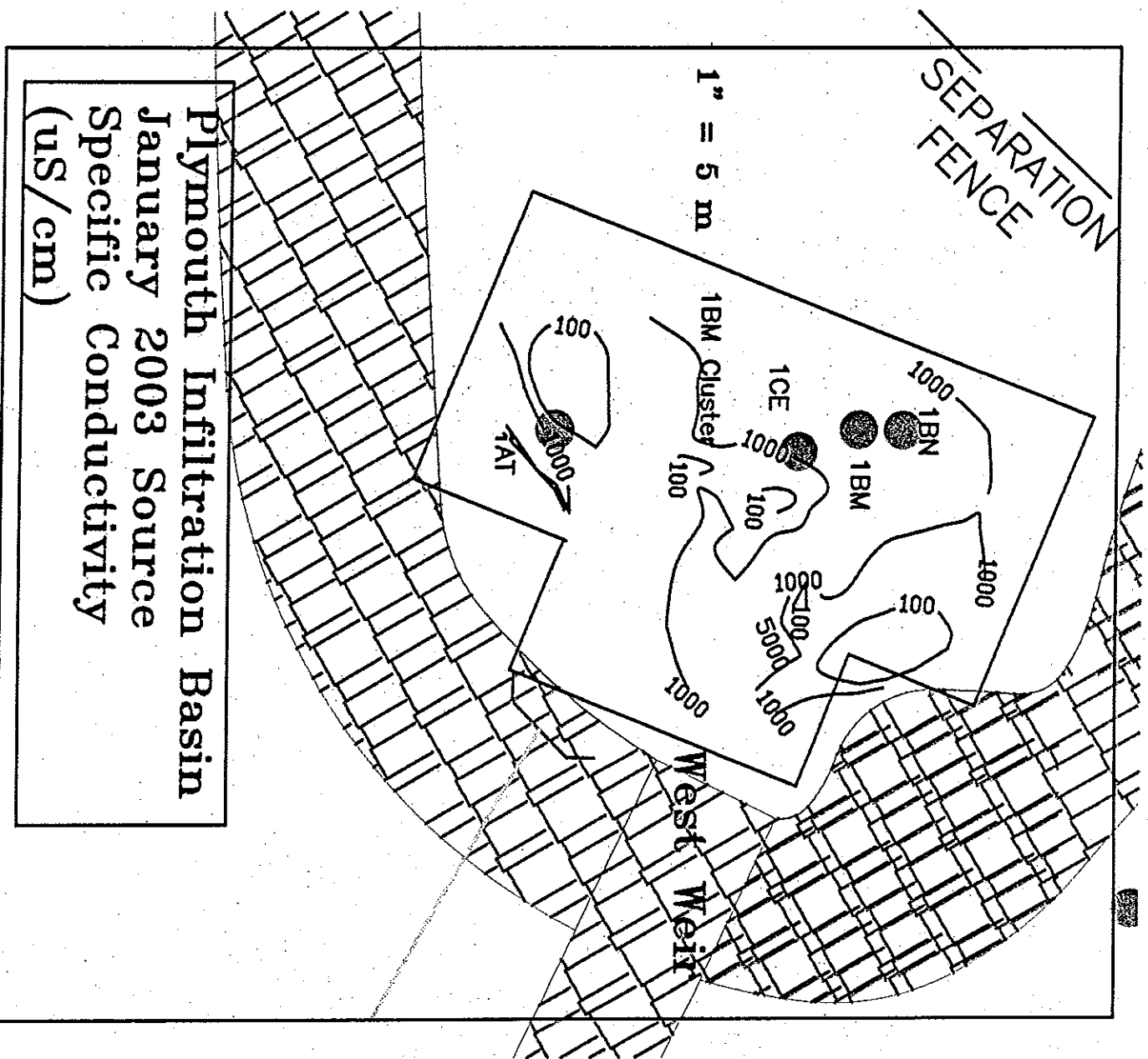
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20	BYpcpE	130	17	4	12/12/2003	effective basin	2	0.7	473.2										
20	BYpcpF	130	17	4	12/12/2003	effective basin	2	0.0	266.0										
20	BYpcpG	130	17	4	12/12/2003	effective basin	2	-0.6	89.7										
20	BYpcpH	130	17	4	12/12/2003	effective basin	2	-1.2	1107.0										
20	BYpcpI	140.0	18.7	4.7	12/12/2003	effective basin	2	-1.8	203.6										
20	ATpcpB	5.0	0.7	0.2	12/13/2003	effective basin	1	5.3	2167.0										
21	BCpcpH	50.0	7.1	1.7	12/13/2003	effective basin	2	-0.8	1105.0										
21	BCpcpI	50.0	7.1	1.7	12/13/2003	effective basin	2	-1.4	834.1										
21	BCpcpJ	50.0	7.1	1.7	12/13/2003	effective basin	2	-2.0	142.2										
20	BMpcpC	5.0	0.7	0.2	12/13/2003	effective basin	1	5.4	3376.1										
20	BTpcpA	50.0	7.1	1.7	12/13/2003	effective basin	1	6.5	178.4										
20	BTpcpB	50.0	7.1	1.7	12/13/2003	effective basin	2	-5.0	159.4										
21	BCpcpD	40.0	5.7	1.3	12/14/2003	effective basin	2	2.6	4085.9										
21	BCpcpE	40.0	5.7	1.3	12/14/2003	effective basin	2	1.0	1513.8										
21	BCpcpF	40.0	5.7	1.3	12/14/2003	effective basin	2	0.4	609.9										
21	BCpcpG	40.0	5.7	1.3	12/14/2003	effective basin	2	-0.2	1028.7										
9	AC	190.0	27.1	6.3	12/15/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.2	353.0										
20	ATpcpA	3.0	0.4	0.1	12/15/2003	effective basin	1	6.8	257.6										
20	BMpcpB	3.0	0.4	0.1	12/15/2003	effective basin	1	6.0	3291.7										
8	AB	35.0	5.0	1.2	12/16/2003	west of rest area, runoff slope	1	8.0	NS										
11	AK	240.0	34.3	8.0	12/16/2003	@ E BC, east of median I3 area	1	7.4	379.0										
14	AN	210.0	30.0	7.0	12/16/2003	area 12 (south shoulder of EB lane)	1	8.0	602.0										
20	AT	2	0	0	12/16/2003	effective basin	1	7.3	1005.0										
21	BE	35.0	5.0	1.2	12/16/2003	effective basin	2	-0.5	1398.0										
20	BTg	70.0	10.0	2.3	12/16/2003	effective basin	2	-0.1	597.0										
20	BTh	70.0	10.0	2.3	12/16/2003	effective basin	2	-1.0	180.0										
20	BTpcpJ	75	11	3	12/16/2003	effective basin	2	-2.6	270.9										
21	BUpcpA	110.0	14.7	3.7	12/16/2003	effective basin	1	6.0	104.5										
21	BUpcpB	110.0	14.7	3.7	12/16/2003	effective basin	2	4.5	5376.4										
21	BUpcpC	110.0	14.7	3.7	12/16/2003	effective basin	2	3.0	71.2										
21	BUpcpD	110.0	14.7	3.7	12/16/2003	effective basin	2	1.5	827.9										
21	BUpcpE	110.0	14.7	3.7	12/16/2003	effective basin	2	0.9	177.3										
21	BUpcpF	110.0	14.7	3.7	12/16/2003	effective basin	2	0.2	172.1										
21	BUpcpG	110.0	14.7	3.7	12/16/2003	effective basin	2	-0.4	148.3										
21	BUpcpH	110.0	14.7	3.7	12/16/2003	effective basin	2	-1.0	145.2										
19	CB	240.0	34.3	8.0	12/16/2003	N of WB lane, near 4 UG wells across rd	1	8.6	337.0										
7	AA	160.0	22.9	5.3	12/17/2003	rest area	1	8.4	NM										
22	AQ	330.0	47.1	11.0	12/17/2003	N of WB lane, near 4 UG wells across rd	1	8.2	NM										
20	BMpcpA	1.0	0.1	0.0	12/17/2003	effective basin	1	6.9	1519.2										
8	CA	160.0	22.9	5.3	12/17/2003	rest area, near E BC	1	6.1	415.7										
20	BTf	68.0	9.7	2.3	12/18/2003	effective basin	2	0.7	619.0										
20	BTpcpC	60.0	8.6	2.0	12/18/2003	effective basin	2	3.5	2417.6										
20	BTpcpK	80	11	3	12/18/2003	effective basin	2	-4.2	136.5										
20	BYpcpJ	150.0	20.0	5.0	12/18/2003	effective basin	2	-3.3	1740.9										
20	BMpcpJ	18.0	2.6	0.6	12/19/2003	effective basin	2	0.8	168.8										
21	BCpcpH	50.0	7.1	1.7	12/20/2003	effective basin	2	-0.8	260.1										
21	BCpcpI	50.0	7.1	1.7	12/20/2003	effective basin	2	-1.4	111.8										
21	BCpcpJ	50.0	7.1	1.7	12/20/2003	effective basin	2	-2.0	117.0										
20	BTpcpA	50.0	7.1	1.7	12/20/2003	effective basin	1	6.5	113.5										
20	BTpcpB	50.0	7.1	1.7	12/20/2003	effective basin	2	5.0	147.5										
18	AP	30.0	4.3	1.0	12/21/2003	effective basin	1	8.0	346.0										
20	BCi	30.0	4.3	1.0	12/21/2003	effective basin	2	1.1	1125.0										
22	BG	30.0	4.3	1.0	12/21/2003	effective basin	1	7.6	479.0										
21	BTa	65.0	9.3	2.2	12/21/2003	effective basin	1	5.4	471.0										
21	BTb	65.0	9.3	2.2	12/21/2003	effective basin	2	4.4	2207.0										
21	BTc	65.0	9.3	2.2	12/21/2003	effective basin	2	3.6	1872.0										
21	BTd	65.0	9.3	2.2	12/21/2003	effective basin	2	2.7	2614.0										
20	BTc	65.0	9.3	2.2	12/21/2003	effective basin	2	1.7	1090.0										
20	BTc	65.0	9.3	2.2	12/21/2003	effective basin	2	1.9	3041.5										
20	BTpcpD	70	10	2	12/21/2003	effective basin	2	1.3	2323.6										
20	BTpcpE	70	10	2	12/21/2003	effective basin	2	0.7	5778.9										
20	BTpcpF	70	10	2	12/21/2003	effective basin	2	0.1	663.9										
20	BTpcpG	70	10	2	12/21/2003	effective basin	2	-0.5	662.2										
20	BTpcpH	70	10	2	12/21/2003	effective basin	2	-1.1	331.1										
20	BYpcpI	140	19	5	12/21/2003	effective basin	2	-1.8	850.0										
14	AF	120.0	17.1	4.0	12/22/2003	area 12 (south shoulder of EB lane)	1	7.3	1596.0										
20	BMpcpI	15.0	2.1	0.5	12/22/2003	effective basin	2	1.7	506.4										
21	BUpcpA	110.0	14.7	3.7	12/22/2003	effective basin	1	6.0	579.7										
21	BUpcpB	110.0	14.7	3.7	12/22/2003	effective basin	2	4.5	298.9										
21	BUpcpC	110.0	14.7	3.7	12/22/2003	effective basin	2	3.0	193.2										

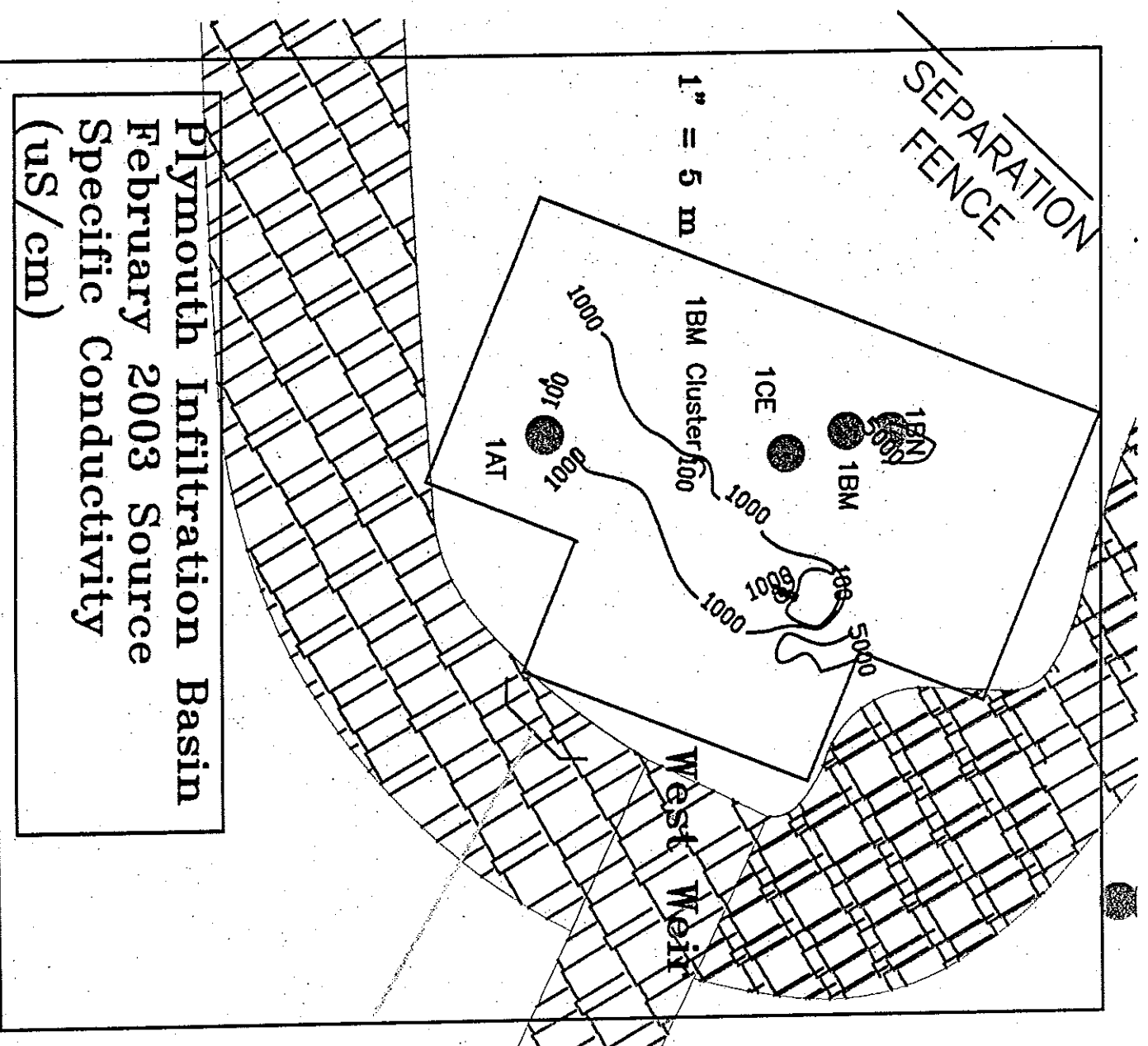
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21	BUcpD	110.0	14.7	3.7	12/22/2003	effective basin	2	1.5	196.3	21	BUcpD	110.0	14.7	3.7	12/22/2003	effective basin	2	1.5	196.3
21	BUcpE	110.0	14.7	3.7	12/22/2003	effective basin	2	0.9	194.2	21	BUcpE	110.0	14.7	3.7	12/22/2003	effective basin	2	0.9	194.2
21	BUcpF	110.0	14.7	3.7	12/22/2003	effective basin	2	0.2	177.3	21	BUcpF	110.0	14.7	3.7	12/22/2003	effective basin	2	0.2	177.3
21	BUcpG	110.0	14.7	3.7	12/22/2003	effective basin	2	-0.4	187.0	21	BUcpG	110.0	14.7	3.7	12/22/2003	effective basin	2	-0.4	187.0
21	BUcpH	110.0	14.7	3.7	12/22/2003	effective basin	2	-1.0	156.8	21	BUcpH	110.0	14.7	3.7	12/22/2003	effective basin	2	-1.0	156.8
21	BUcpI	120	16	4	12/22/2003	effective basin	2	-1.6	279.6	21	BUcpI	120	16	4	12/22/2003	effective basin	2	-1.6	279.6
20	BYcpA	120	17	4	12/22/2003	effective basin	1	5.8	735.0	20	BYcpA	120	17	4	12/22/2003	effective basin	1	5.8	735.0
20	BYcpB	120	16	4	12/22/2003	effective basin	2	4.3	2107.9	20	BYcpB	120	16	4	12/22/2003	effective basin	2	4.3	2107.9
20	BYcpC	120	16	4	12/22/2003	effective basin	2	2.8	409.2	20	BYcpC	120	16	4	12/22/2003	effective basin	2	2.8	409.2
20	BYcpD	130.0	17.3	4.3	12/22/2003	effective basin	2	1.3	375.1	20	BYcpD	130.0	17.3	4.3	12/22/2003	effective basin	2	1.3	375.1
20	BYcpE	130.0	17.3	4.3	12/22/2003	effective basin	2	0.7	473.2	20	BYcpE	130.0	17.3	4.3	12/22/2003	effective basin	2	0.7	473.2
20	BYcpF	130.0	17.3	4.3	12/22/2003	effective basin	2	0.0	266.0	20	BYcpF	130.0	17.3	4.3	12/22/2003	effective basin	2	0.0	266.0
20	BYcpG	130.0	17.3	4.3	12/22/2003	effective basin	2	-0.6	59.7	20	BYcpG	130.0	17.3	4.3	12/22/2003	effective basin	2	-0.6	59.7
20	BYcpH	130.0	17.3	4.3	12/22/2003	effective basin	2	-1.2	1107.0	20	BYcpH	130.0	17.3	4.3	12/22/2003	effective basin	2	-1.2	1107.0
21	BZ	120.0	17.1	4.0	12/22/2003	effective basin	1	6.7	471.0	21	BZ	120.0	17.1	4.0	12/22/2003	effective basin	1	6.7	471.0
21	BCcpD	40.0	5.7	1.3	12/23/2003	effective basin	2	2.6	3502.2	21	BCcpD	40.0	5.7	1.3	12/23/2003	effective basin	2	2.6	3502.2
21	BCcpE	40.0	5.7	1.3	12/23/2003	effective basin	2	1.0	2532.7	21	BCcpE	40.0	5.7	1.3	12/23/2003	effective basin	2	1.0	2532.7
21	BCcpF	40.0	5.7	1.3	12/23/2003	effective basin	2	0.4	1516.8	21	BCcpF	40.0	5.7	1.3	12/23/2003	effective basin	2	0.4	1516.8
21	BCcpG	40.0	5.7	1.3	12/23/2003	effective basin	2	-0.2	1210.2	21	BCcpG	40.0	5.7	1.3	12/23/2003	effective basin	2	-0.2	1210.2
20	BTcpJ	75	11	3	12/23/2003	effective basin	2	-2.6	254.8	20	BTcpJ	75	11	3	12/23/2003	effective basin	2	-2.6	254.8
20	BTcpK	80.0	11.4	2.7	12/23/2003	effective basin	2	-4.2	119.2	20	BTcpK	80.0	11.4	2.7	12/23/2003	effective basin	2	-4.2	119.2
21	BCcpC	30.0	4.3	1.0	12/24/2003	effective basin	2	4.1	2678.3	21	BCcpC	30.0	4.3	1.0	12/24/2003	effective basin	2	4.1	2678.3
20	BMcpH	13.0	1.9	0.4	12/24/2003	effective basin	2	2.3	590.8	20	BMcpH	13.0	1.9	0.4	12/24/2003	effective basin	2	2.3	590.8
10	AI	200.0	28.6	6.7	12/26/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	270.0	10	AI	200.0	28.6	6.7	12/26/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	270.0
20	BCg	25.0	3.6	0.8	12/26/2003	effective basin	2	2.9	2844.0	20	BCg	25.0	3.6	0.8	12/26/2003	effective basin	2	2.9	2844.0
20	BMcpG	11.0	1.6	0.4	12/26/2003	effective basin	2	2.9	506.4	20	BMcpG	11.0	1.6	0.4	12/26/2003	effective basin	2	2.9	506.4
9	AD	150.0	21.4	5.0	12/27/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	387.5	9	AD	150.0	21.4	5.0	12/27/2003	b/tw areas 6/16, N of ramp, S of shoulder	1	8.1	387.5
20	BYcpJ	150.0	20.0	5.0	12/27/2003	effective basin	2	-3.3	4406.8	20	BYcpJ	150.0	20.0	5.0	12/27/2003	effective basin	2	-3.3	4406.8
21	BCcpH	50.0	7.1	1.7	12/28/2003	effective basin	2	-0.8	3803.7	21	BCcpH	50.0	7.1	1.7	12/28/2003	effective basin	2	-0.8	3803.7
21	BCcpI	50.0	7.1	1.7	12/28/2003	effective basin	2	-1.4	5517.3	21	BCcpI	50.0	7.1	1.7	12/28/2003	effective basin	2	-1.4	5517.3
21	BCcpJ	50.0	7.1	1.7	12/28/2003	effective basin	2	-2.0	115.9	21	BCcpJ	50.0	7.1	1.7	12/28/2003	effective basin	2	-2.0	115.9
20	BMcpF	9.0	1.3	0.3	12/28/2003	effective basin	2	3.6	928.4	20	BMcpF	9.0	1.3	0.3	12/28/2003	effective basin	2	3.6	928.4
20	BTcpA	50.0	7.1	1.7	12/28/2003	effective basin	1	6.5	63.2	20	BTcpA	50.0	7.1	1.7	12/28/2003	effective basin	1	6.5	63.2
20	BTcpB	50.0	7.1	1.7	12/28/2003	effective basin	2	5.0	150.8	20	BTcpB	50.0	7.1	1.7	12/28/2003	effective basin	2	5.0	150.8
20	BTcpD	70	10	2	12/28/2003	effective basin	2	1.9	633.7	20	BTcpD	70	10	2	12/28/2003	effective basin	2	1.9	633.7
20	BTcpE	70	10	2	12/28/2003	effective basin	2	1.3	1240.5	20	BTcpE	70	10	2	12/28/2003	effective basin	2	1.3	1240.5
20	BTcpF	70	10	2	12/28/2003	effective basin	2	0.7	758.4	20	BTcpF	70	10	2	12/28/2003	effective basin	2	0.7	758.4
20	BTcpG	70	10	2	12/28/2003	effective basin	2	0.1	484.1	20	BTcpG	70	10	2	12/28/2003	effective basin	2	0.1	484.1
20	BTcpH	70	10	2	12/28/2003	effective basin	2	-0.5	260.2	20	BTcpH	70	10	2	12/28/2003	effective basin	2	-0.5	260.2
20	BTcpI	70	10	2	12/28/2003	effective basin	2	-1.1	284.4	20	BTcpI	70	10	2	12/28/2003	effective basin	2	-1.1	284.4
20	BTcpJ	75.0	10.7	2.5	12/28/2003	effective basin	2	-2.6	212.9	20	BTcpJ	75.0	10.7	2.5	12/28/2003	effective basin	2	-2.6	212.9
20	BYcpI	140.0	18.7	4.7	12/28/2003	effective basin	2	-1.8	484.5	20	BYcpI	140.0	18.7	4.7	12/28/2003	effective basin	2	-1.8	484.5
21	BCcpA	25.0	3.6	0.8	12/29/2003	effective basin	1	7.1	466.4	21	BCcpA	25.0	3.6	0.8	12/29/2003	effective basin	1	7.1	466.4
21	BCcpB	25.0	3.6	0.8	12/29/2003	effective basin	1	5.6	4213.8	21	BCcpB	25.0	3.6	0.8	12/29/2003	effective basin	1	5.6	4213.8
20	BMcpE	8.0	1.1	0.3	12/29/2003	effective basin	2	4.2	13504.3	20	BMcpE	8.0	1.1	0.3	12/29/2003	effective basin	2	4.2	13504.3
20	BMcpK	25.0	3.6	0.8	12/29/2003	effective basin	2	-0.7	253.2	20	BMcpK	25.0	3.6	0.8	12/29/2003	effective basin	2	-0.7	253.2
21	BCcpD	40.0	5.7	1.3	12/30/2003	effective basin	2	2.6	3458.5	21	BCcpD	40.0	5.7	1.3	12/30/2003	effective basin	2	2.6	3458.5
21	BCcpE	40.0	5.7	1.3	12/30/2003	effective basin	2	1.0	864.6	21	BCcpE	40.0	5.7	1.3	12/30/2003	effective basin	2	1.0	864.6
21	BCcpF	40.0	5.7	1.3	12/30/2003	effective basin	2	0.4	331.1	21	BCcpF	40.0	5.7	1.3	12/30/2003	effective basin	2	0.4	331.1
21	BCcpO	40.0	5.7	1.3	12/30/2003	effective basin	2	-0.2	870.6	21	BCcpO	40.0	5.7	1.3	12/30/2003	effective basin	2	-0.2	870.6
13	AH	90.0	12.9	3.0	12/31/2003	area 12 (south shoulder of EB lane)	1	7.4	1526.0	13	AH	90.0	12.9	3.0	12/31/2003	area 12 (south shoulder of EB lane)	1	7.4	1526.0
20	ATcpC	6.0	0.9	0.2	12/31/2003	effective basin	2	4.7	213.7	20	ATcpC	6.0	0.9	0.2	12/31/2003	effective basin	2	4.7	213.7
19	BCe	20.0	2.9	0.7	12/31/2003	effective basin	1	6.0	2220.0	19	BCe	20.0	2.9	0.7	12/31/2003	effective basin	1	6.0	2220.0
19	BCb	20.0	2.9	0.7	12/31/2003	effective basin	2	3.6	2662.0	19	BCb	20.0	2.9	0.7	12/31/2003	effective basin	2	3.6	2662.0
20	BCe	20.0	2.9	0.7	12/31/2003	effective basin	2	2.0	2330.0	20	BCe	20.0	2.9	0.7	12/31/2003	effective basin	2	2.0	2330.0
21	BD	20.0	2.9	0.7	12/31/2003	effective basin	1	5.6	2406.0	21	BD	20.0	2.9	0.7	12/31/2003	effective basin	1	5.6	2406.0
20	BMcpD	6.0	0.9	0.2	12/31/2003	effective basin	2	4.8	17724.4	20	BMcpD	6.0	0.9	0.2	12/31/2003	effective basin	2	4.8	17724.4
20	BTJ	90.0	12.9	3.0	12/31/2003	effective basin	2	-3.7	372.0	20	BTJ	90.0	12.9	3.0	12/31/2003	effective basin	2	-3.7	372.0
20	BTcpC	60	9	2	12/31/2003	effective basin	2	3.5	2280.8	20	BTcpC	60	9	2	12/31/2003	effective basin	2	3.5	2280.8
20	BYcpD	130	17	4	12/31/2003	effective basin	2	1.3	379.6	20	BYcpD	130	17	4	12/31/2003	effective basin	2	1.3	379.6
20	BYcpE	130	17	4	12/31/2003	effective basin	2	0.7	1107.5	20	BYcpE	130	17	4	12/31/2003	effective basin	2	0.7	1107.5
20	BYcpF	130	17	4	12/31/2003	effective basin	2	0.0	839.5	20	BYcpF	130	17	4	12/31/2003	effective basin	2	0.0	839.5
20	BYcpG	130	17	4	12/31/2003	effective basin	2	-0.6	46.1	20	BYcpG	130	17	4	12/31/2003	effective basin	2	-0.6	46.1
20	BYcpH	130	17	4	12/31/2003	effective basin	2	-1.2	676.0	20	BYcpH	130	17	4	12/31/2003	effective basin	2	-1.2	676.0

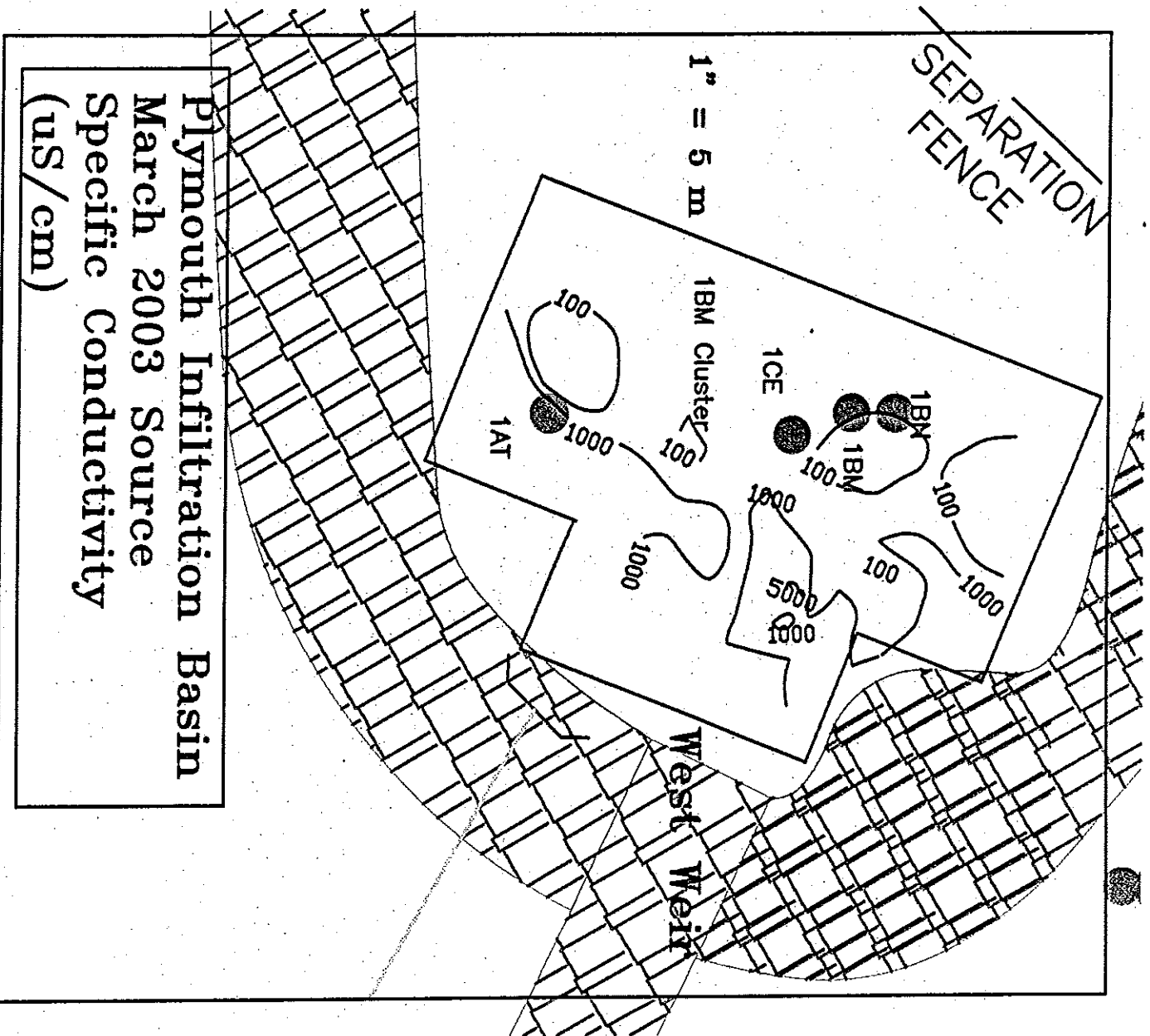
APPENDIX H
Specific Conductivity Source Isopleths, November 2002 – May 2004

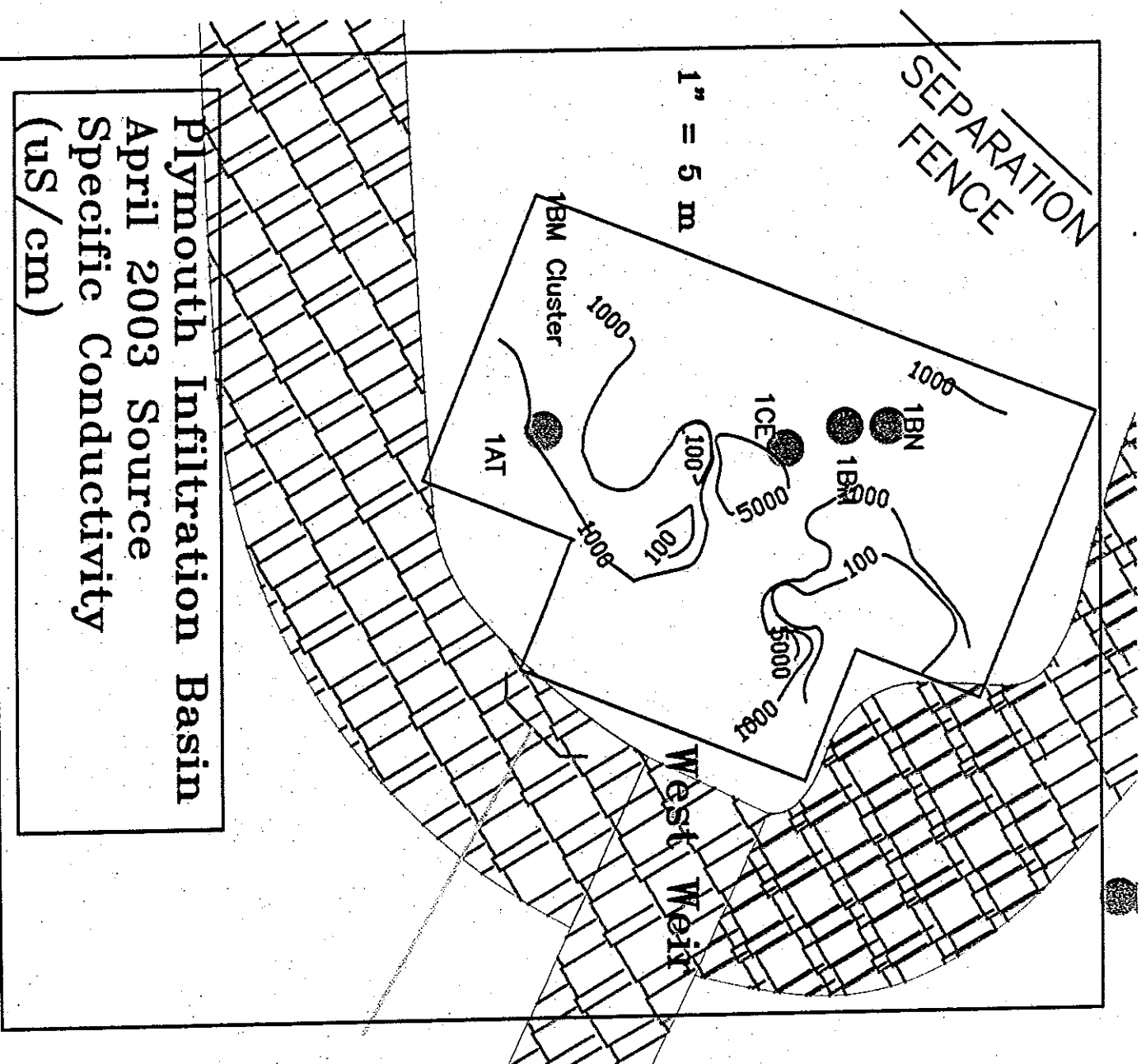


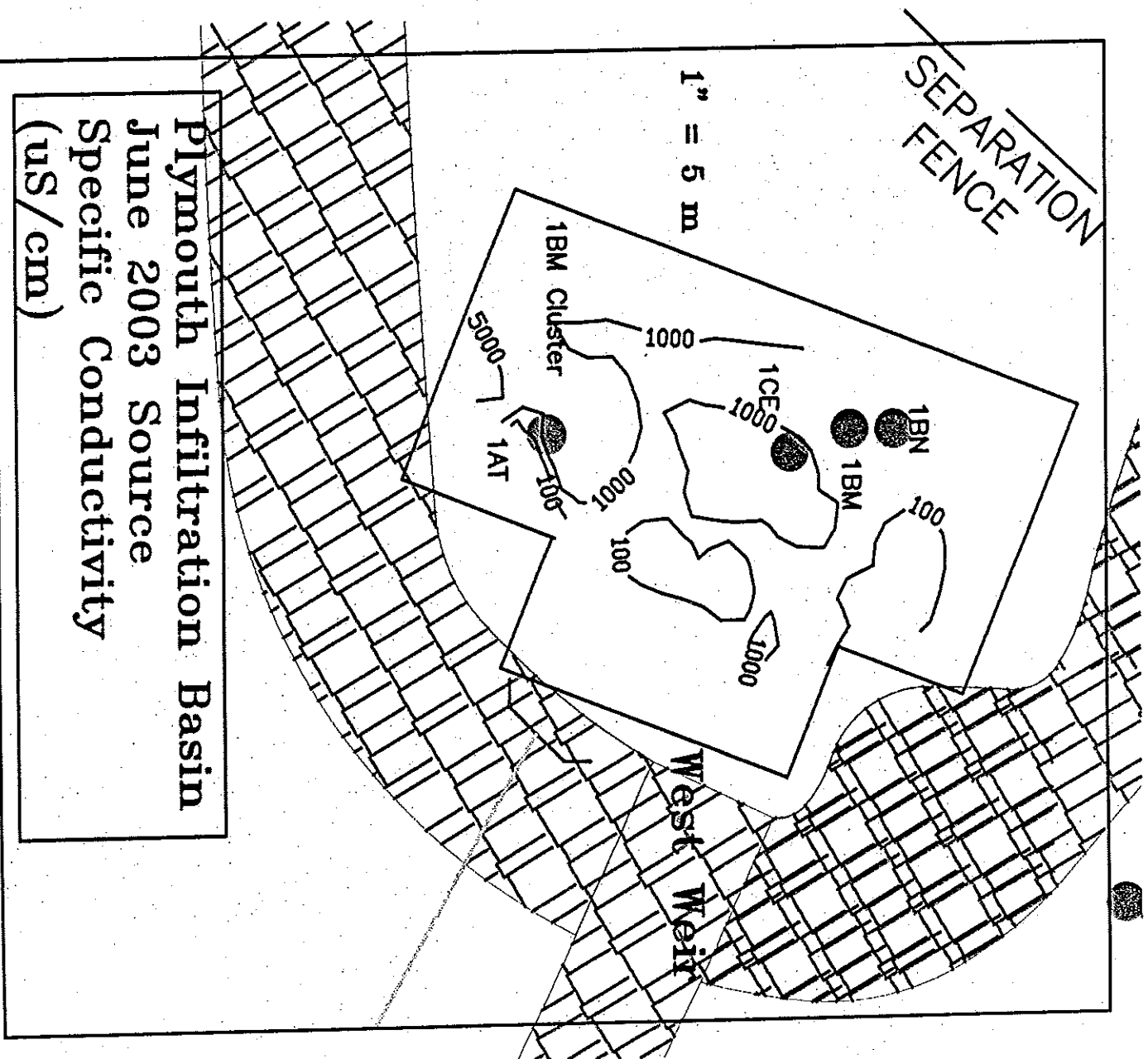


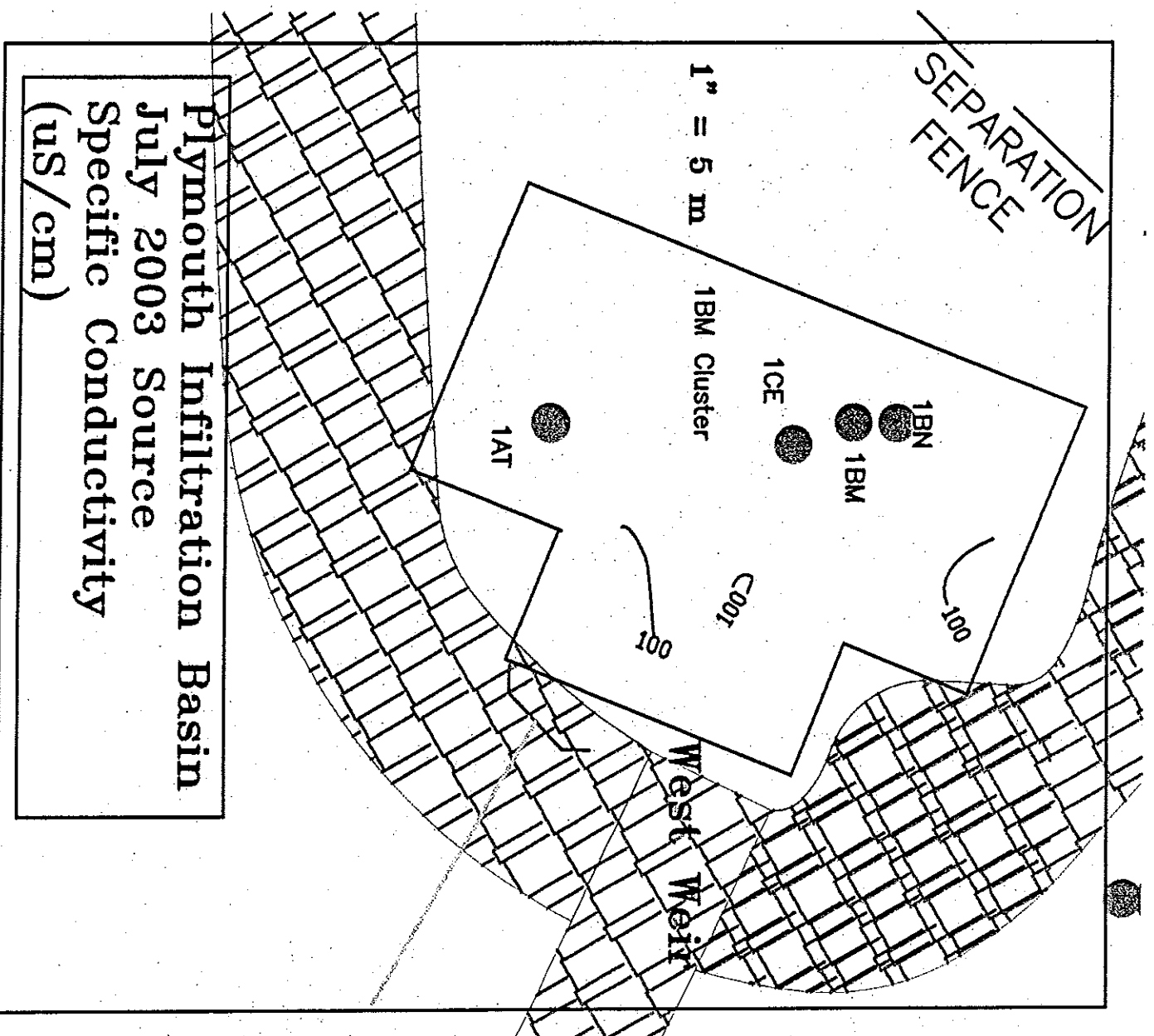


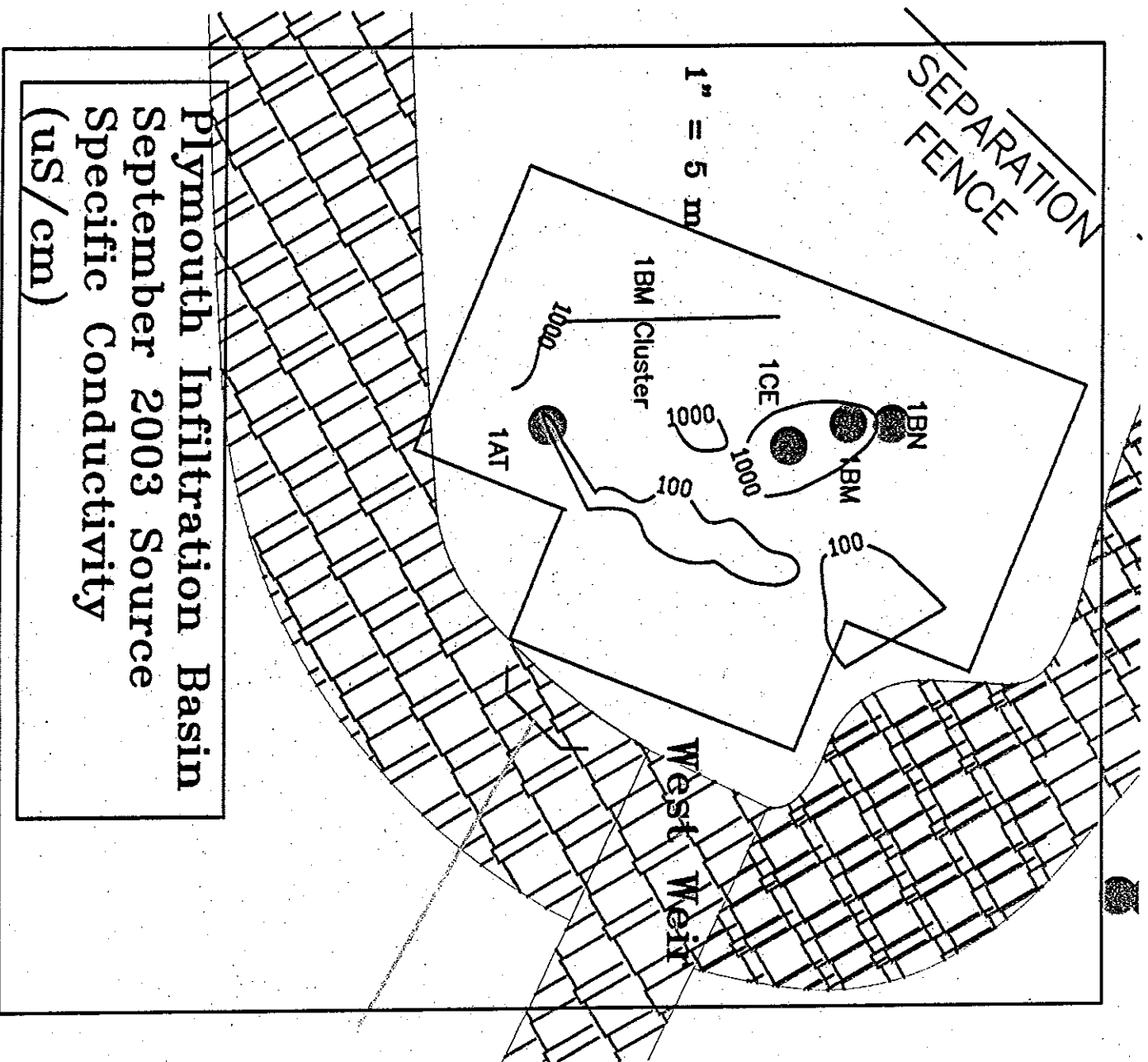


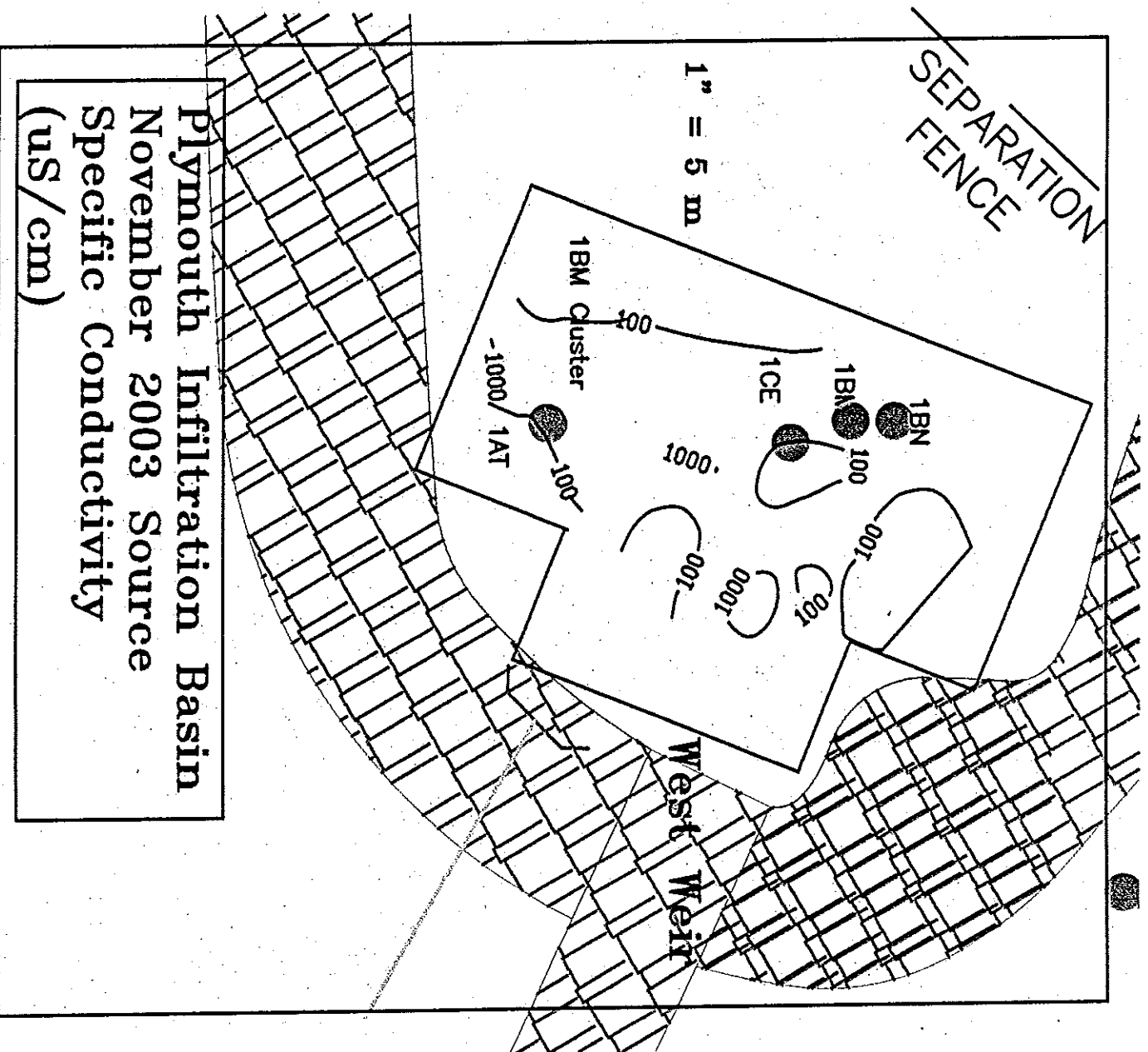


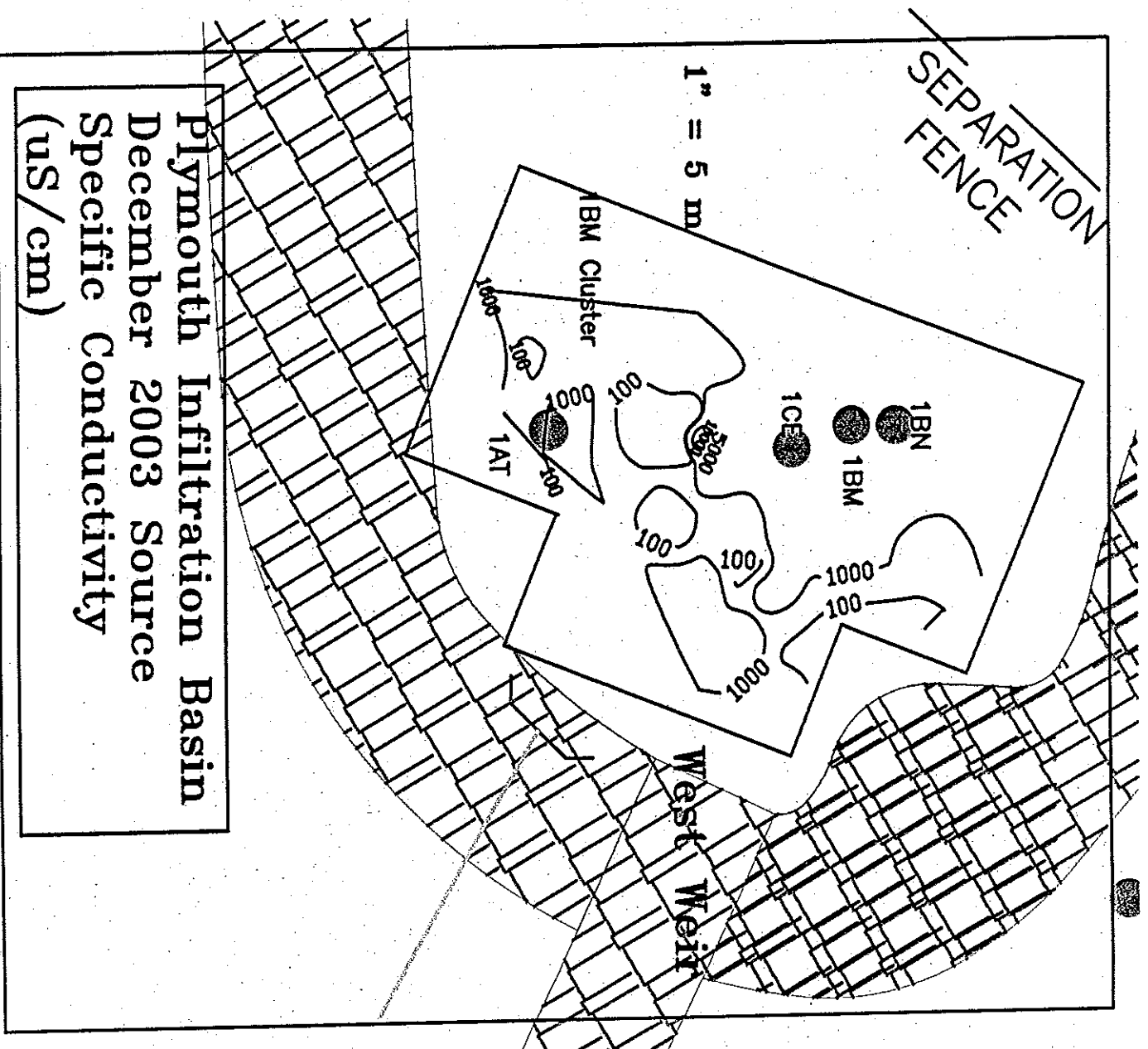


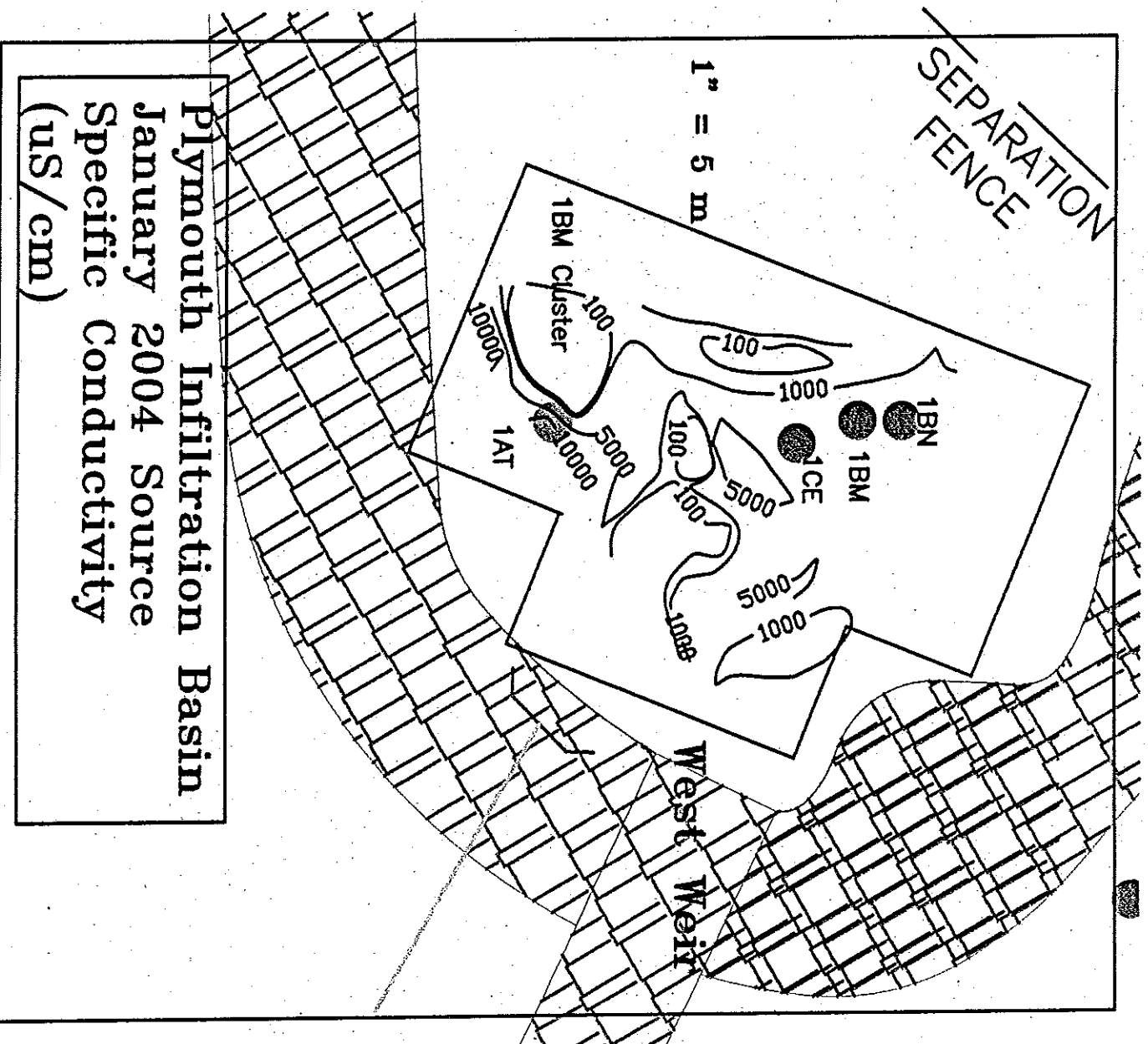


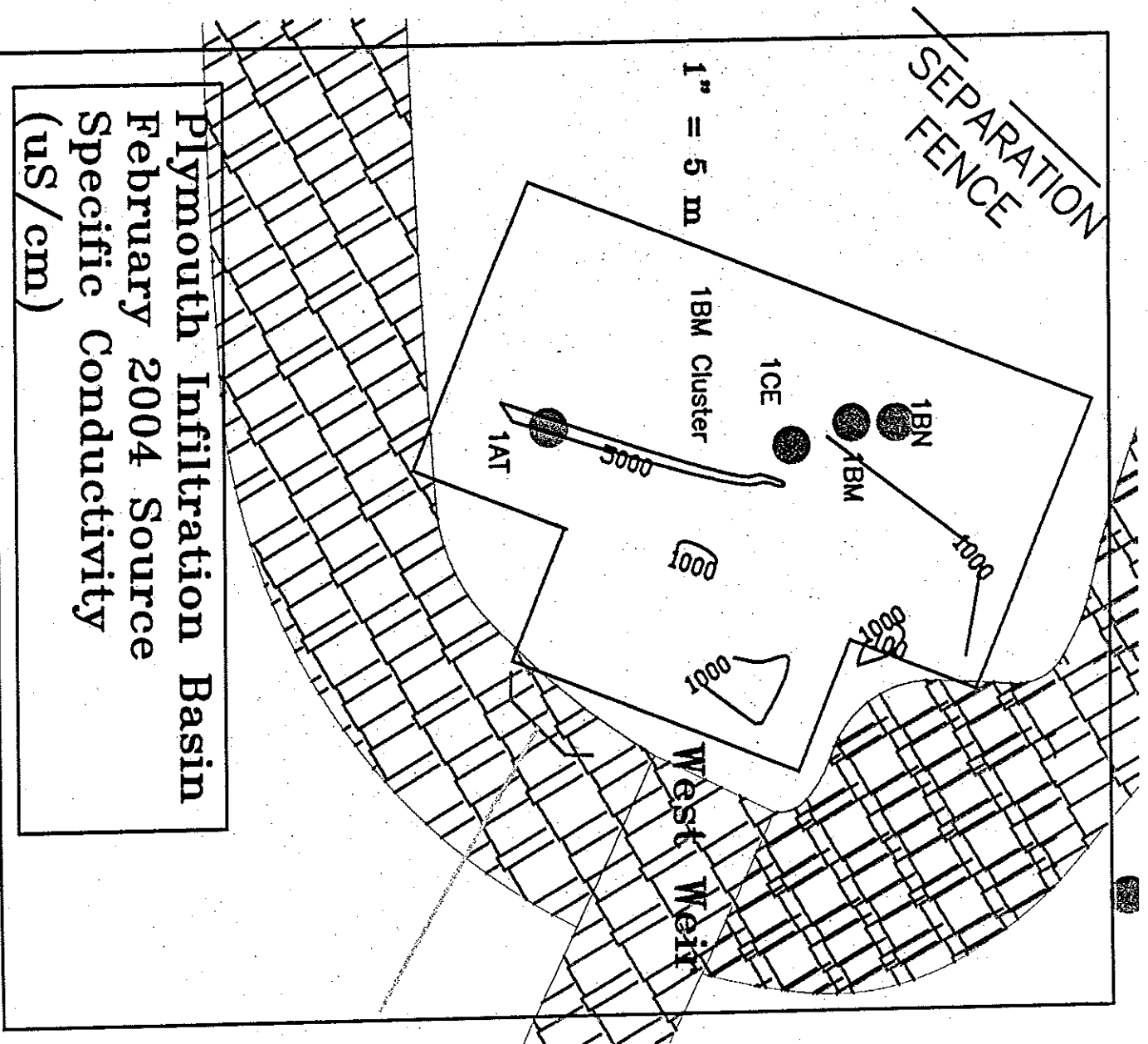


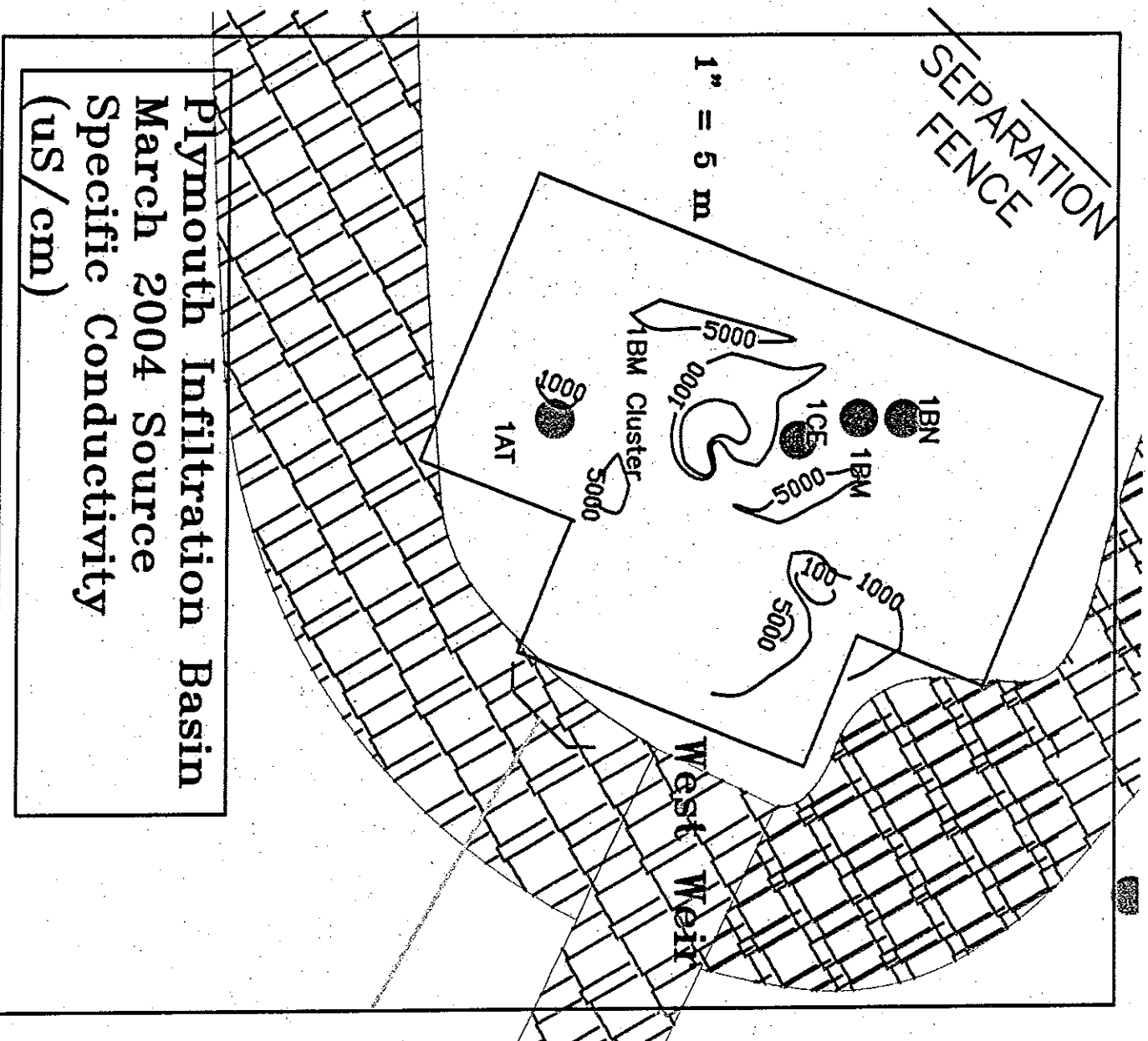


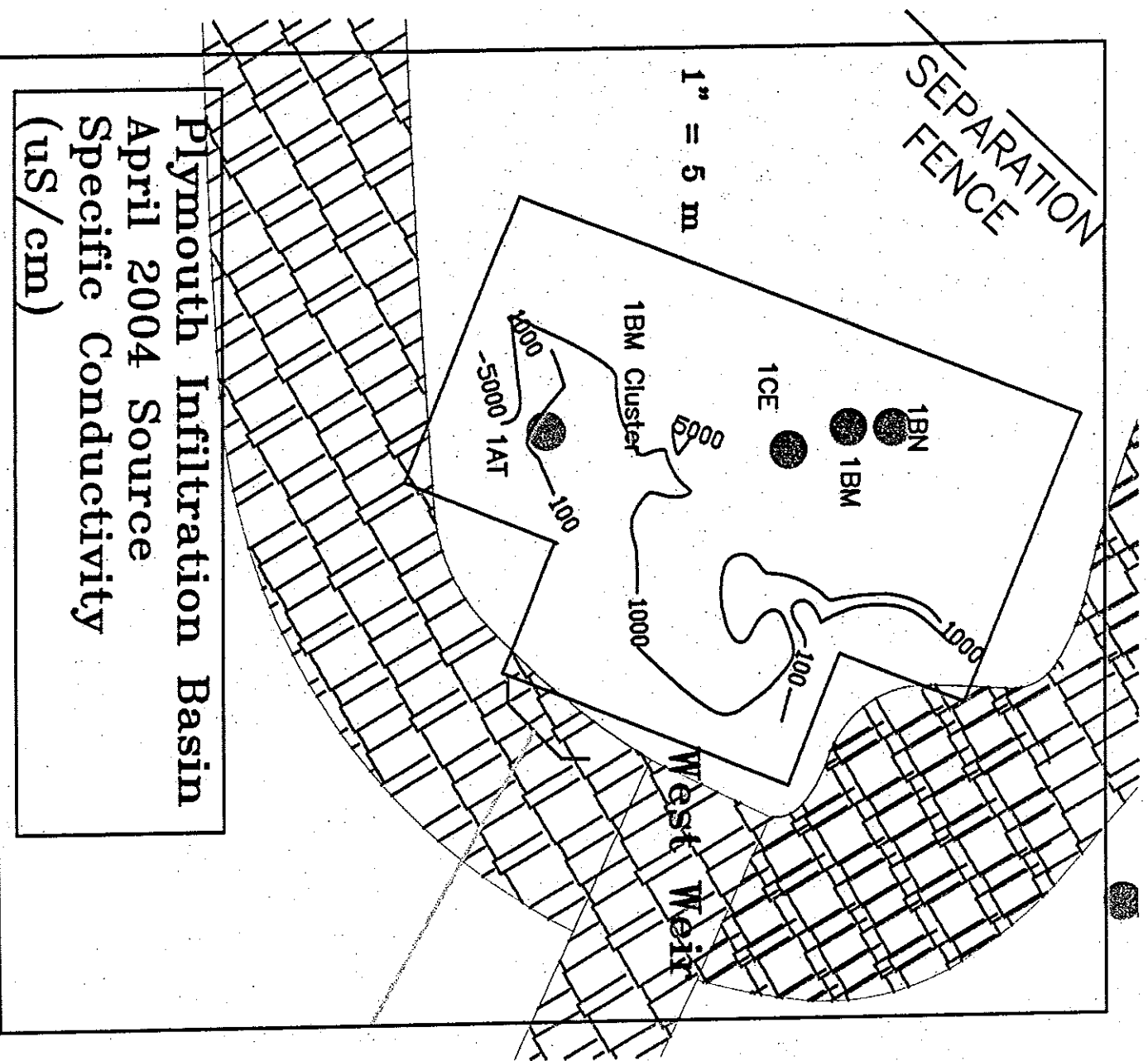


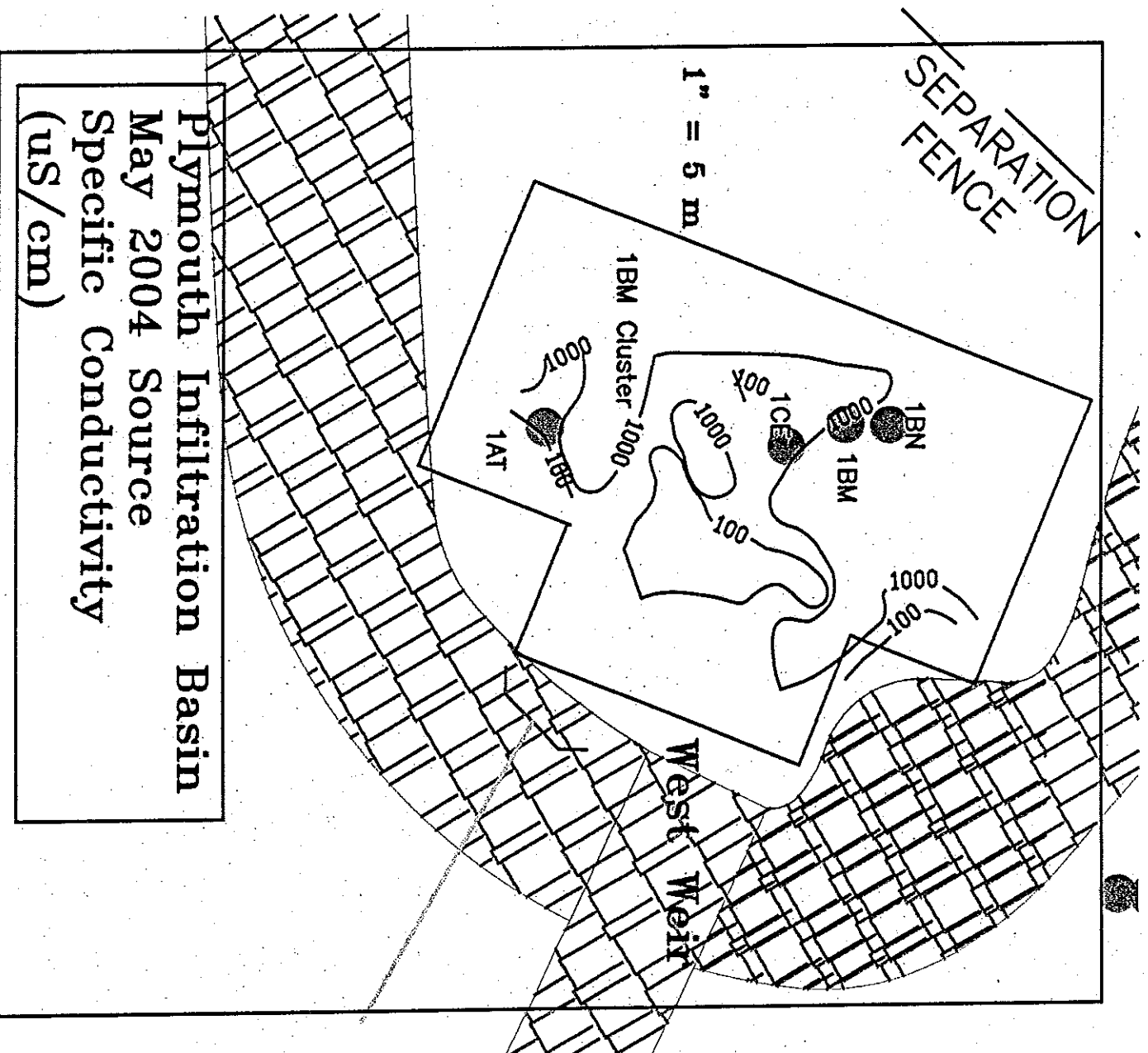




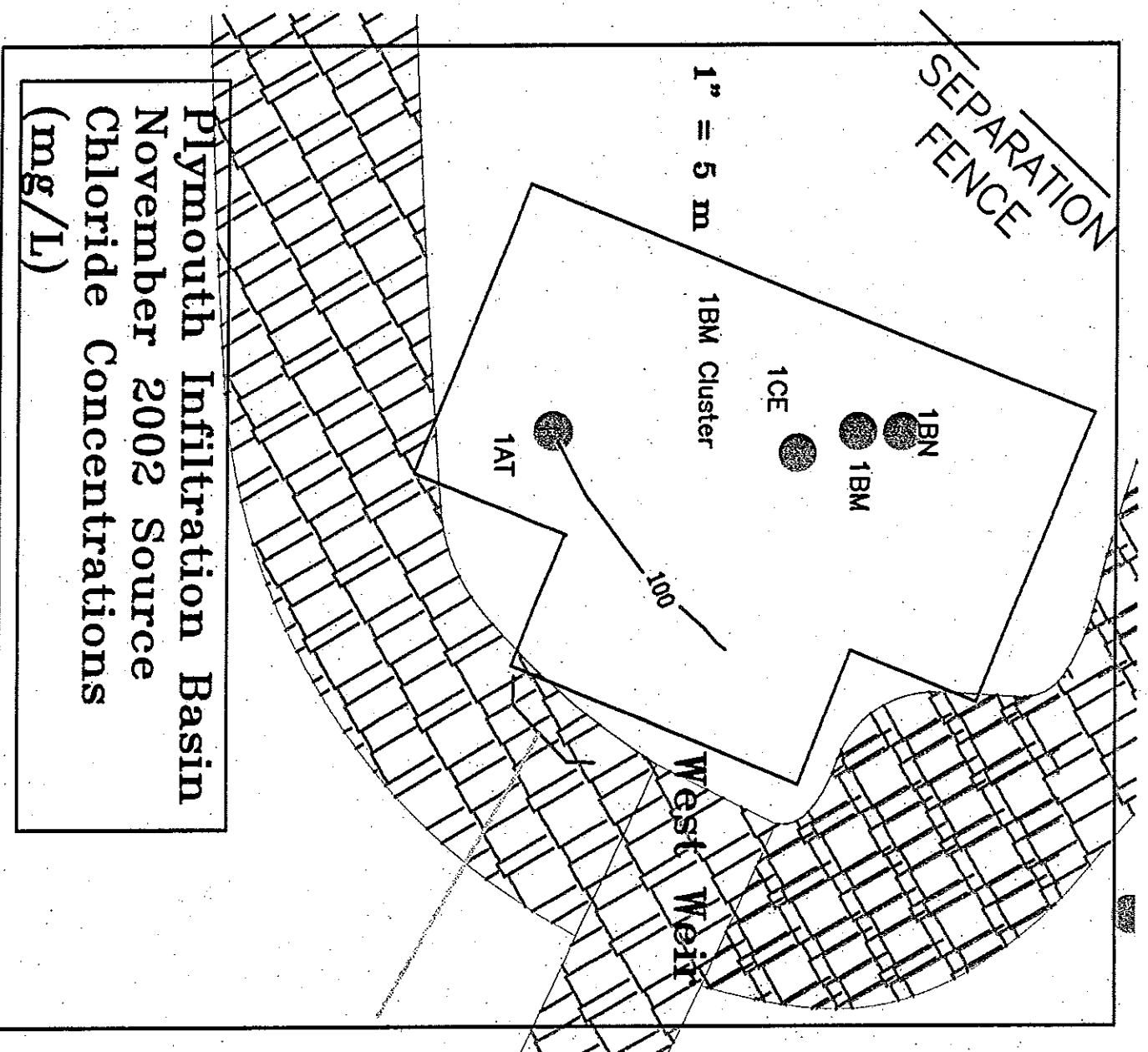




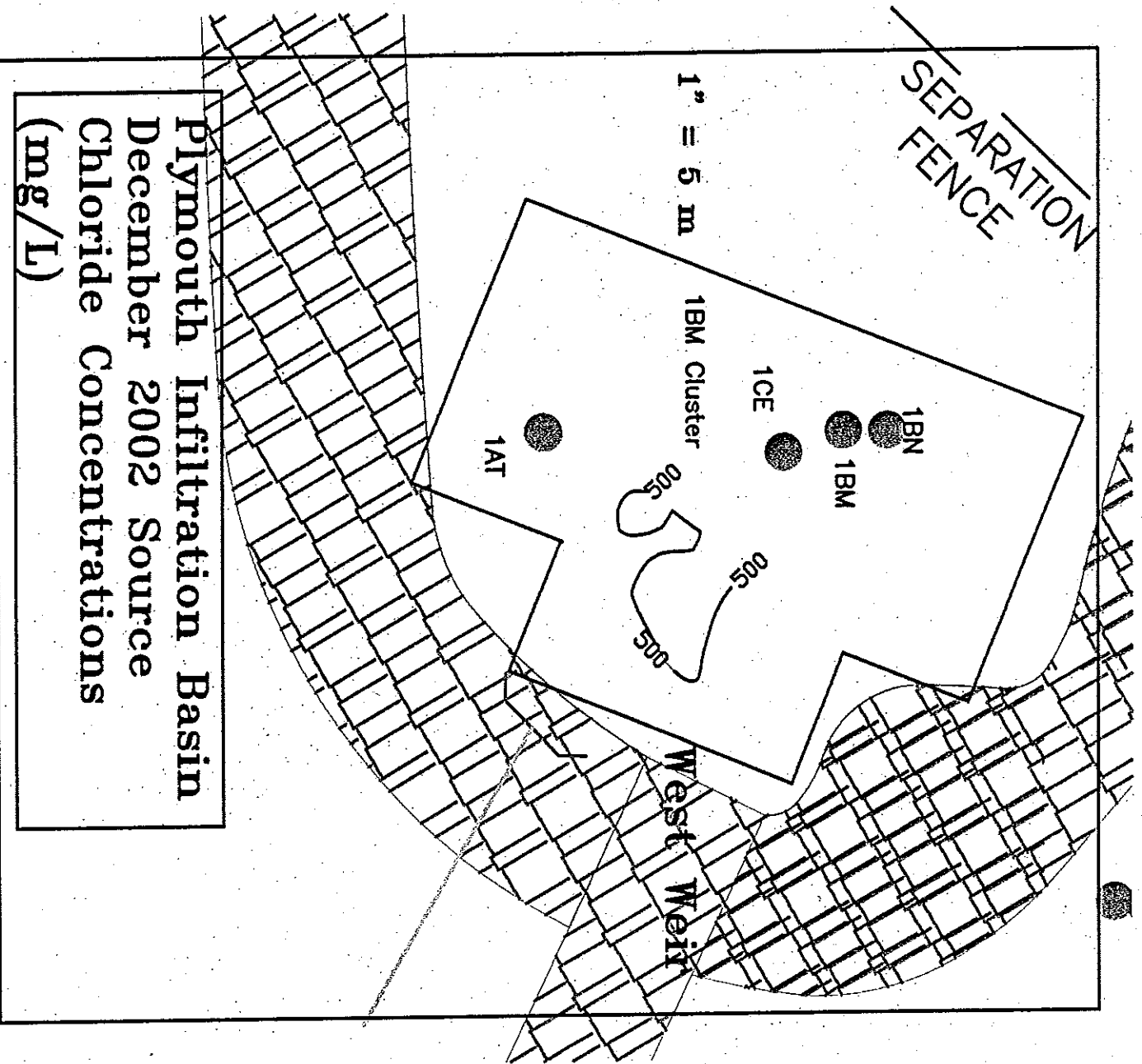




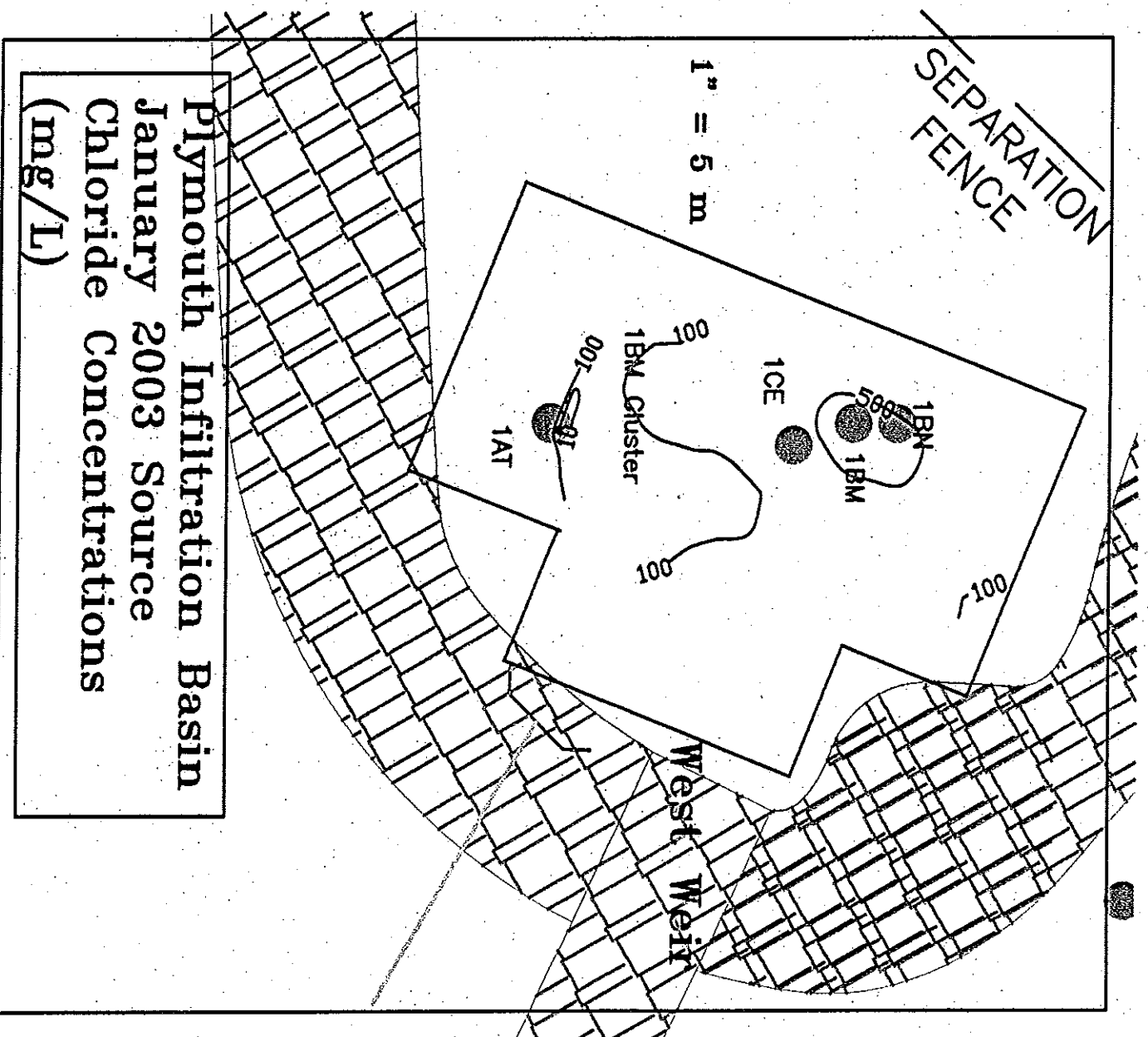
APPENDIX I
Chloride Source Isopleths, November 2002 – May 2004

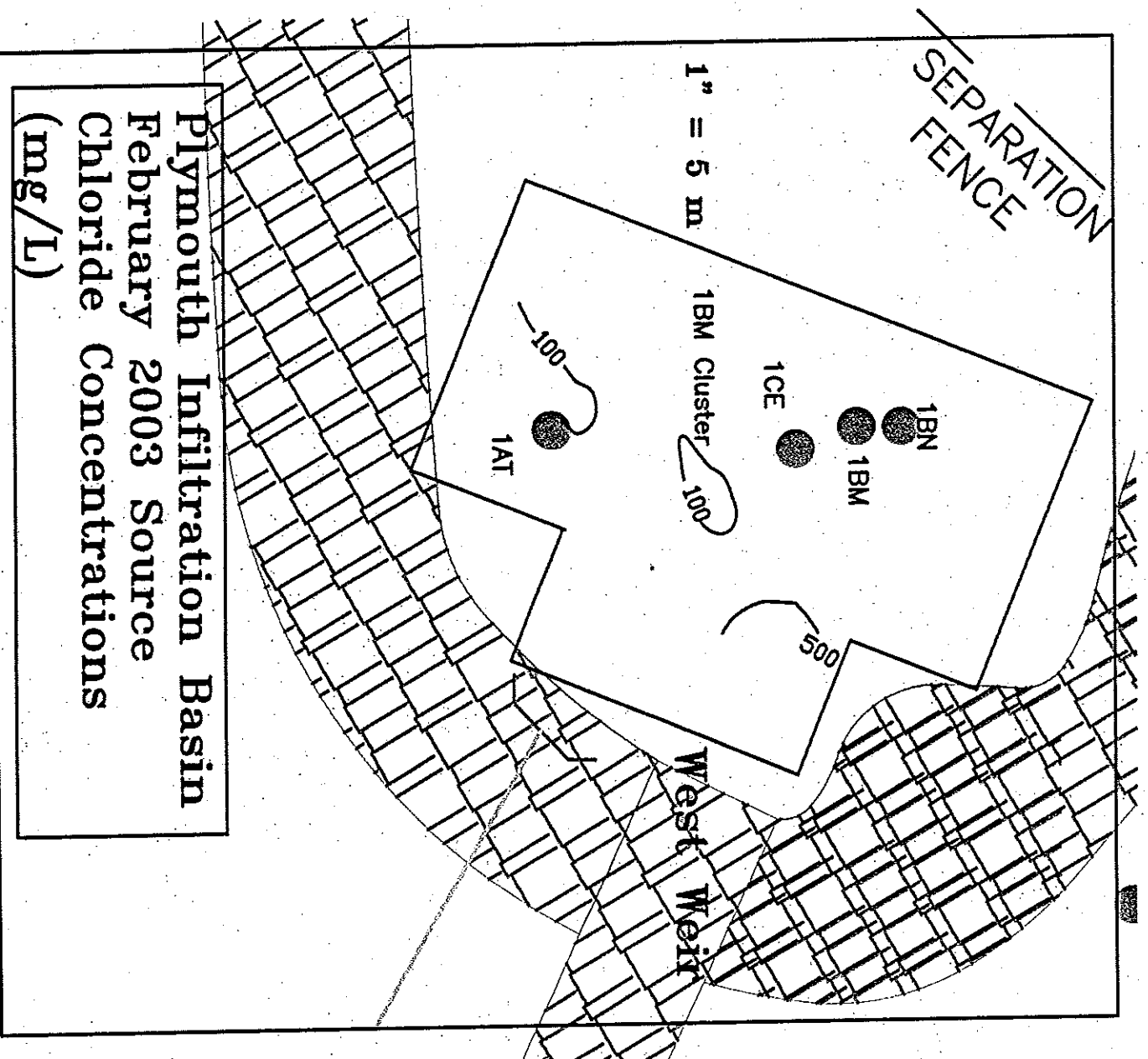


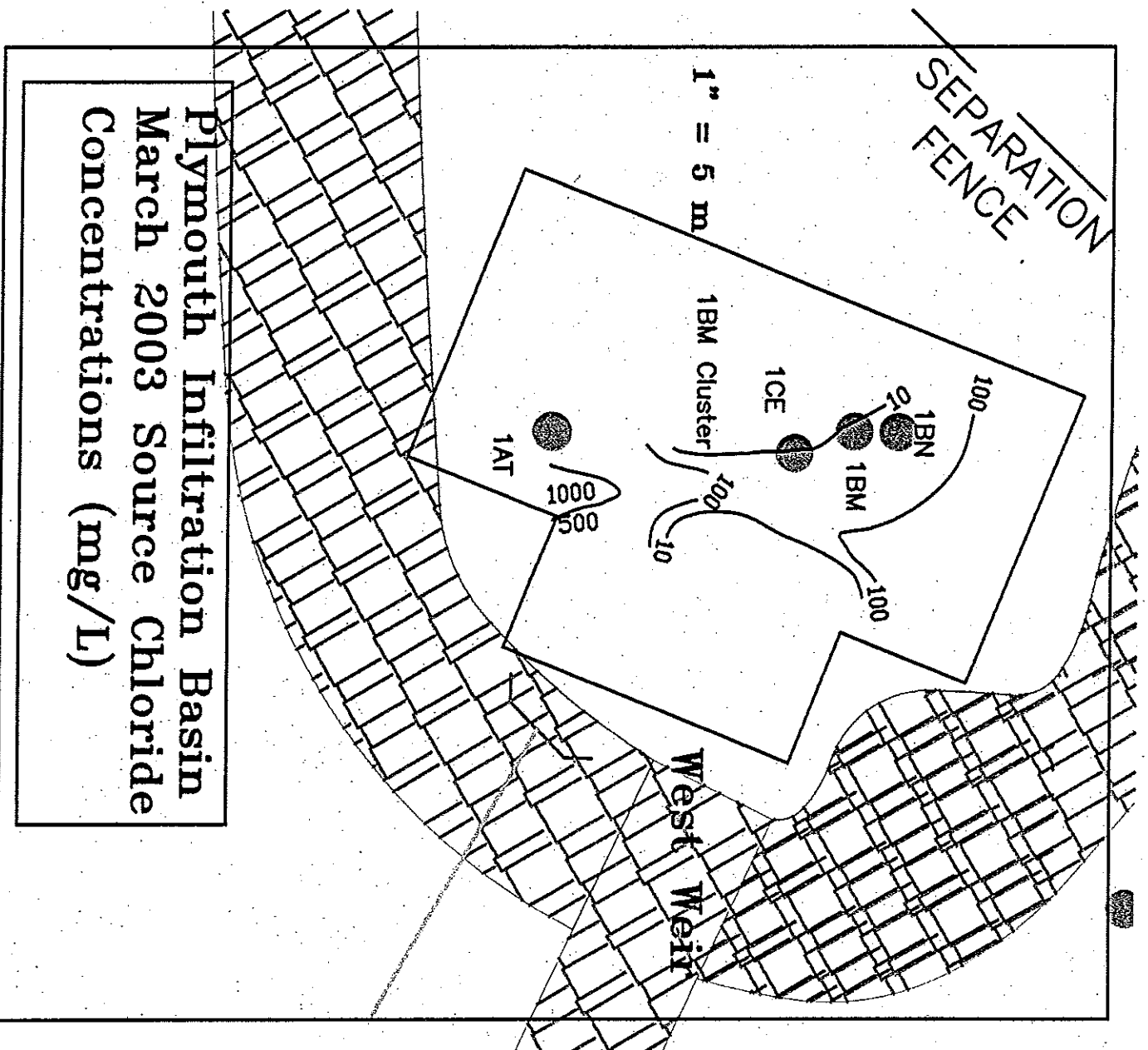
Plymouth Infiltration Basin
November 2002 Source
Chloride Concentrations
(mg/L)

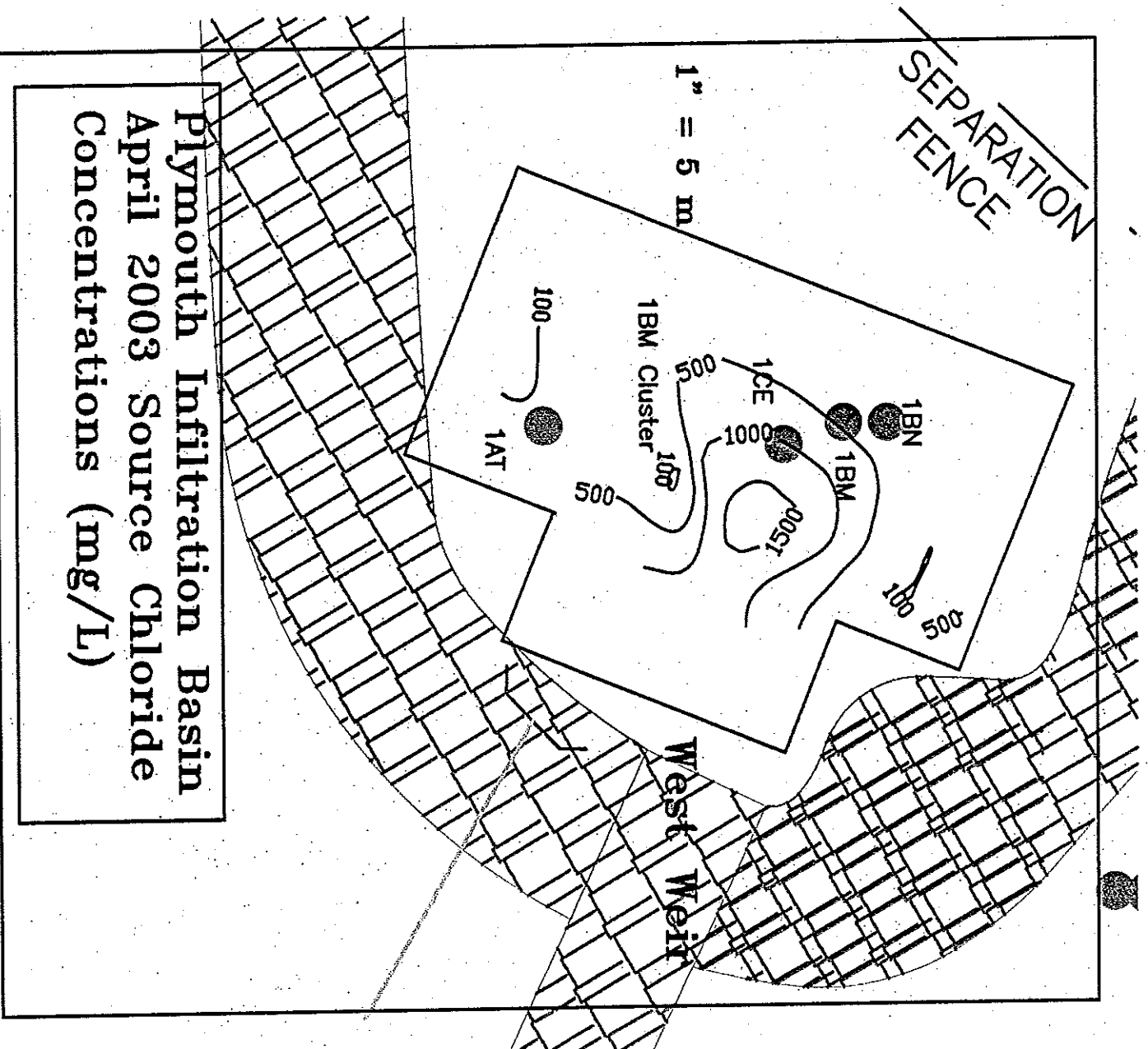


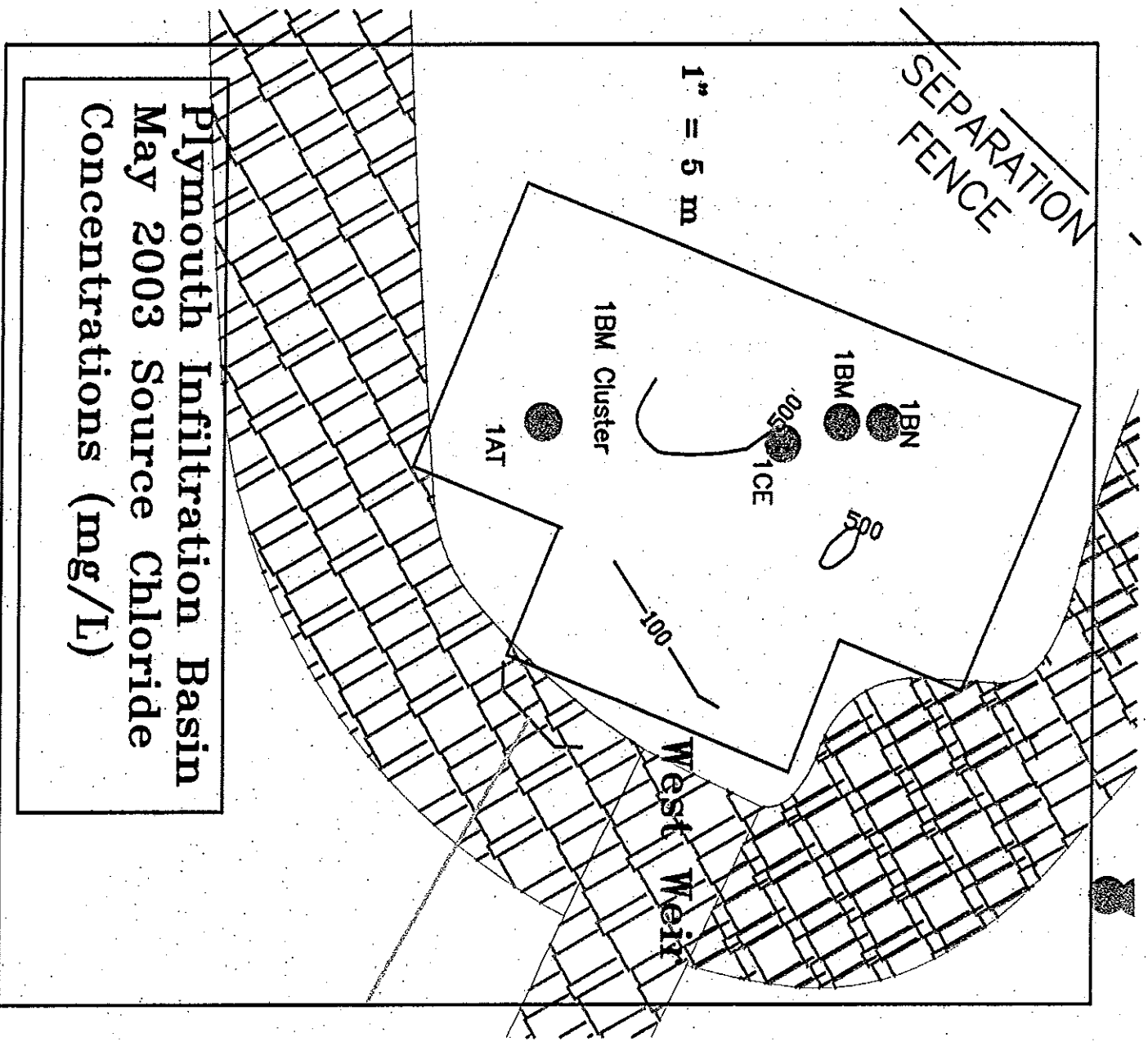
Plymouth Infiltration Basin
December 2002 Source
Chloride Concentrations
(mg/L)

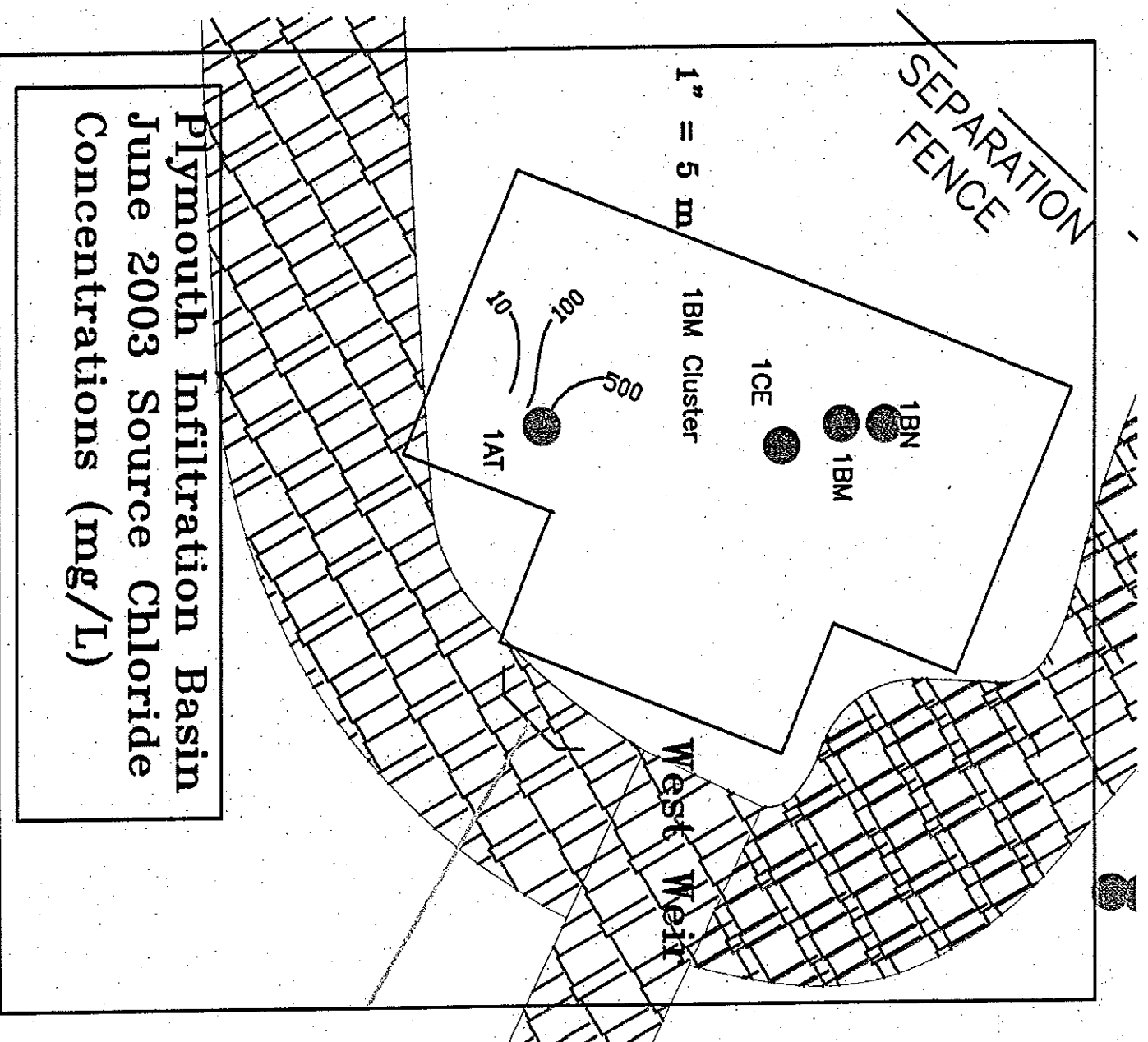


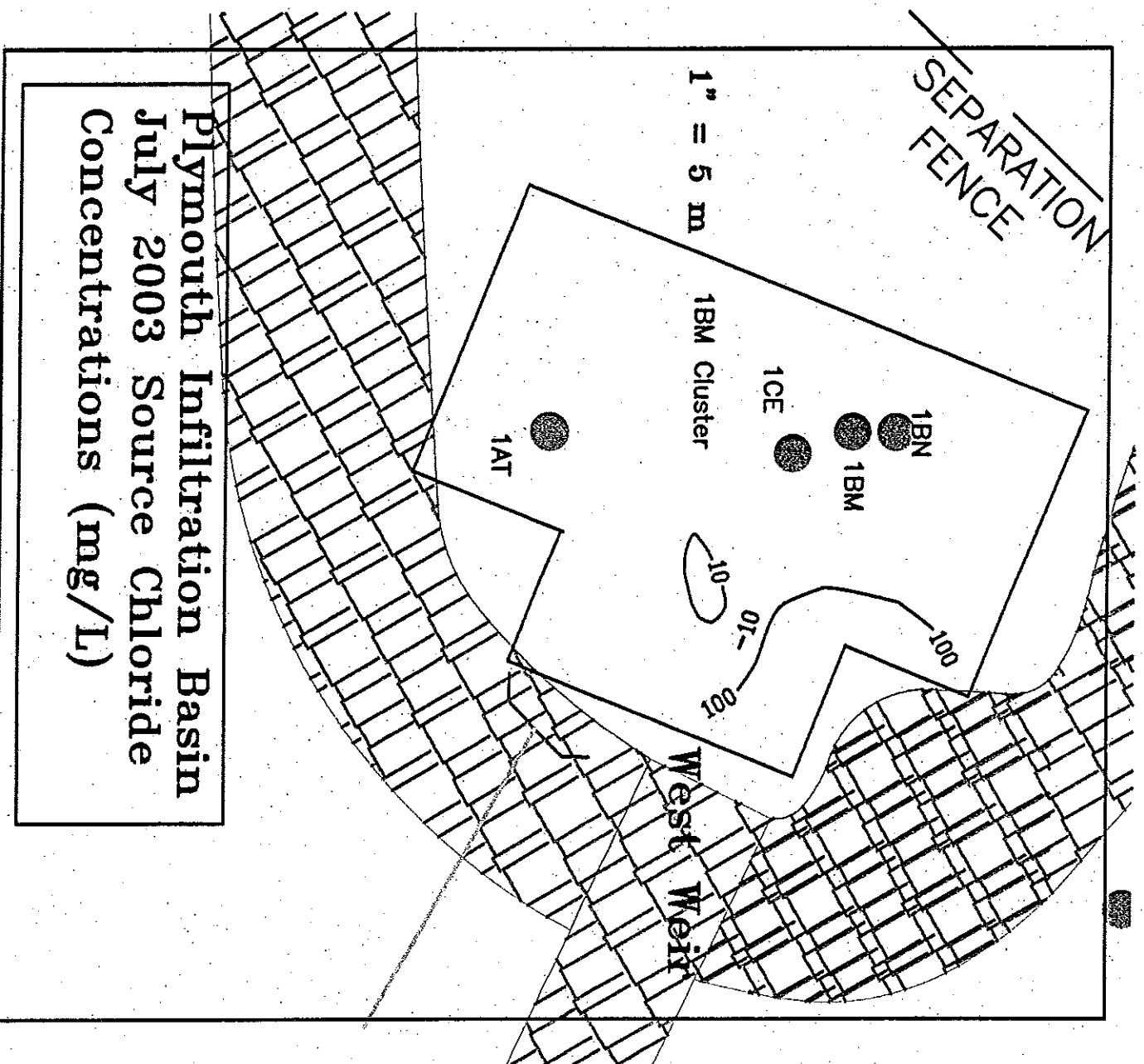


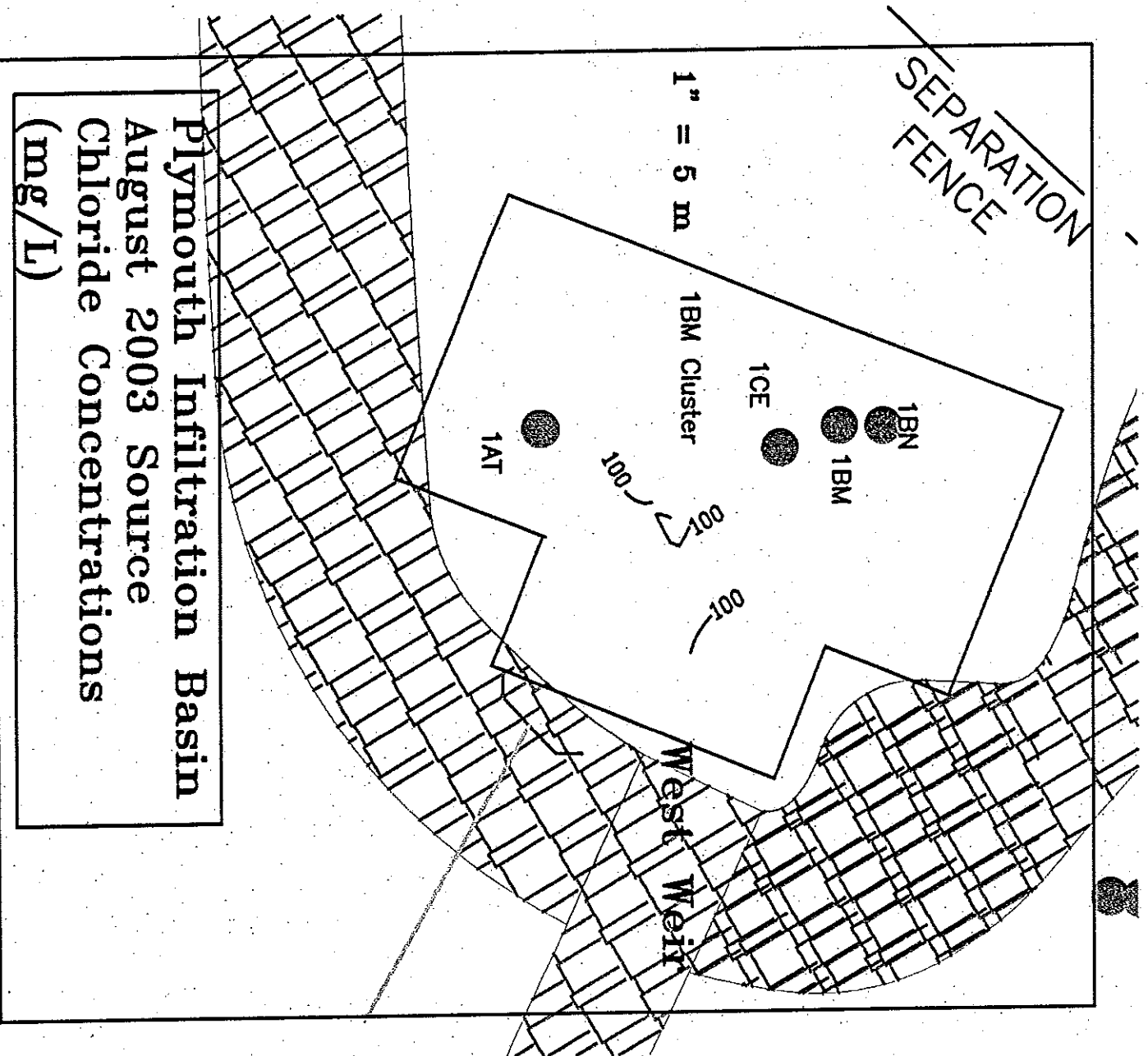


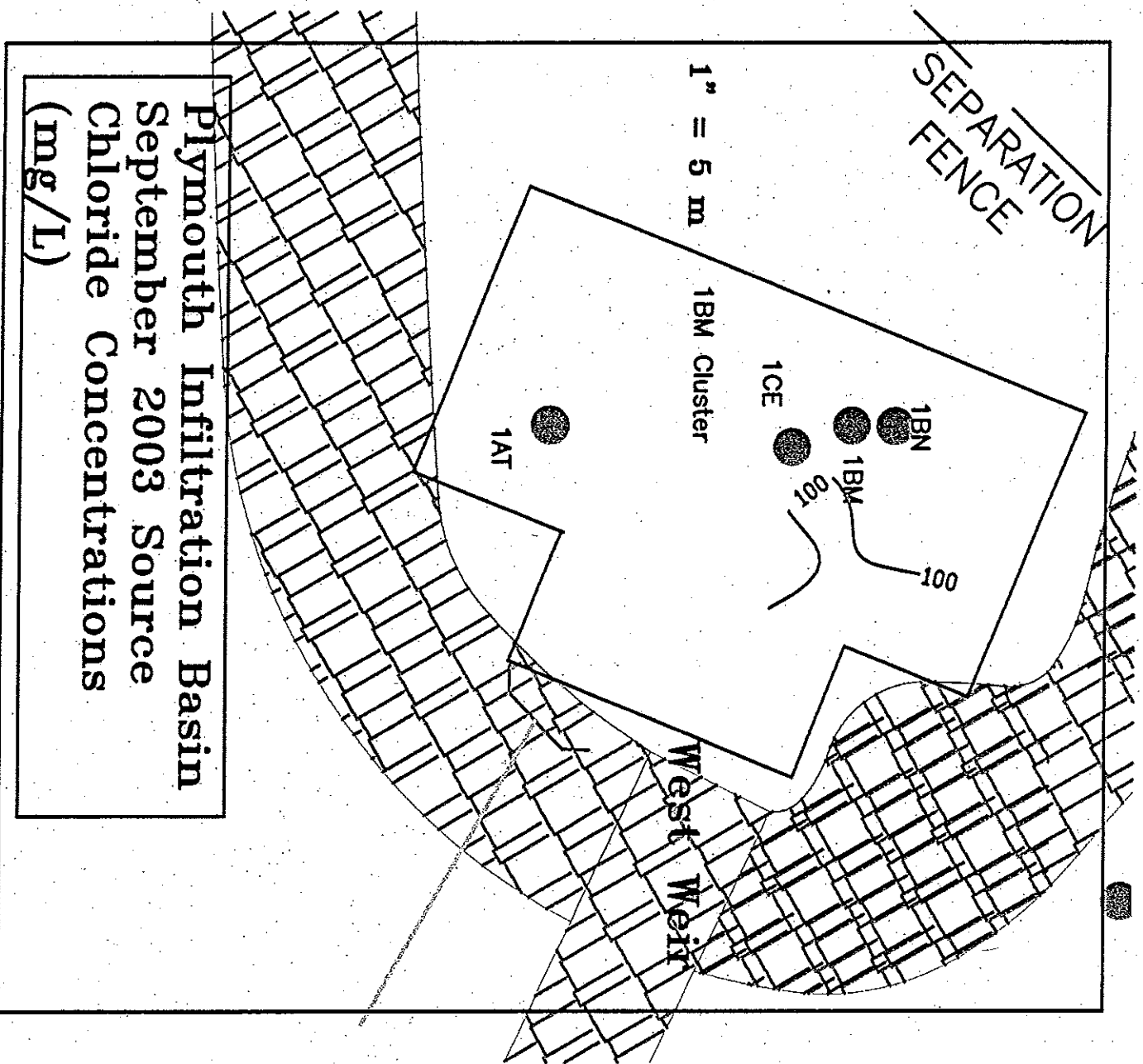


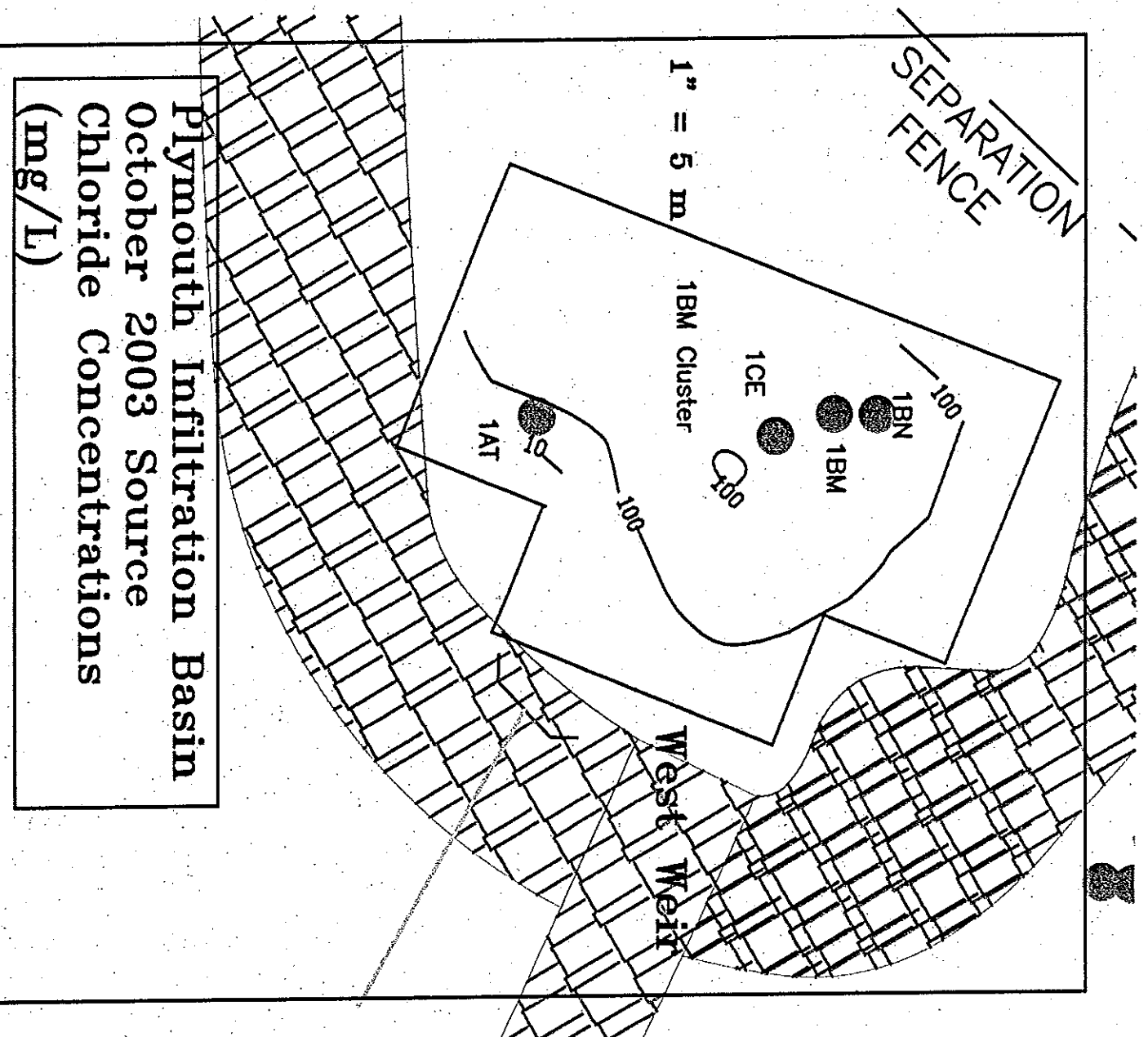


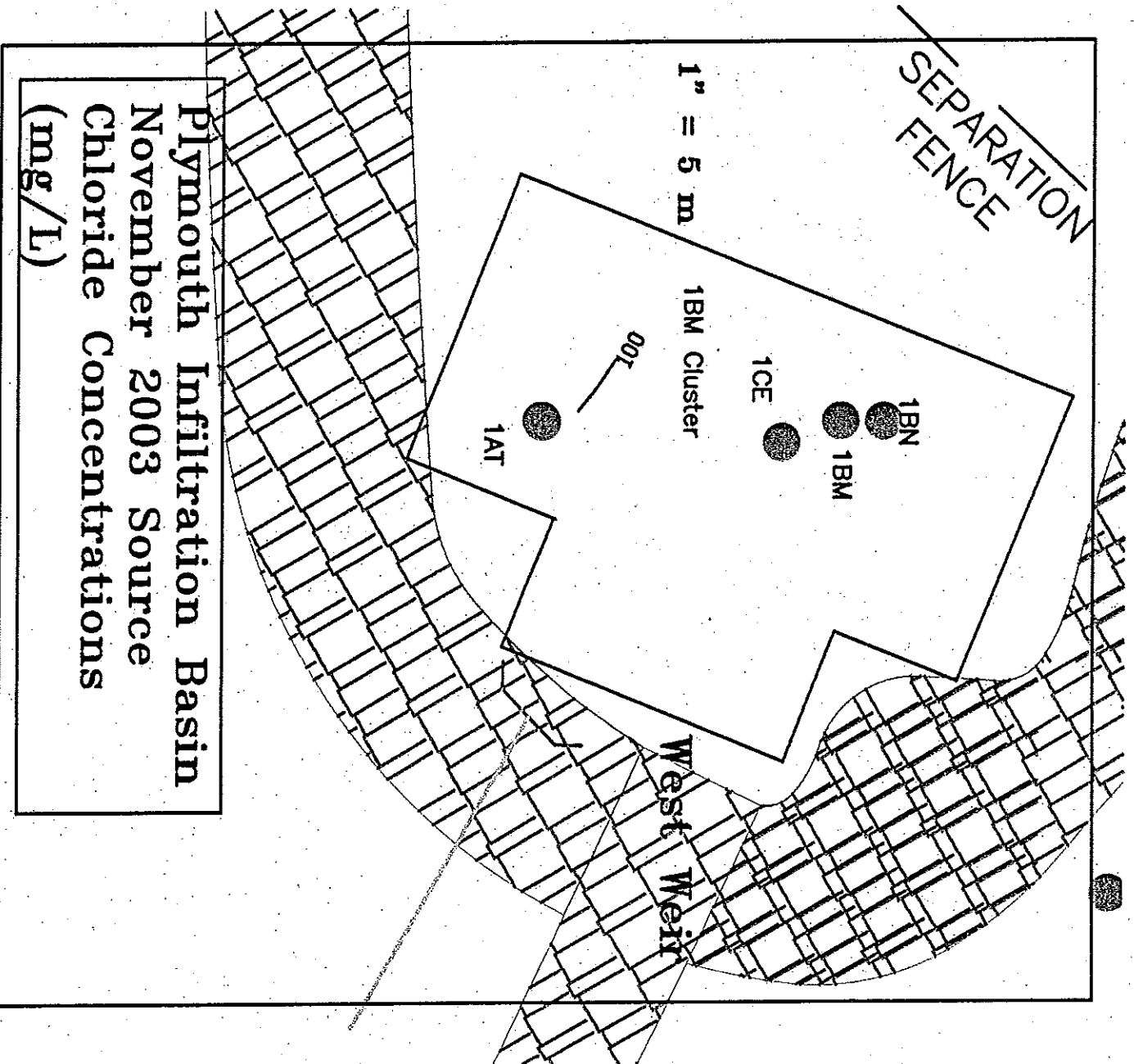


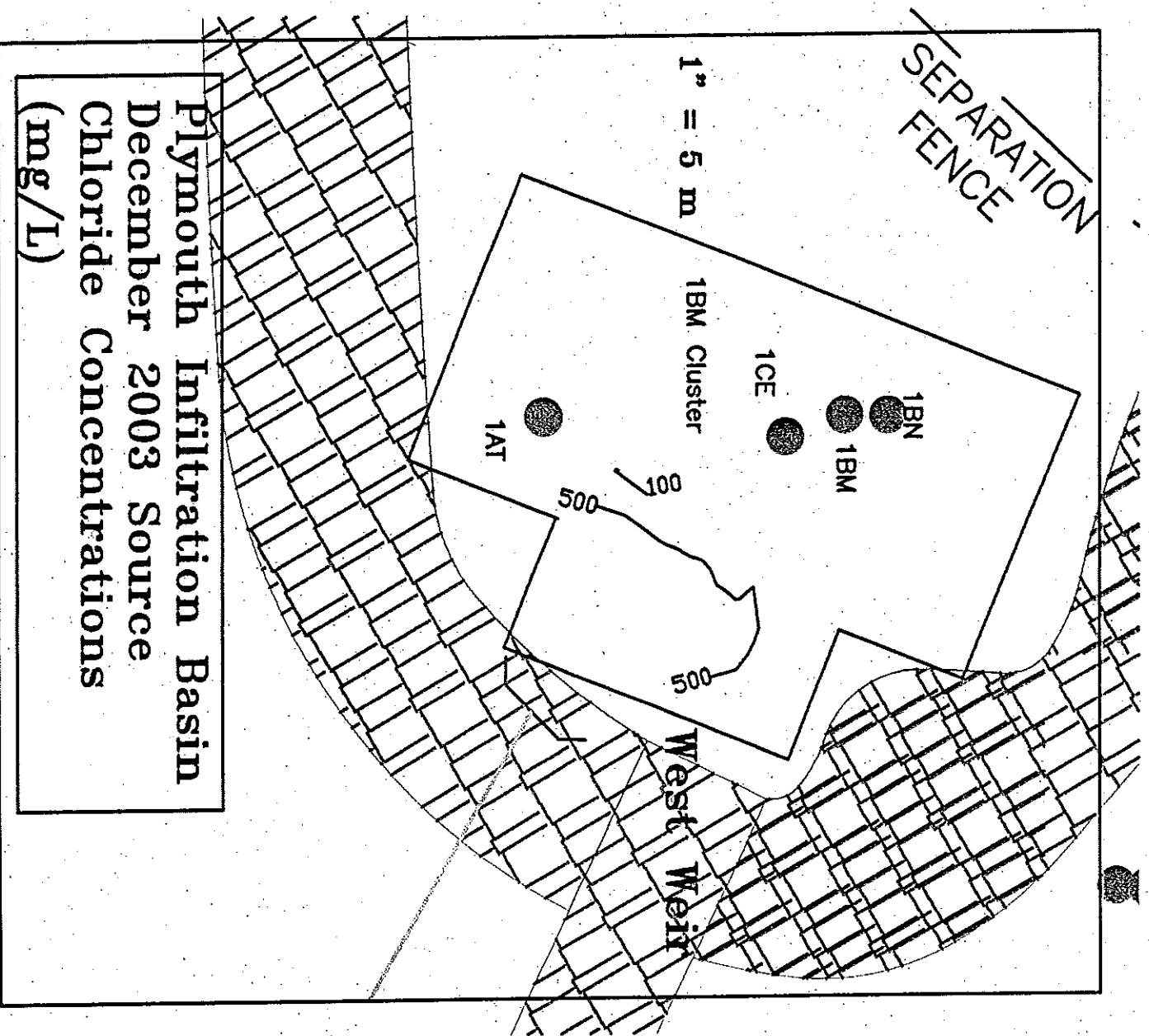


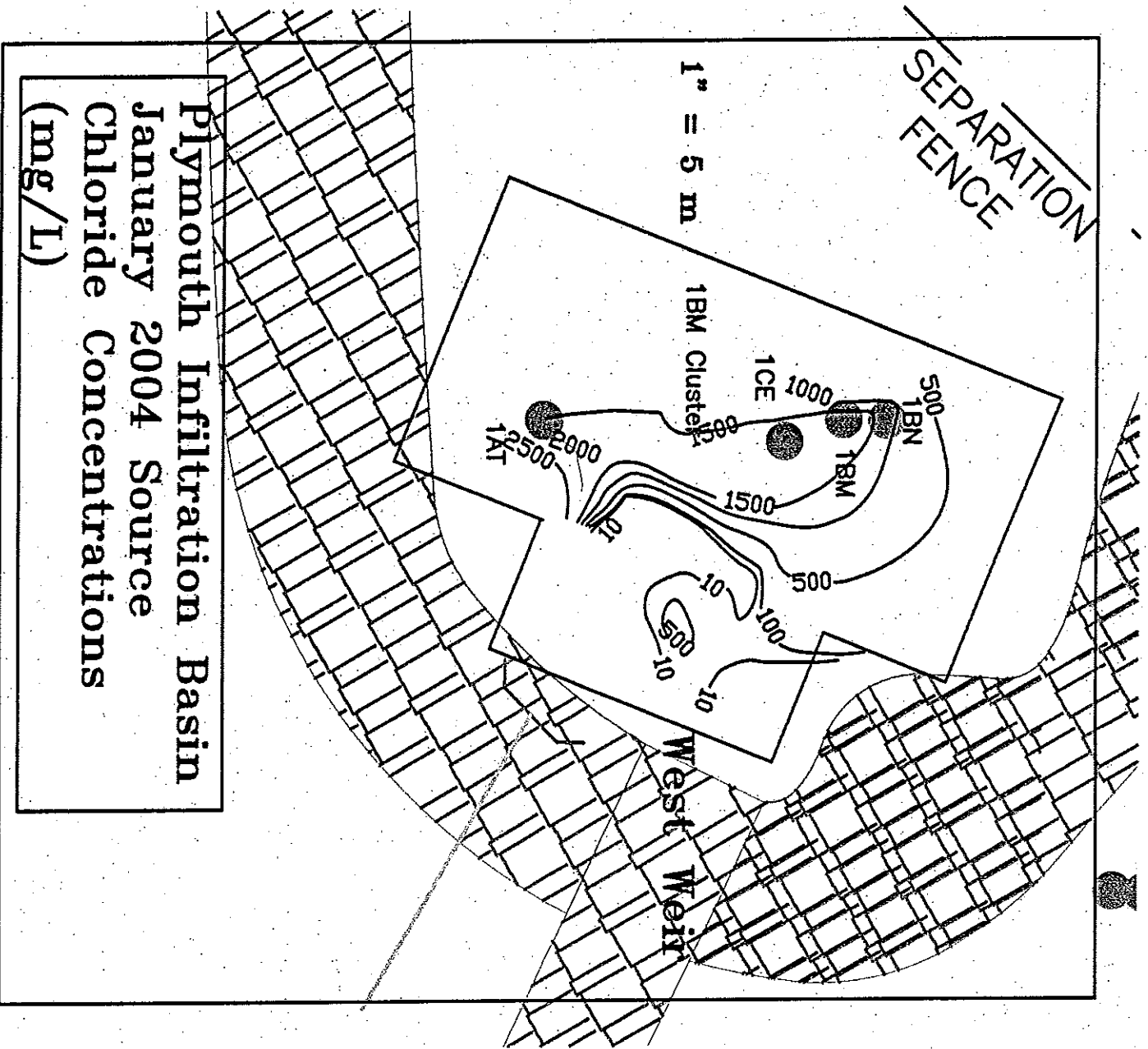


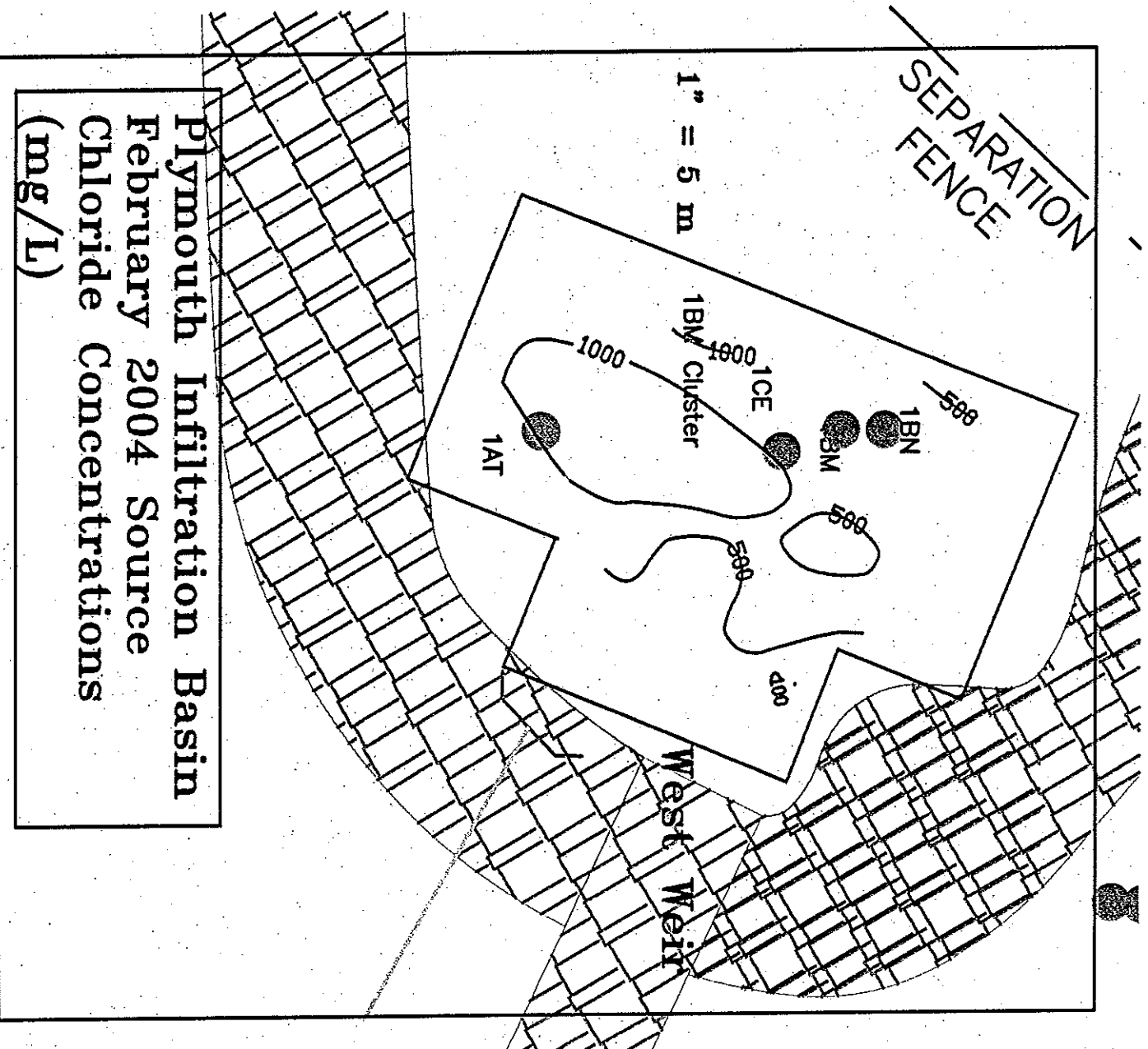


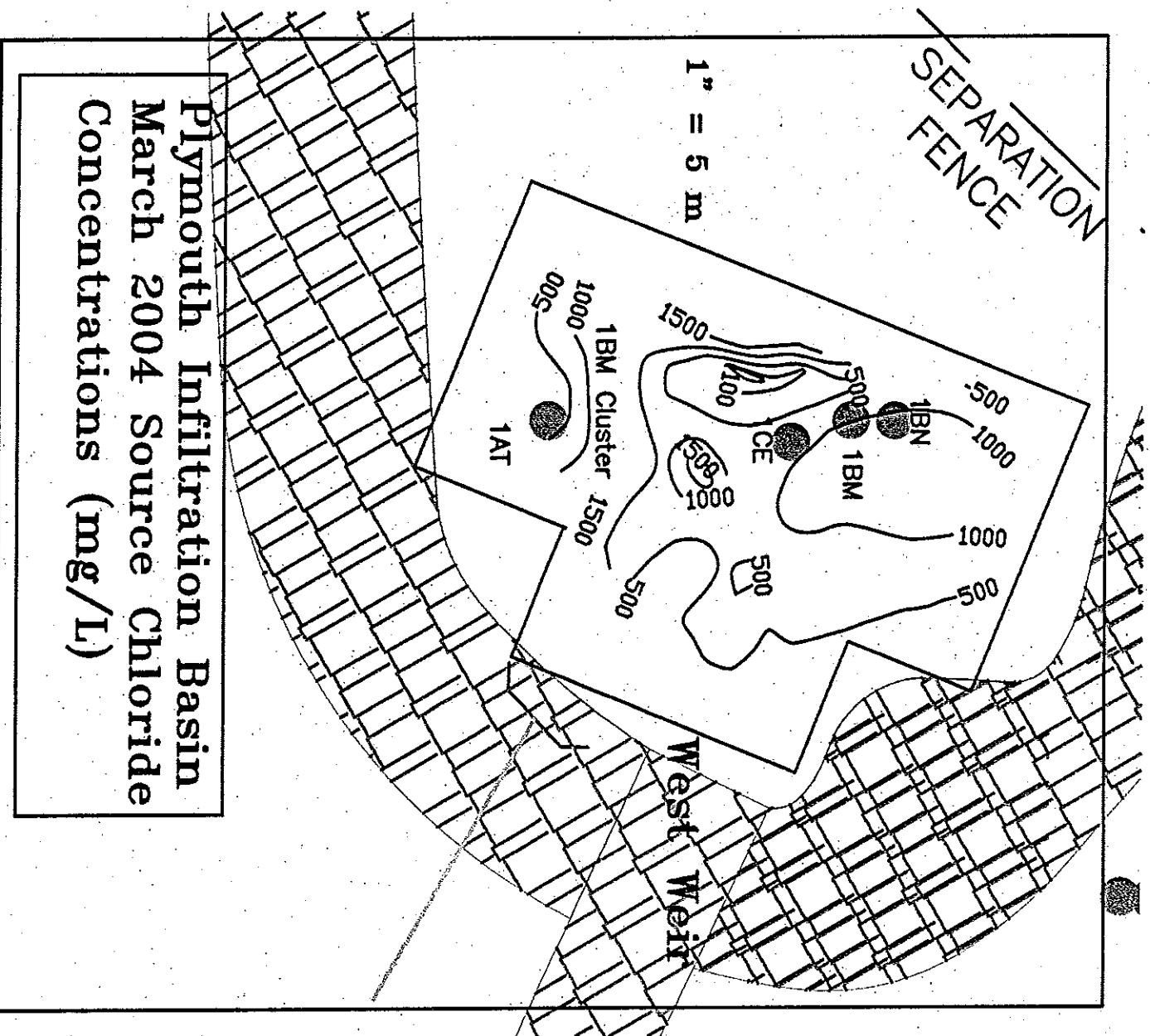


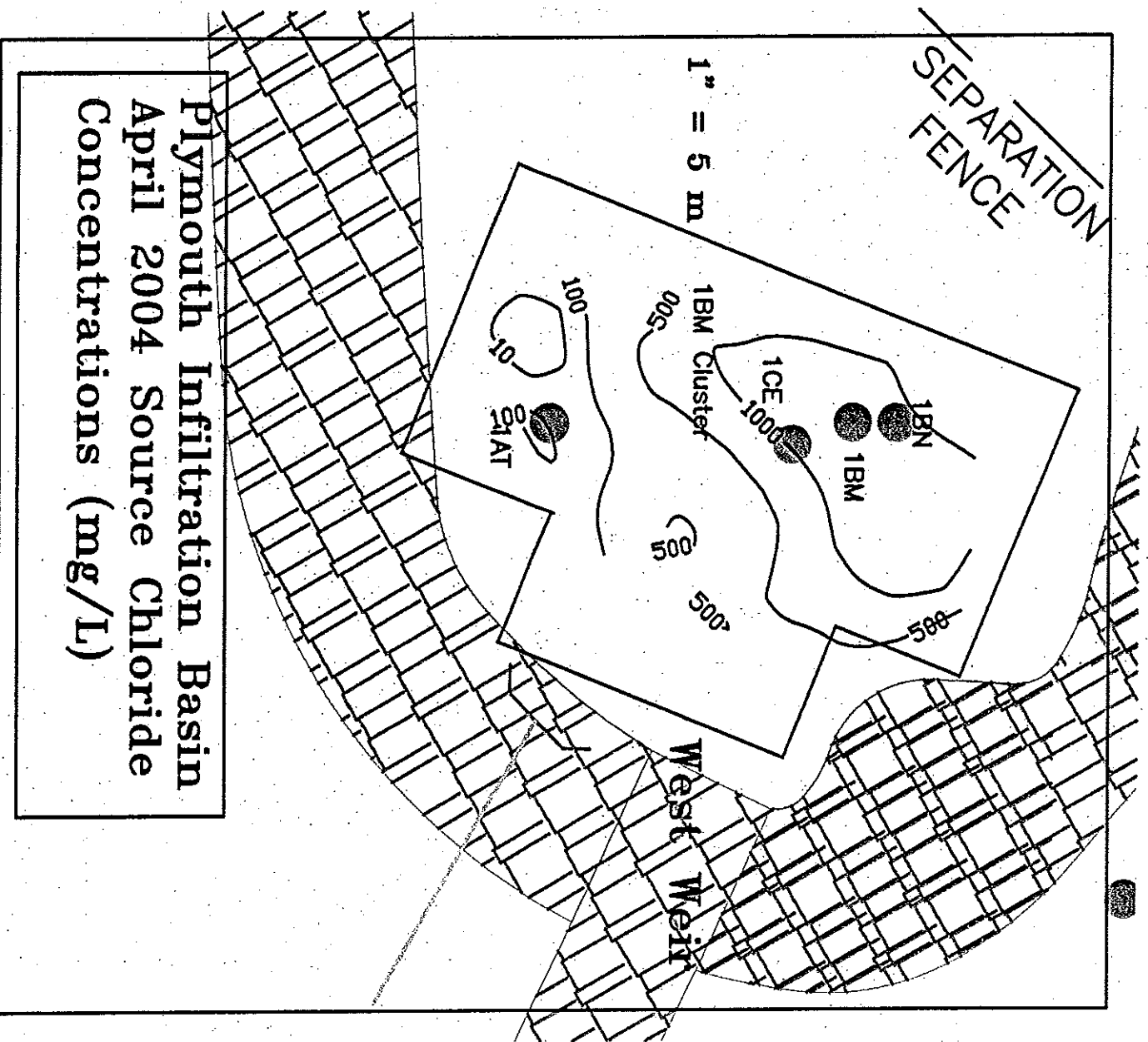


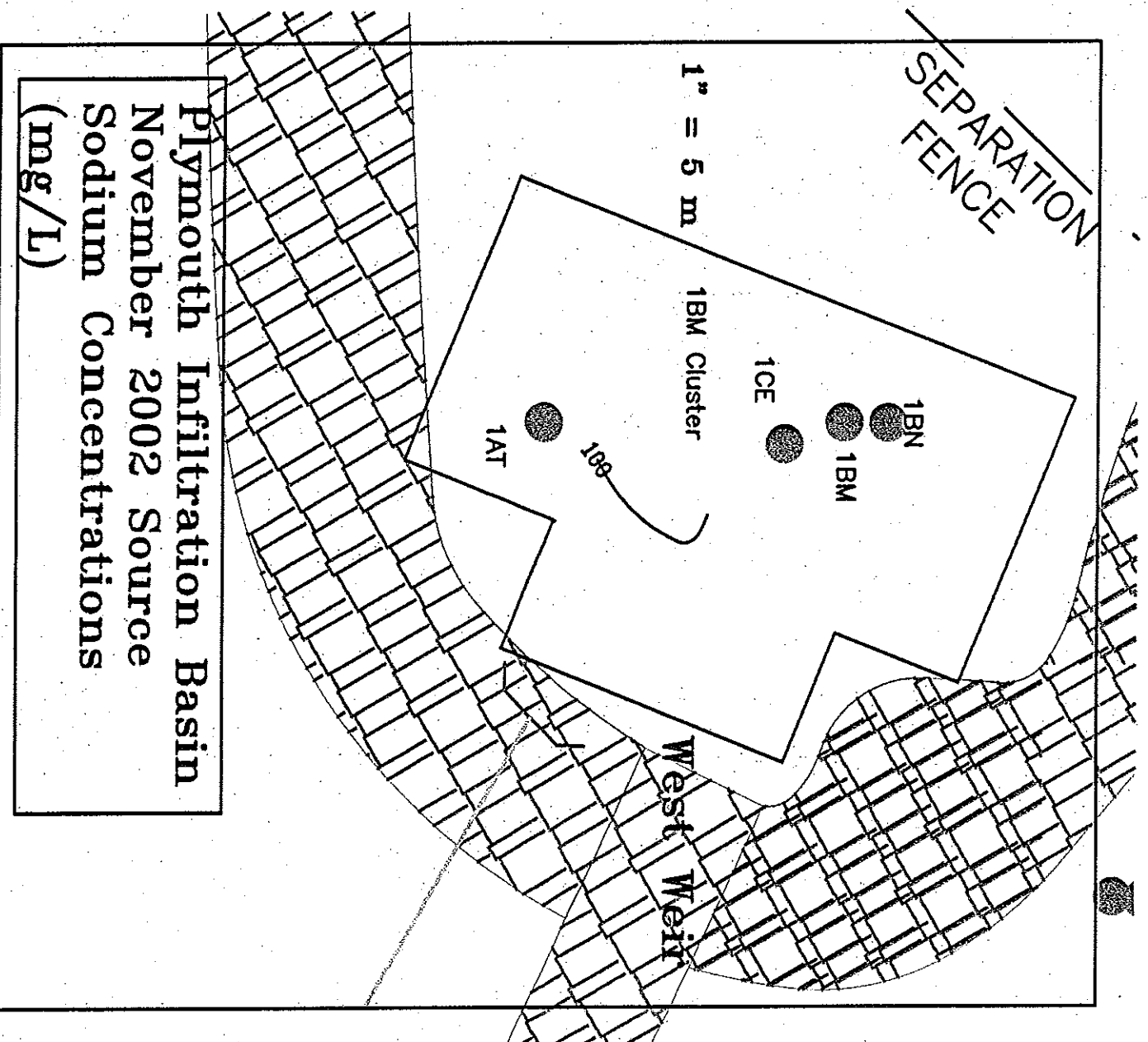


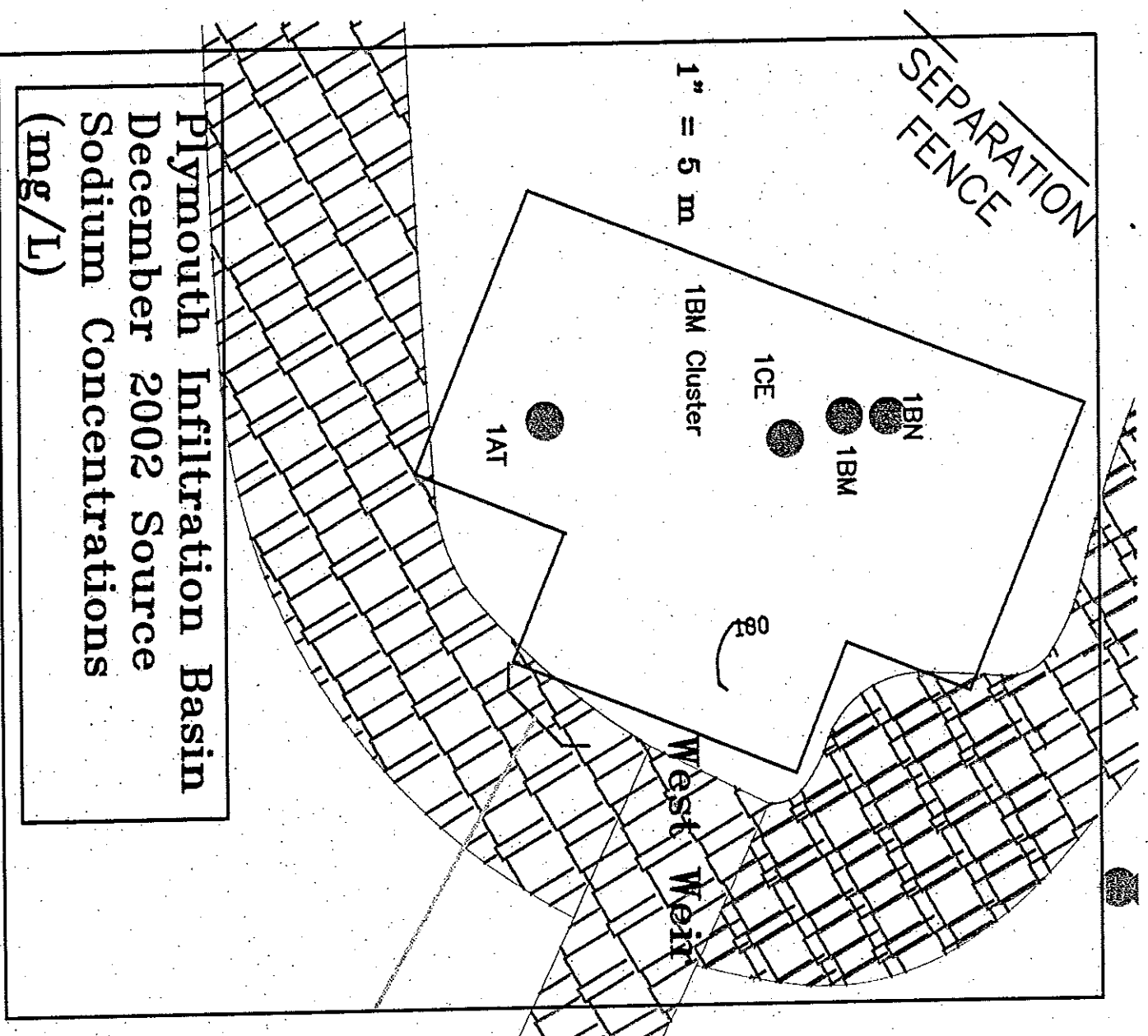


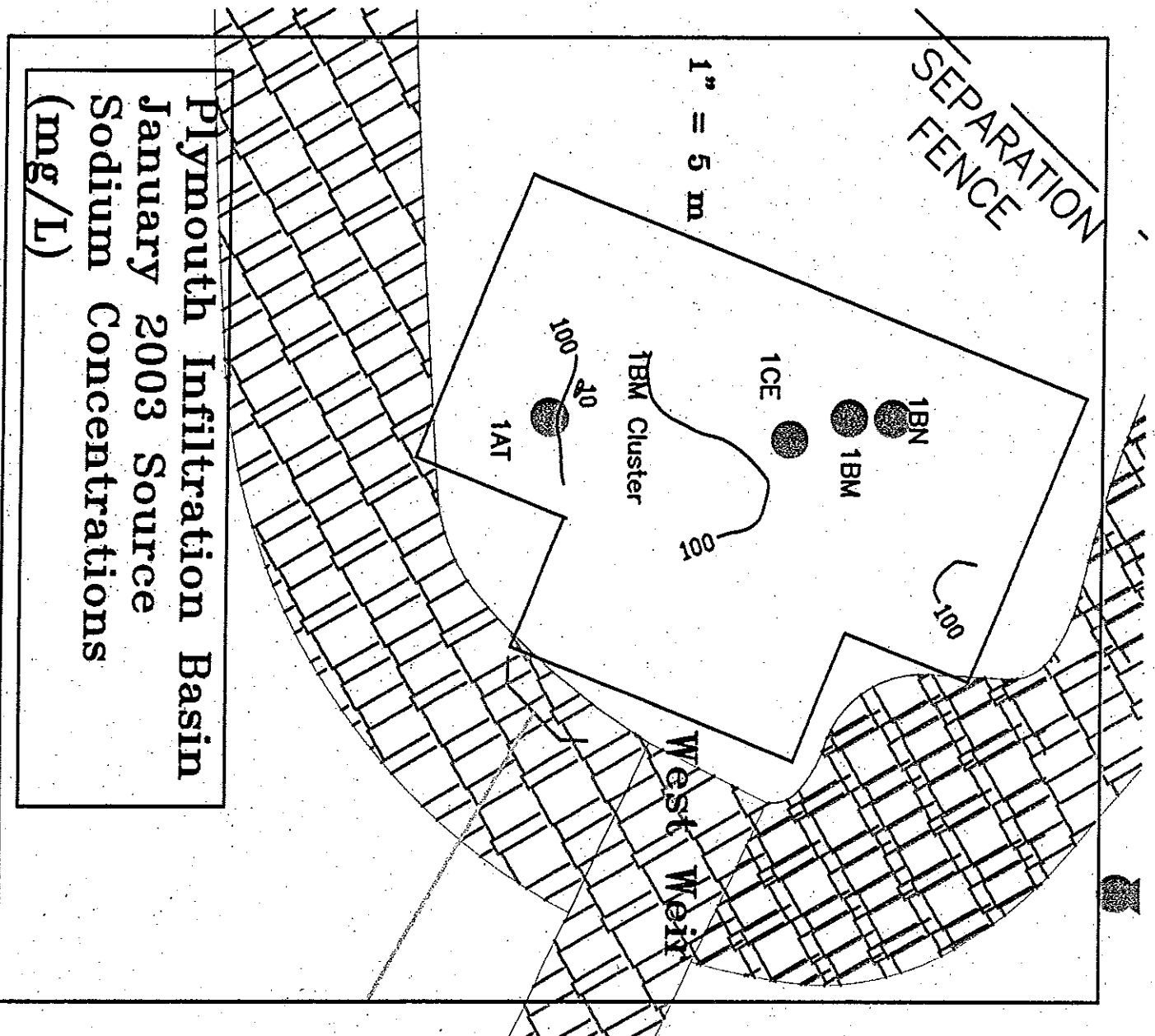


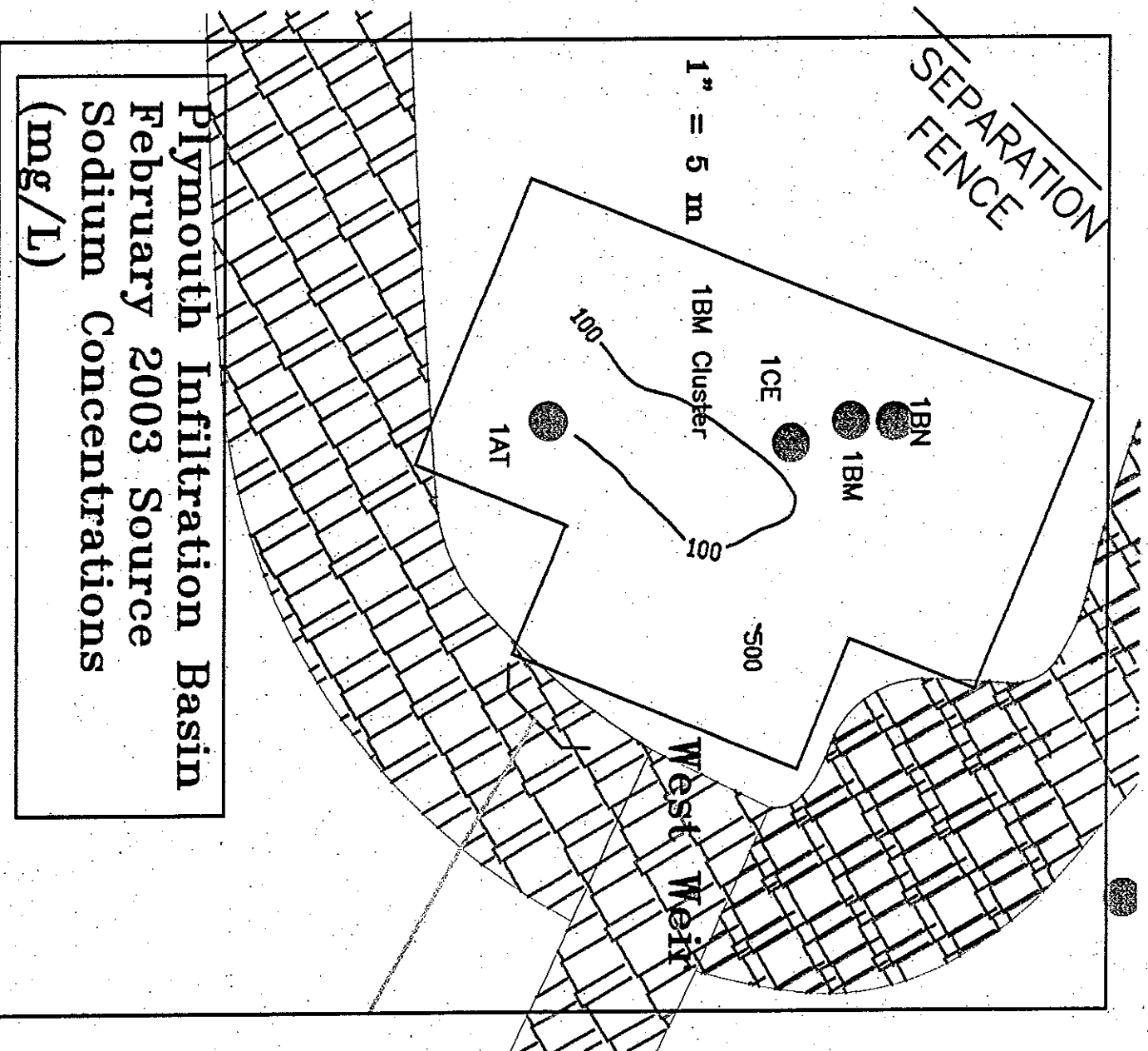


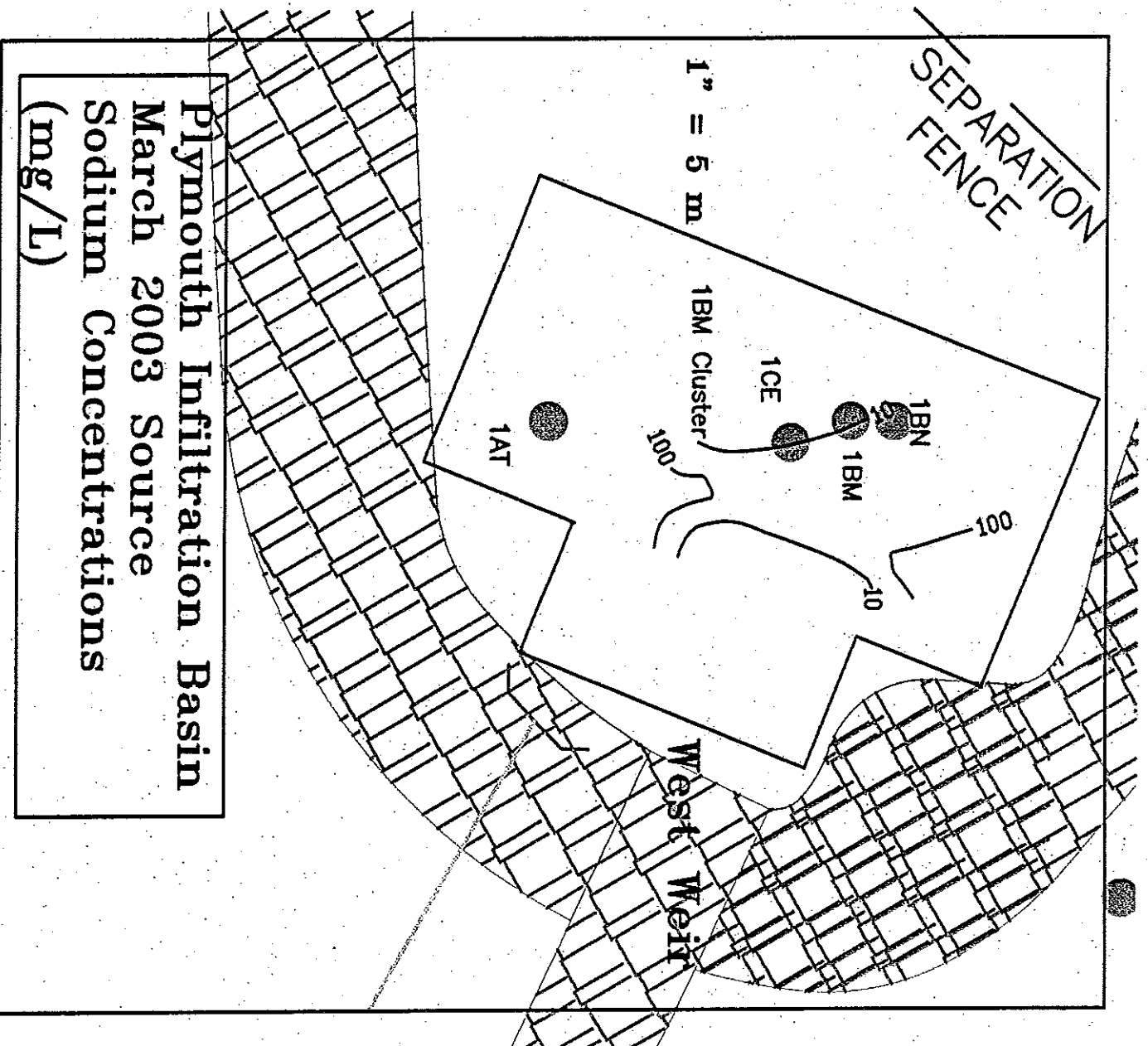


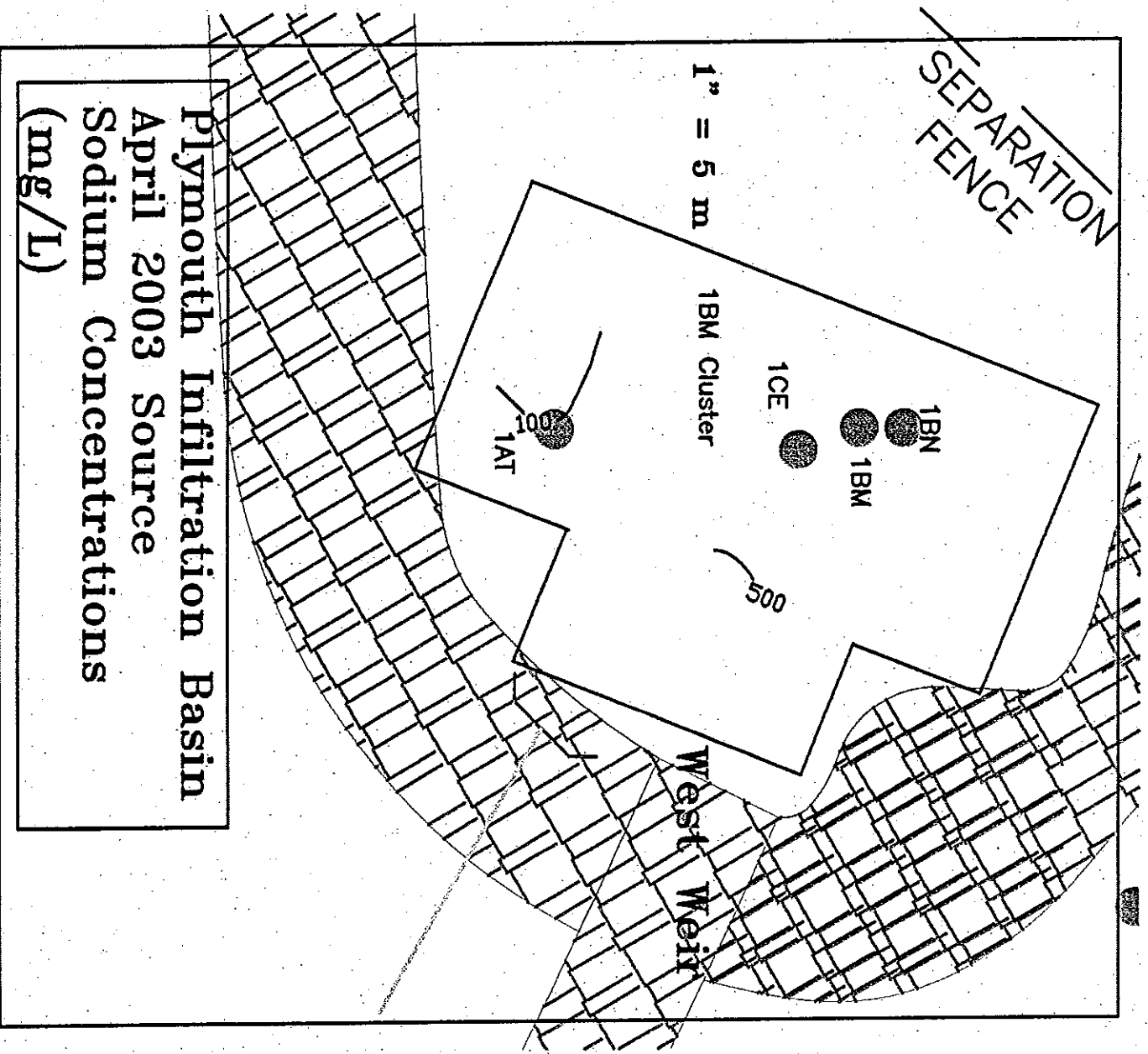


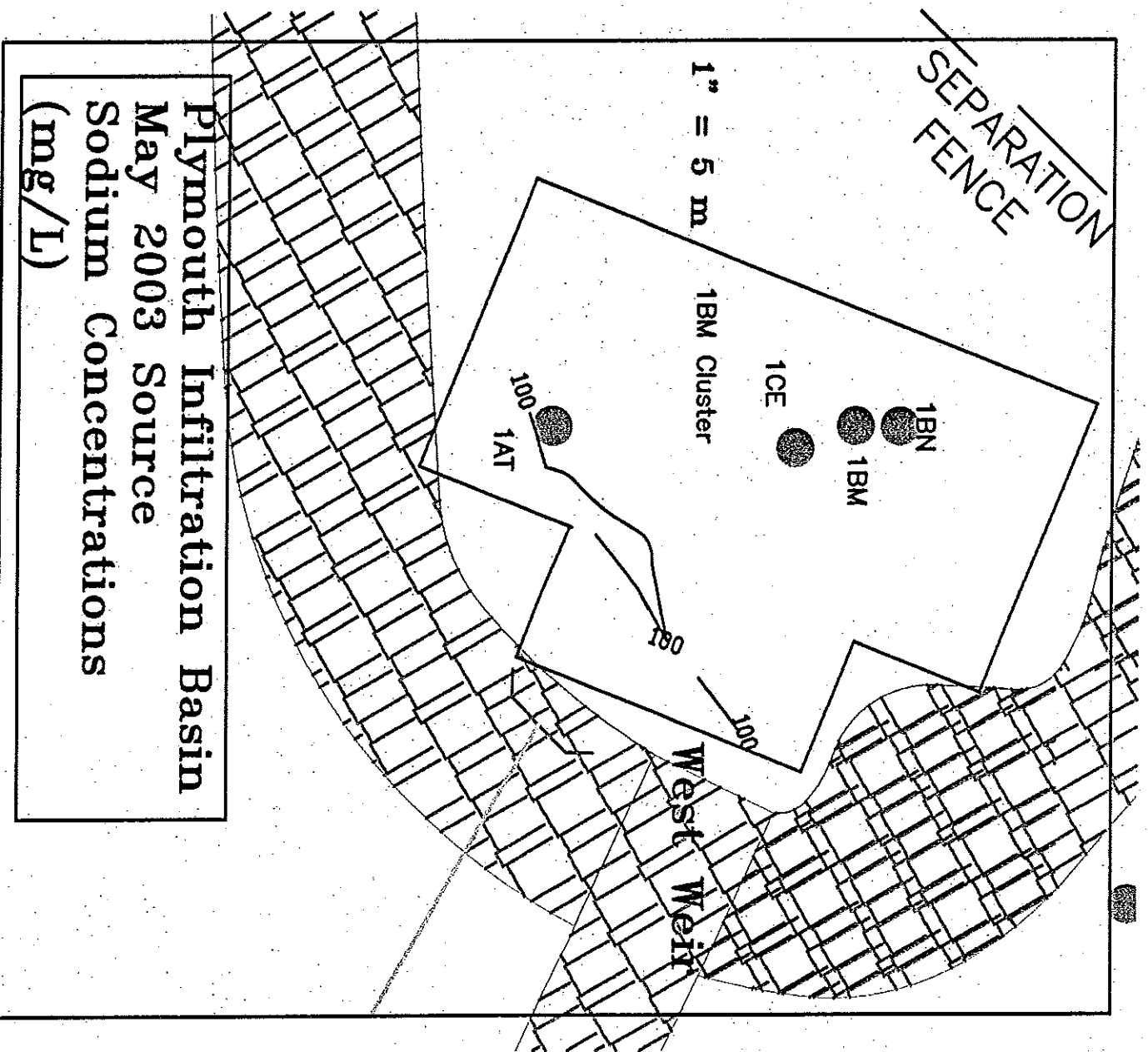


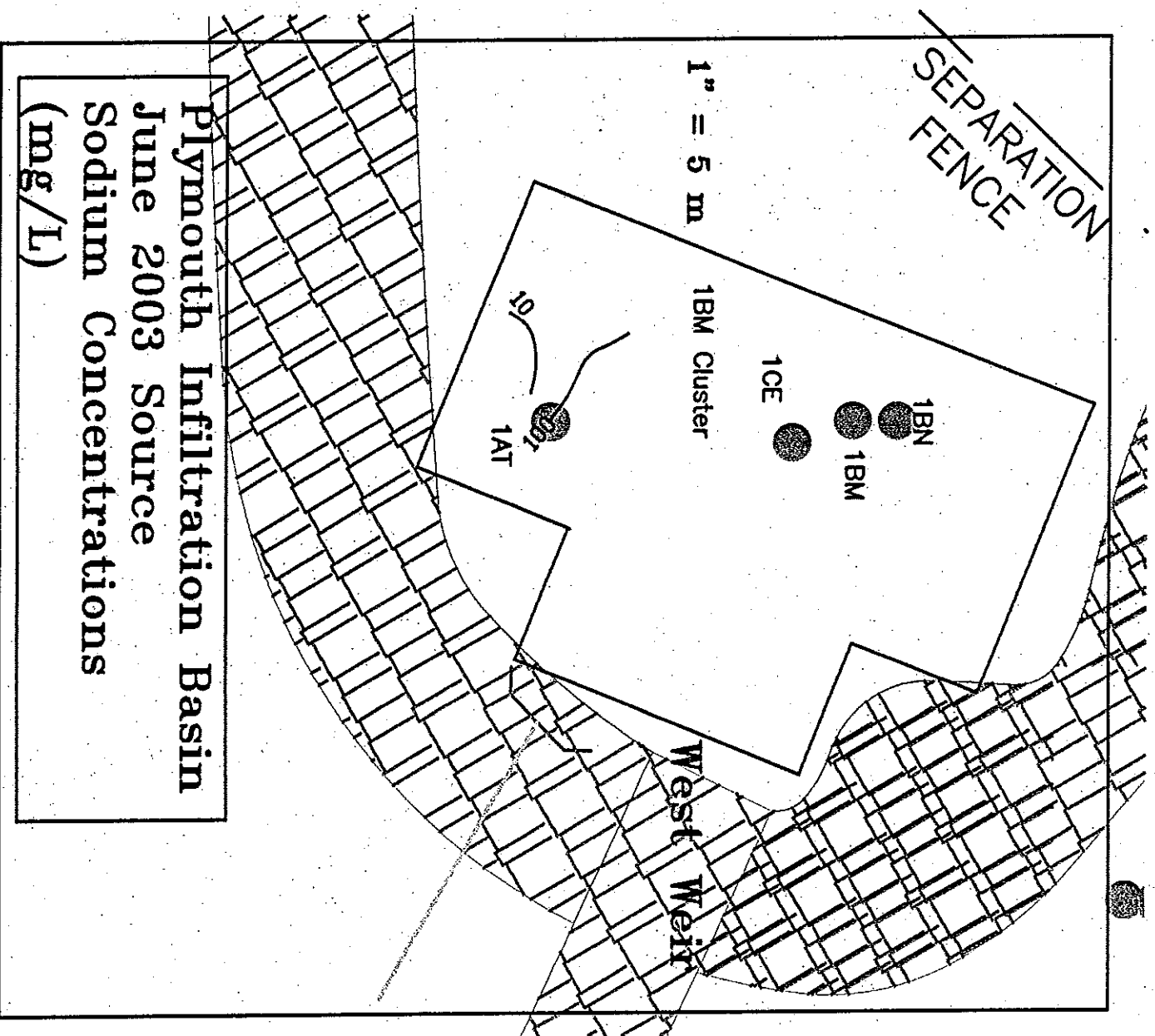


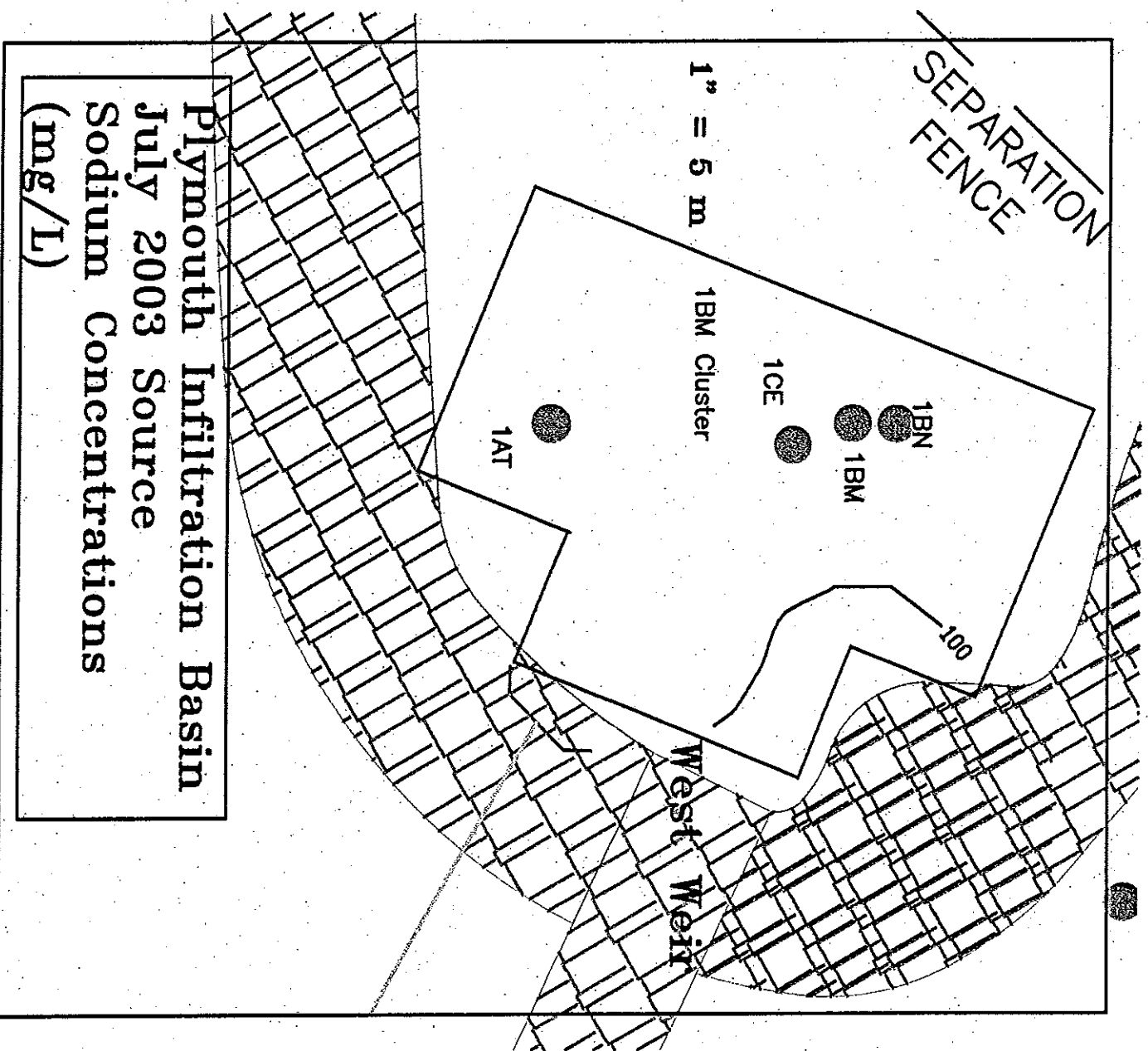


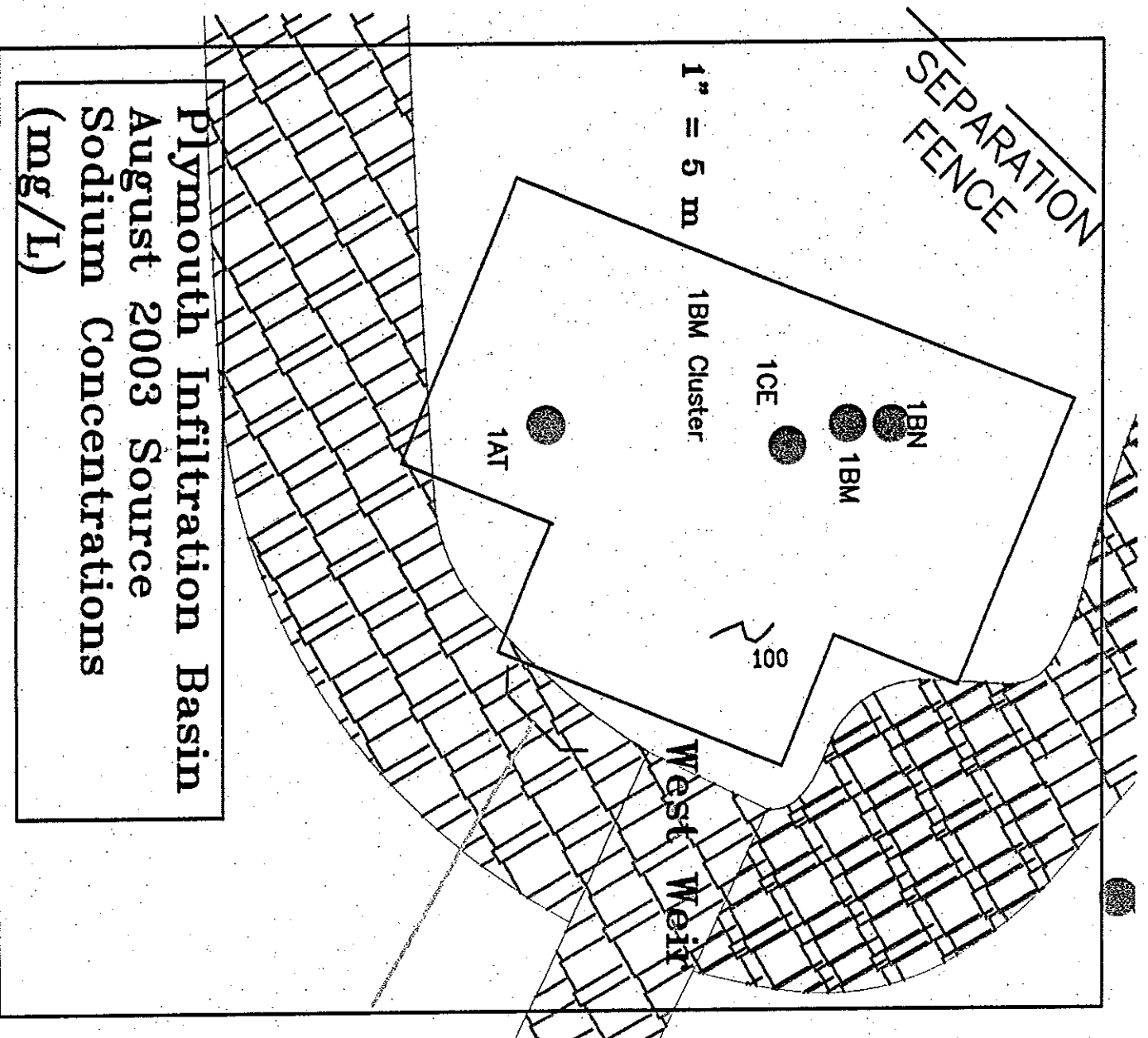


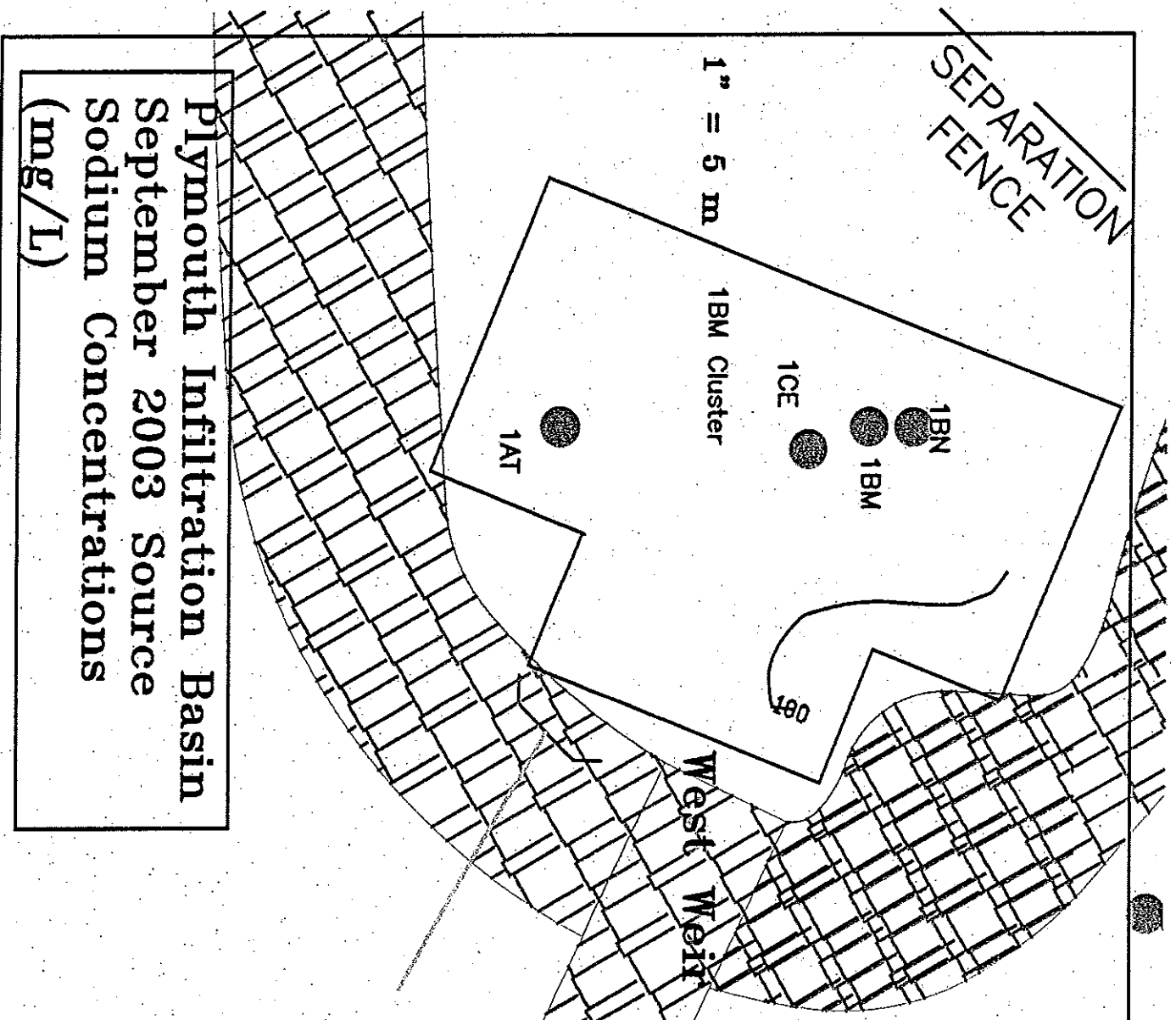


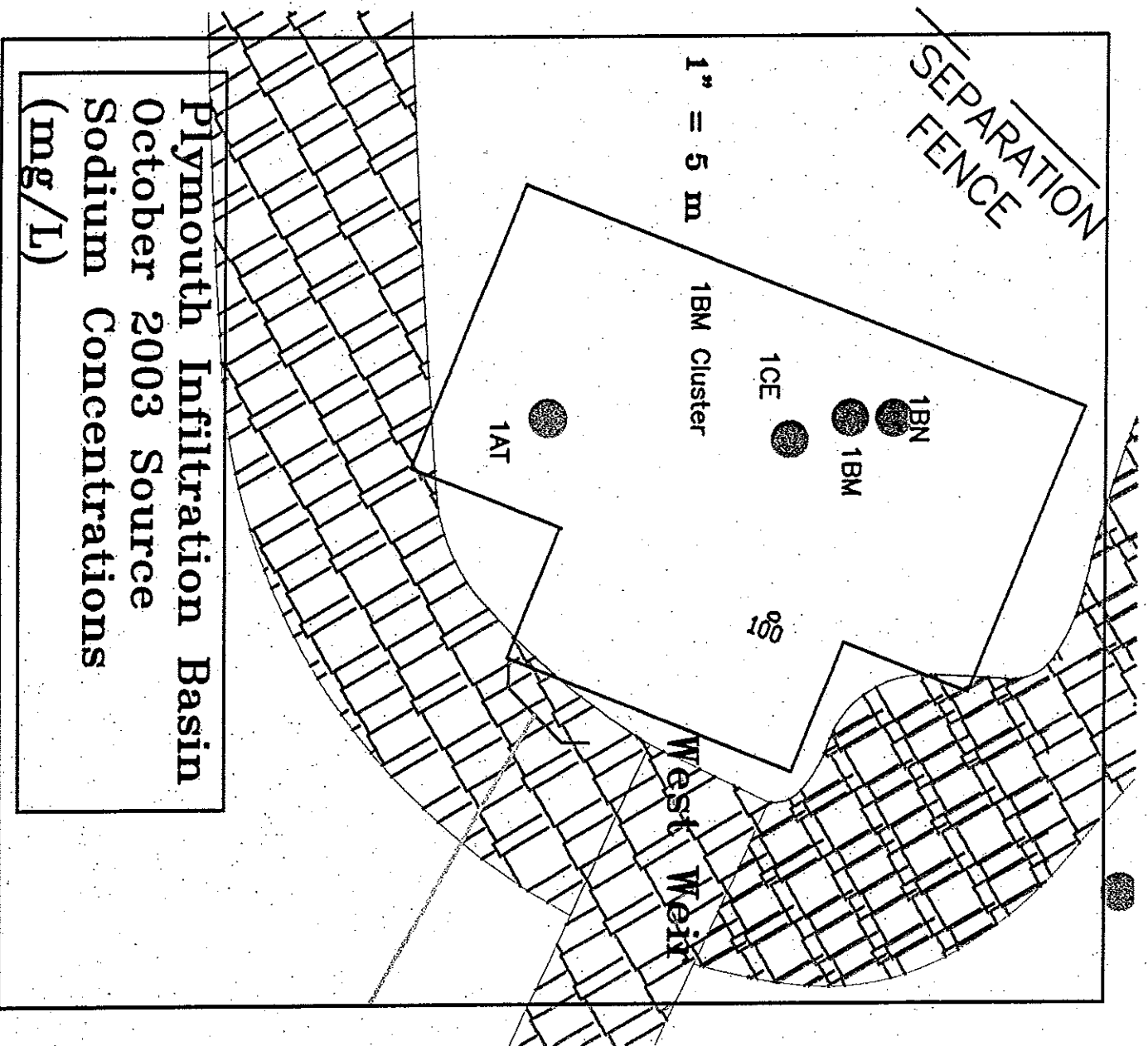


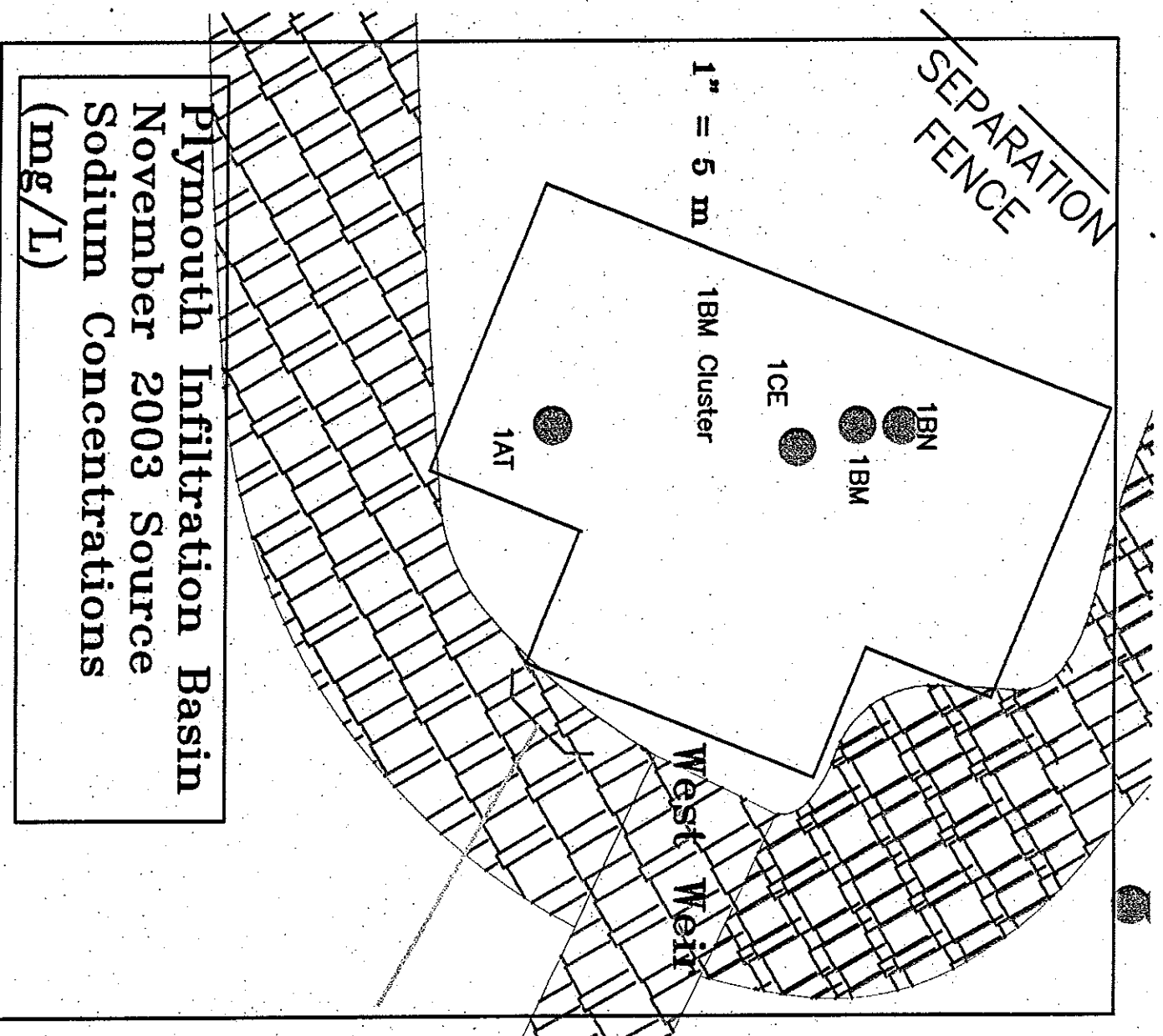


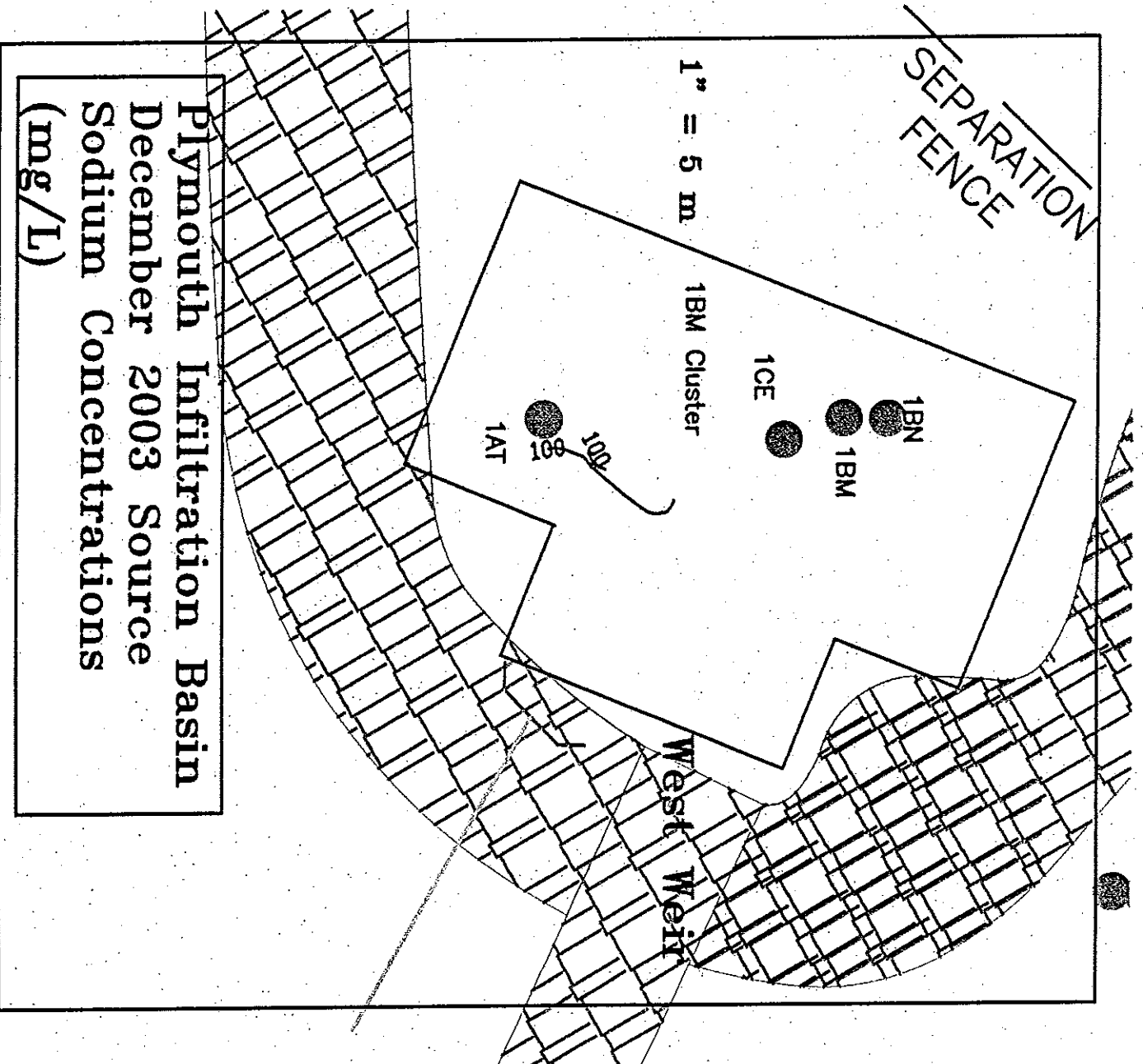




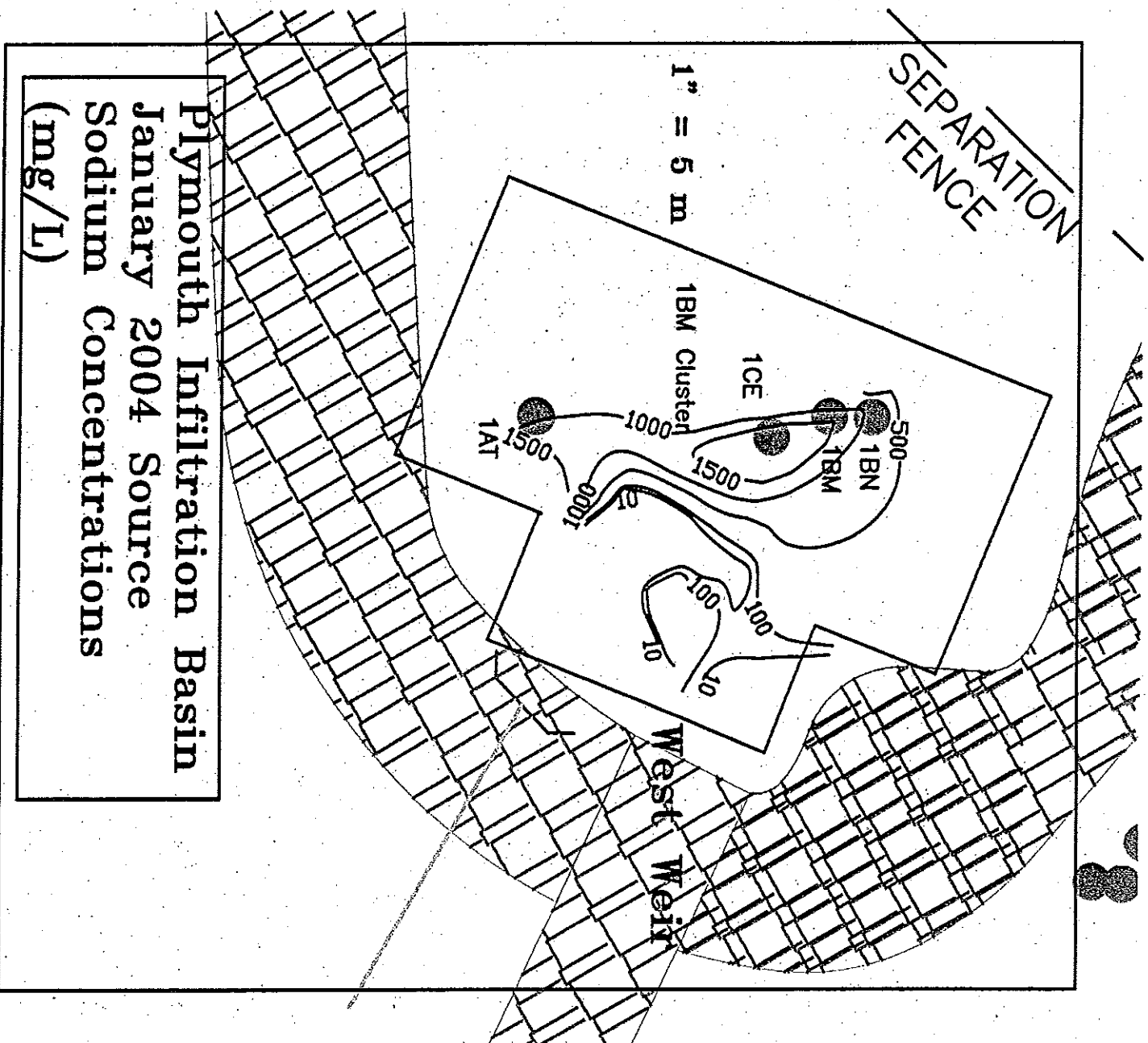


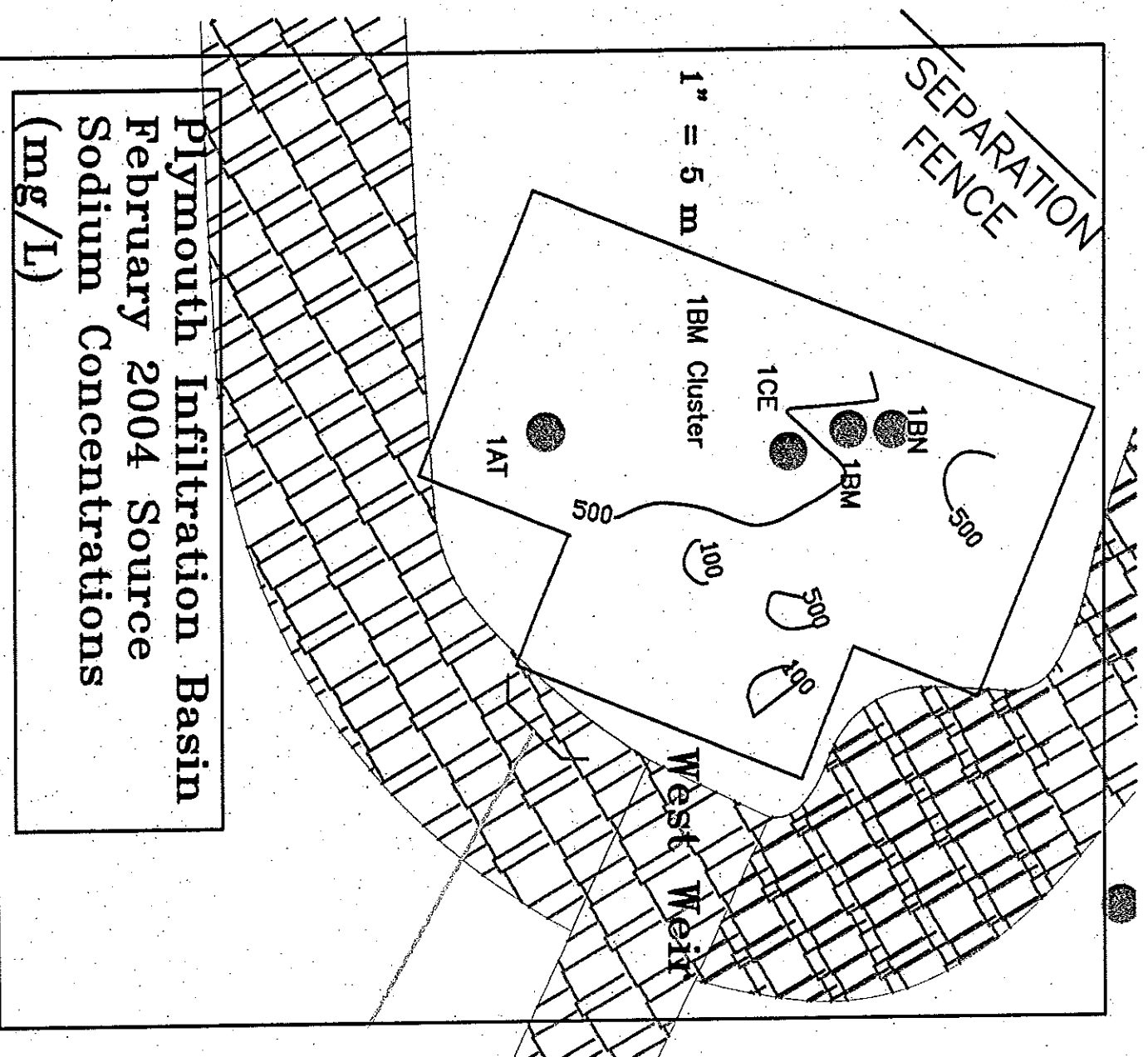


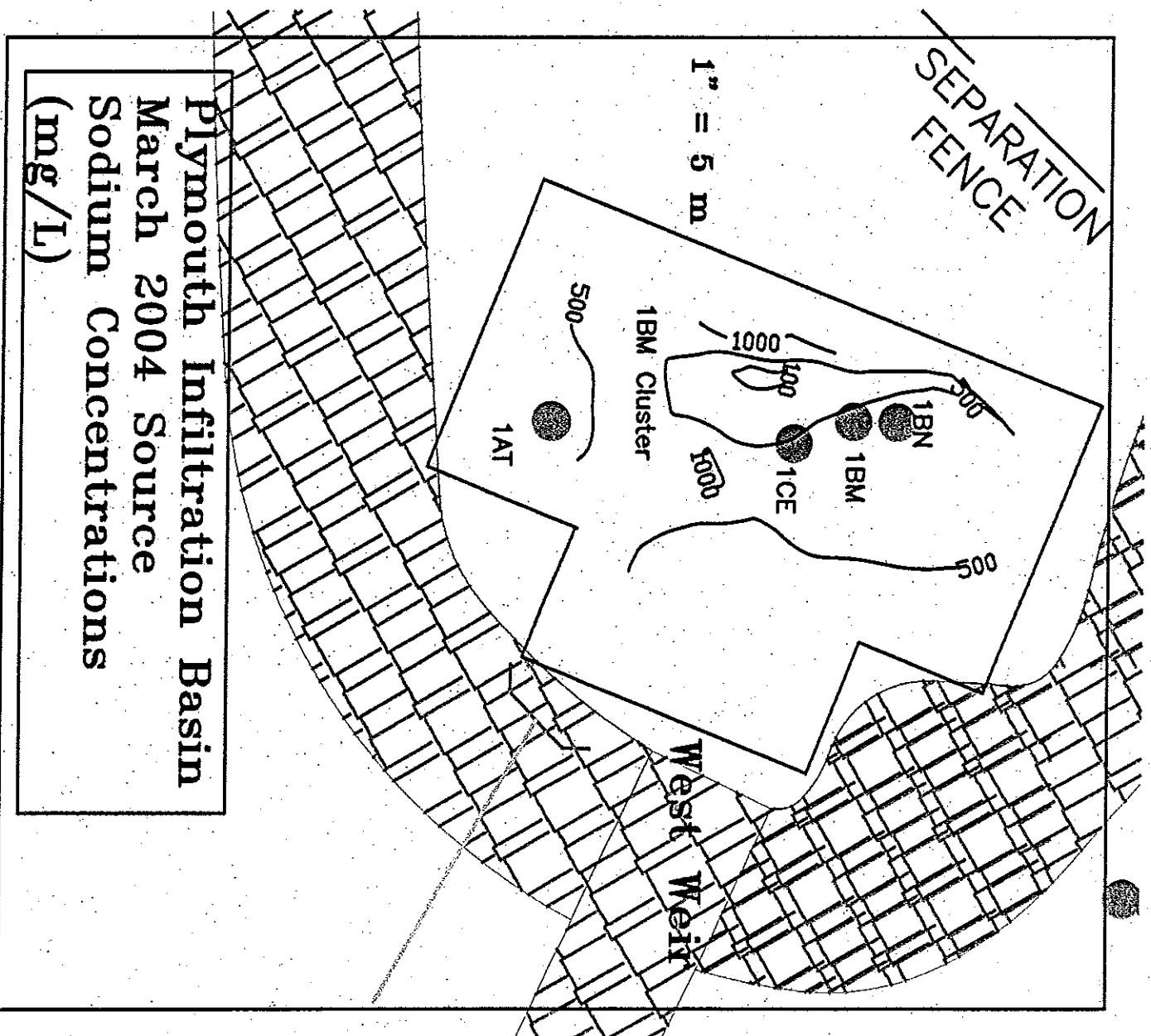


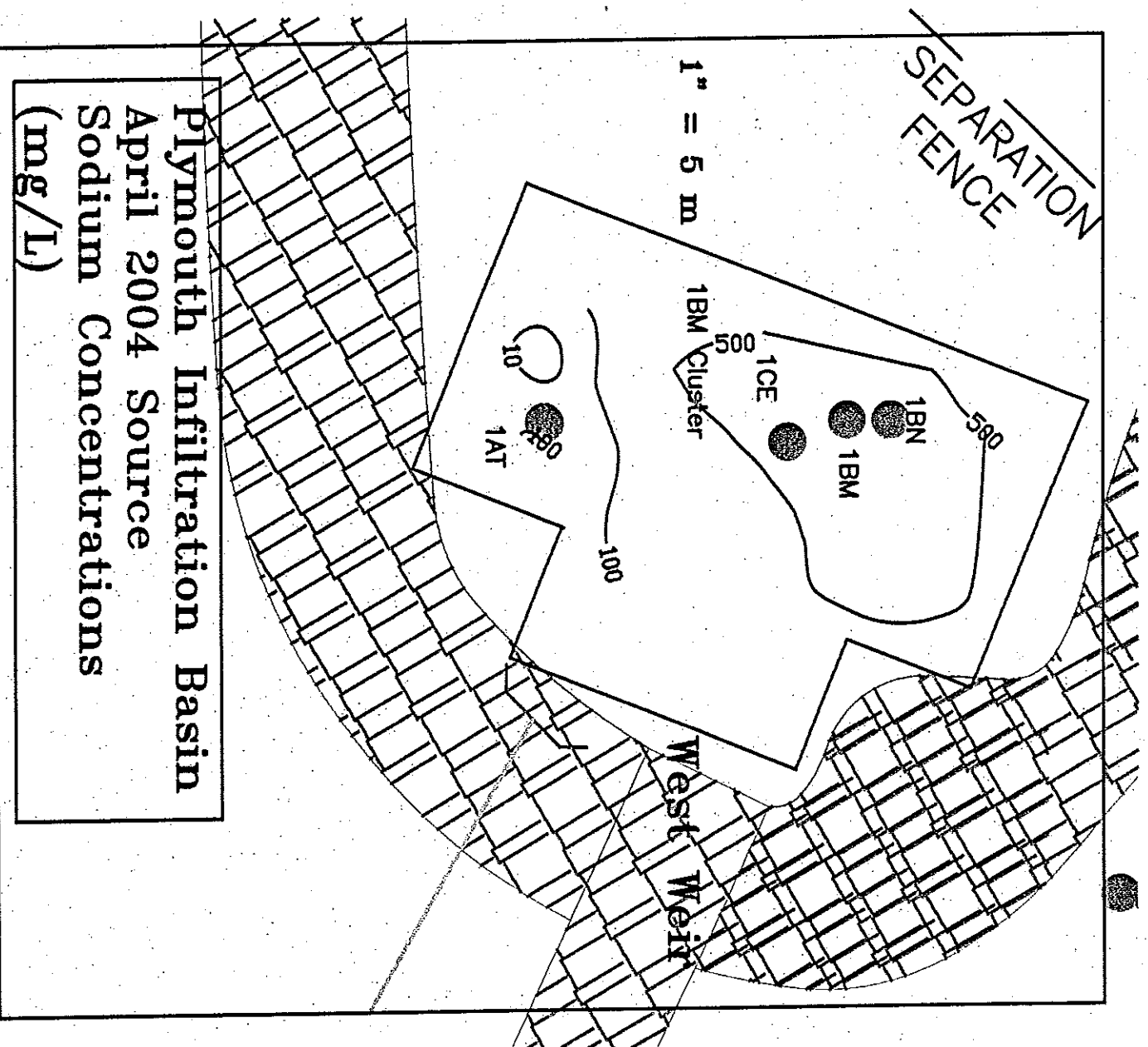


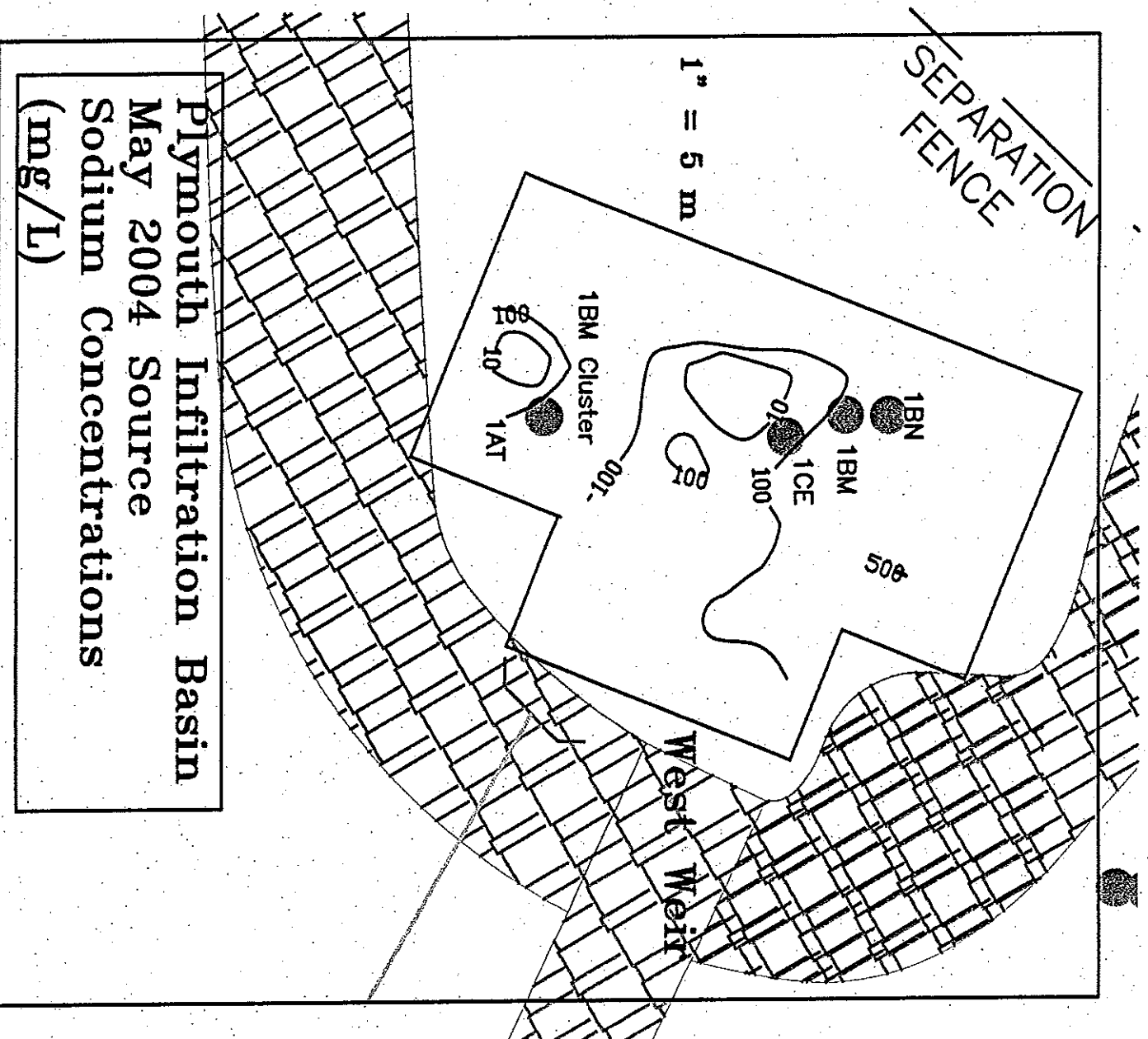
Plymouth Infiltration Basin
December 2003 Source
Sodium Concentrations
(mg/L)





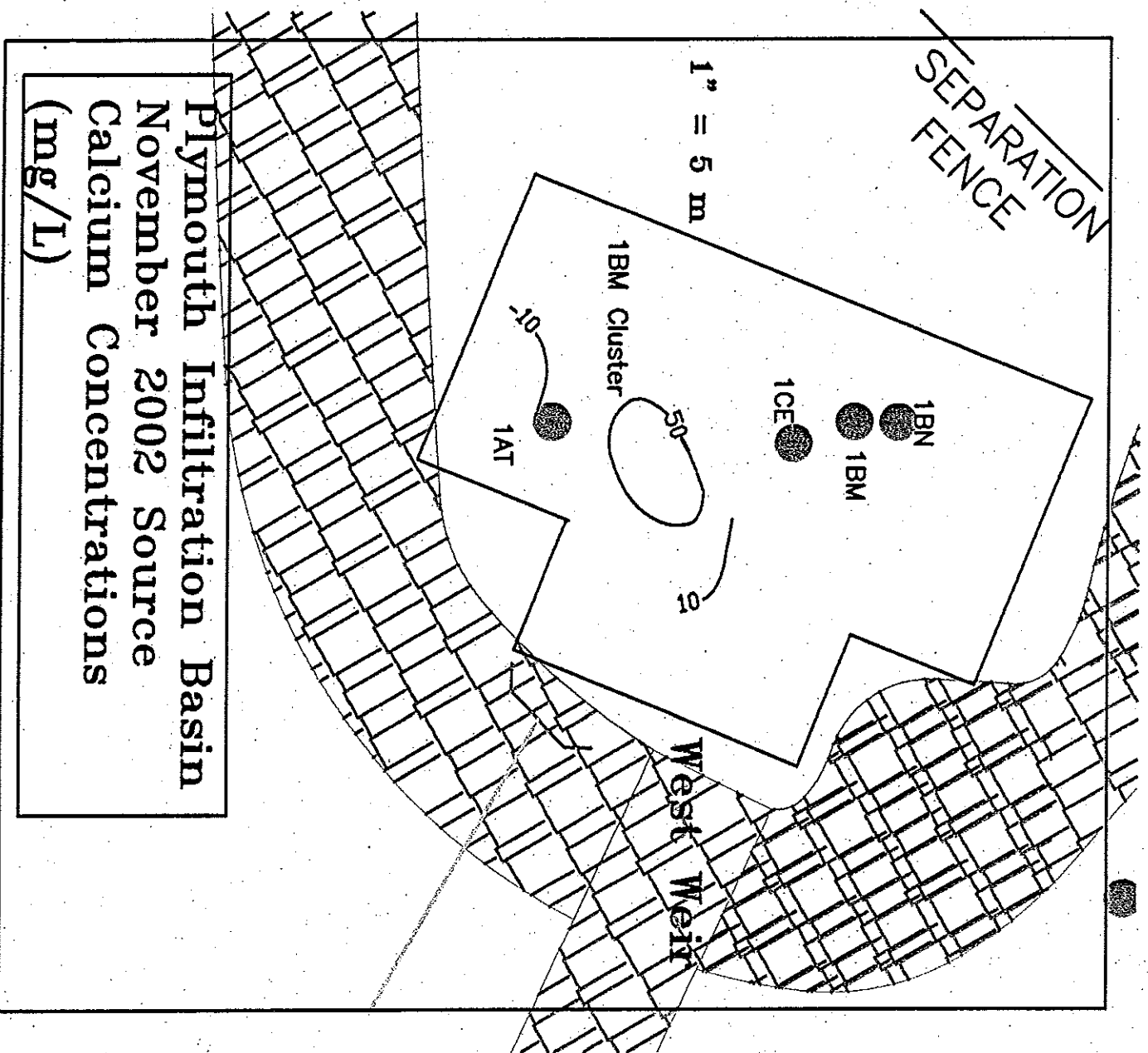


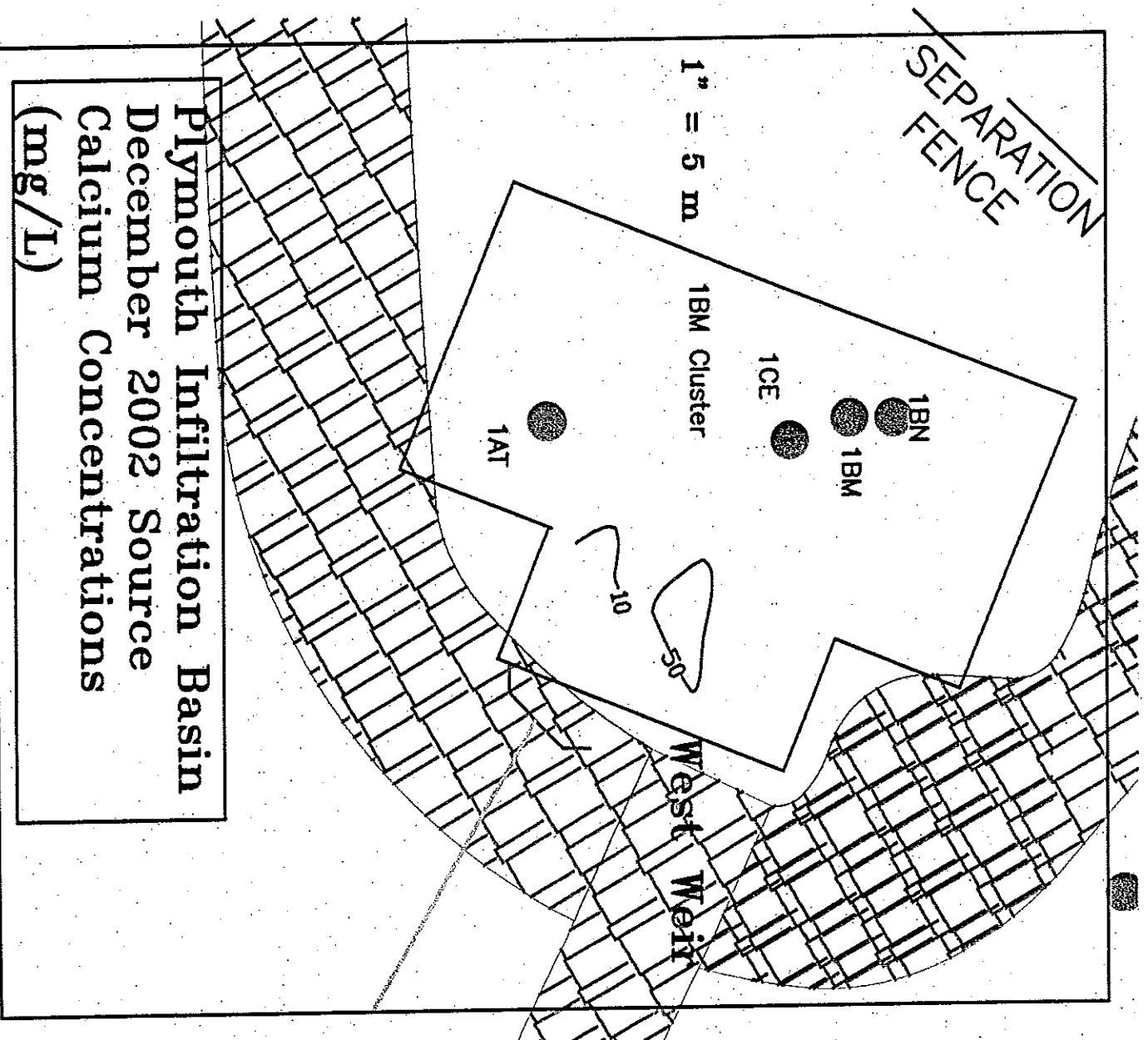


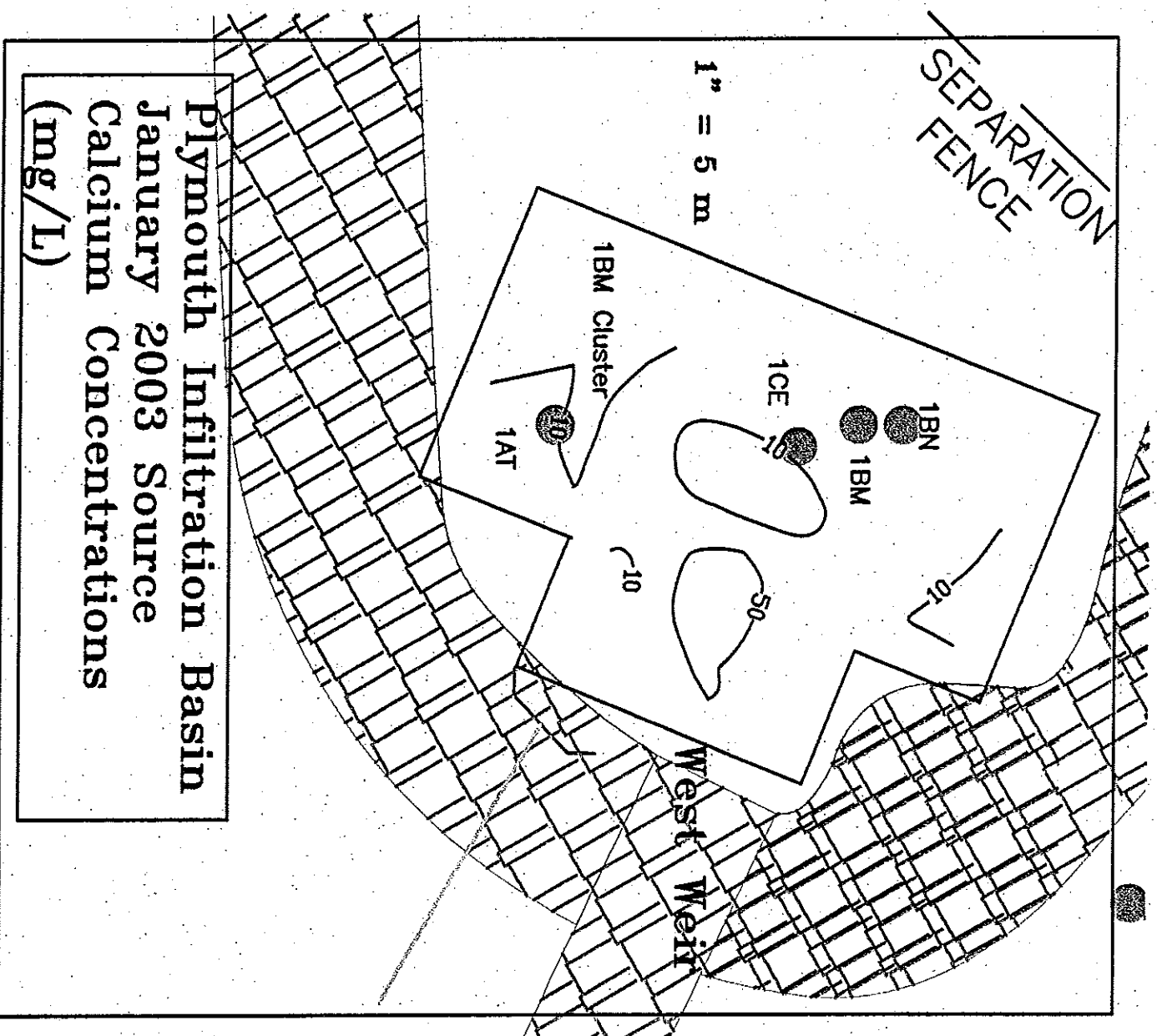


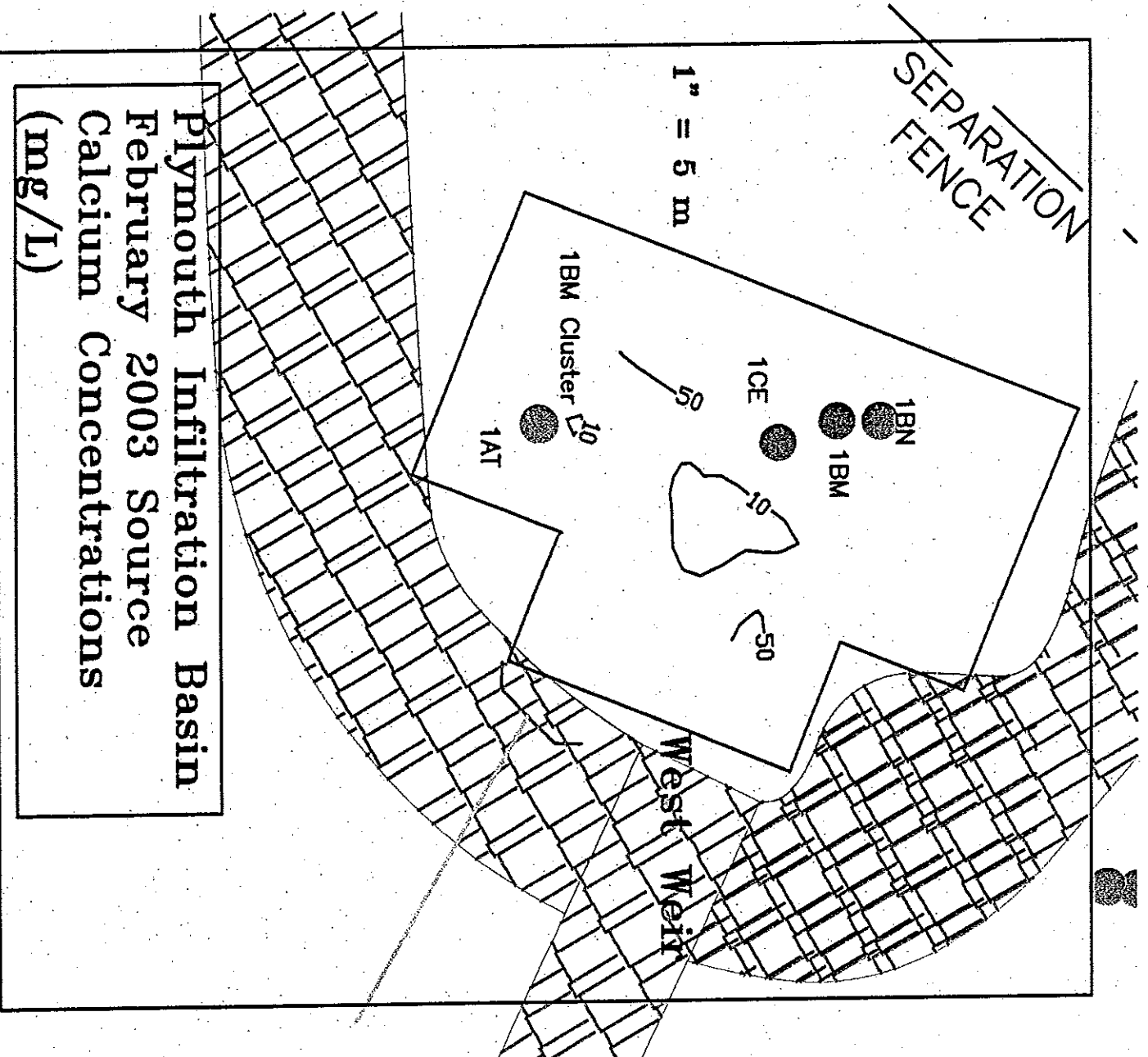
APPENDIX K
Calcium Source Isopleths, November 2002 – May 2004

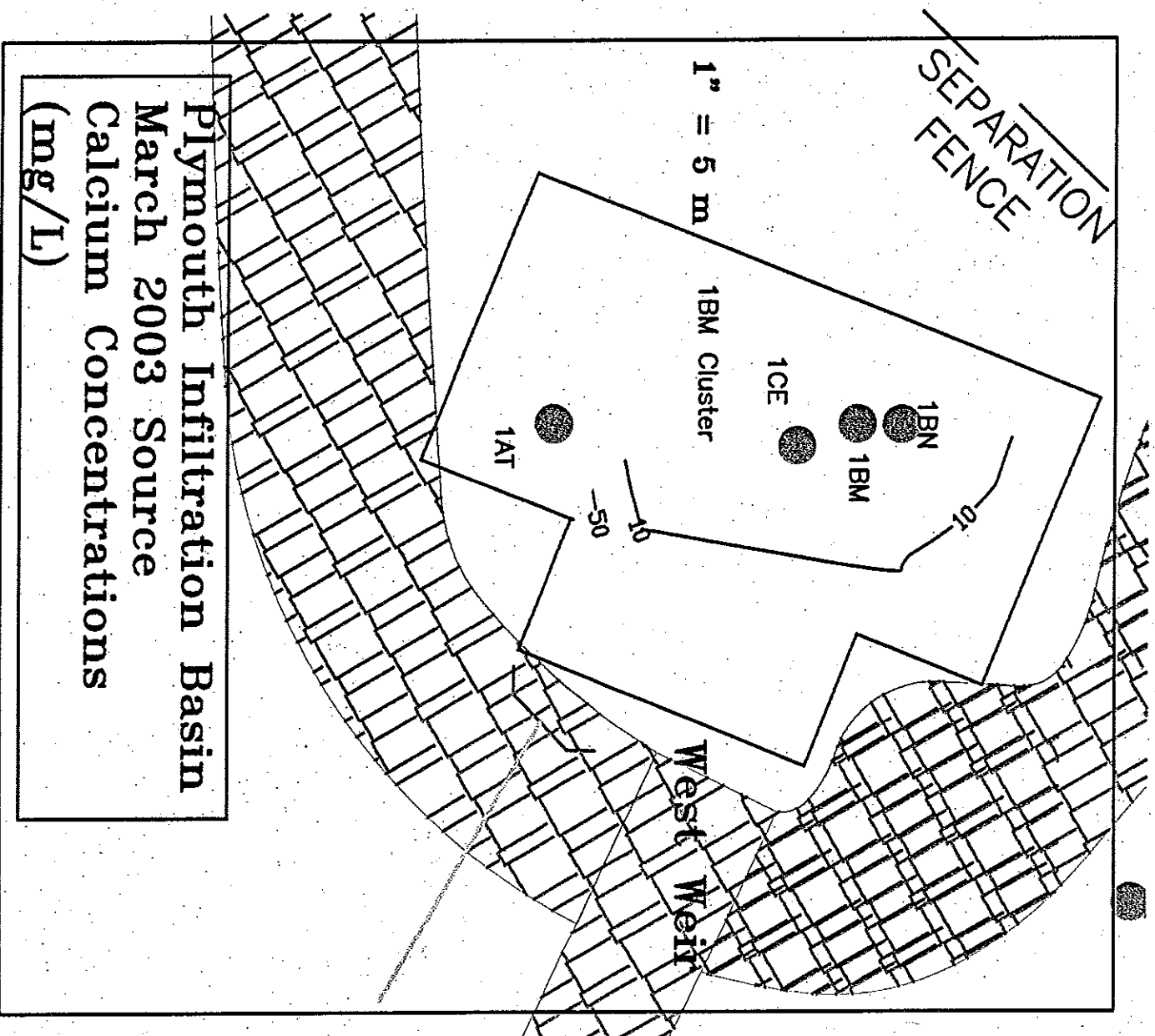
a

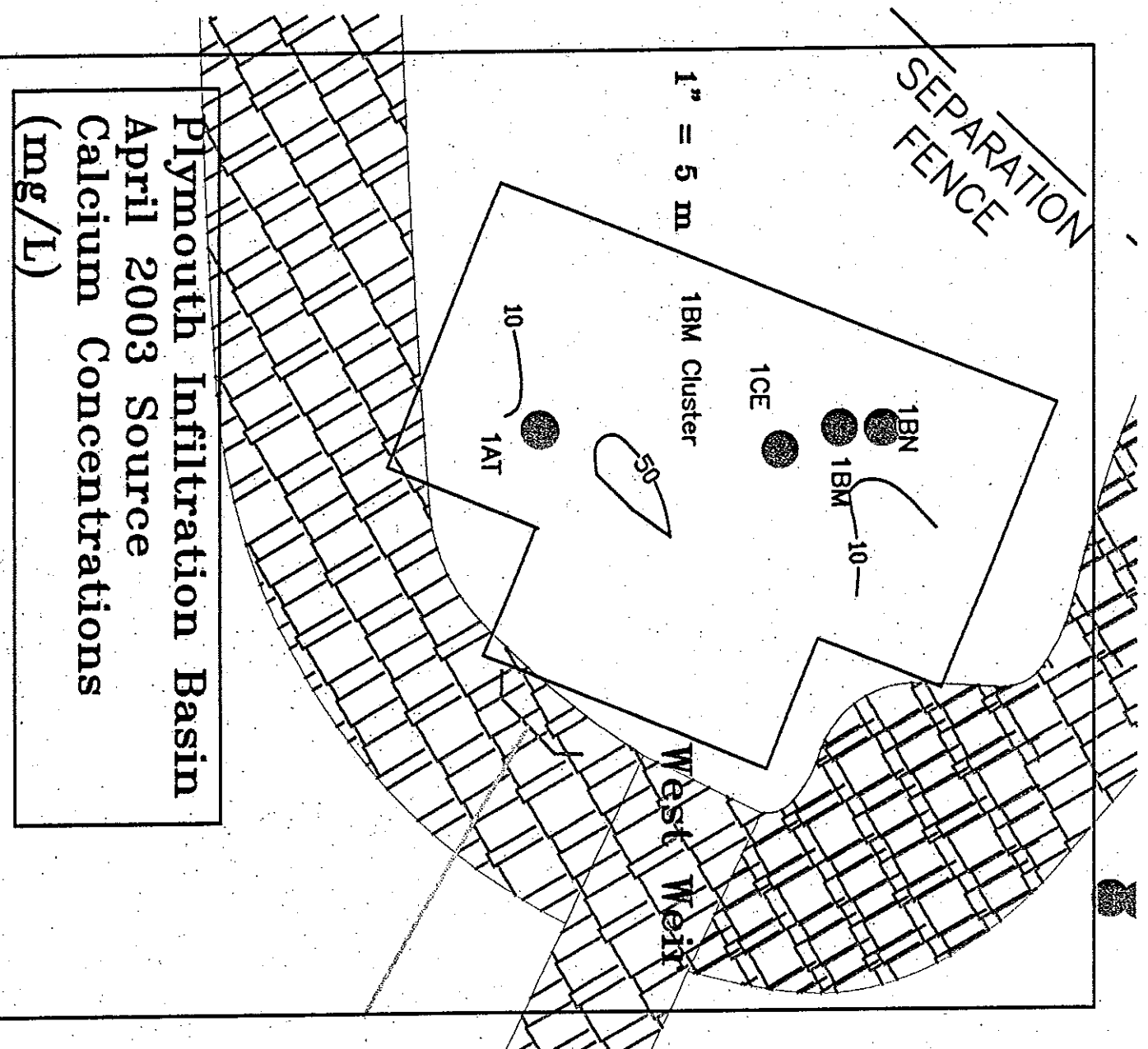


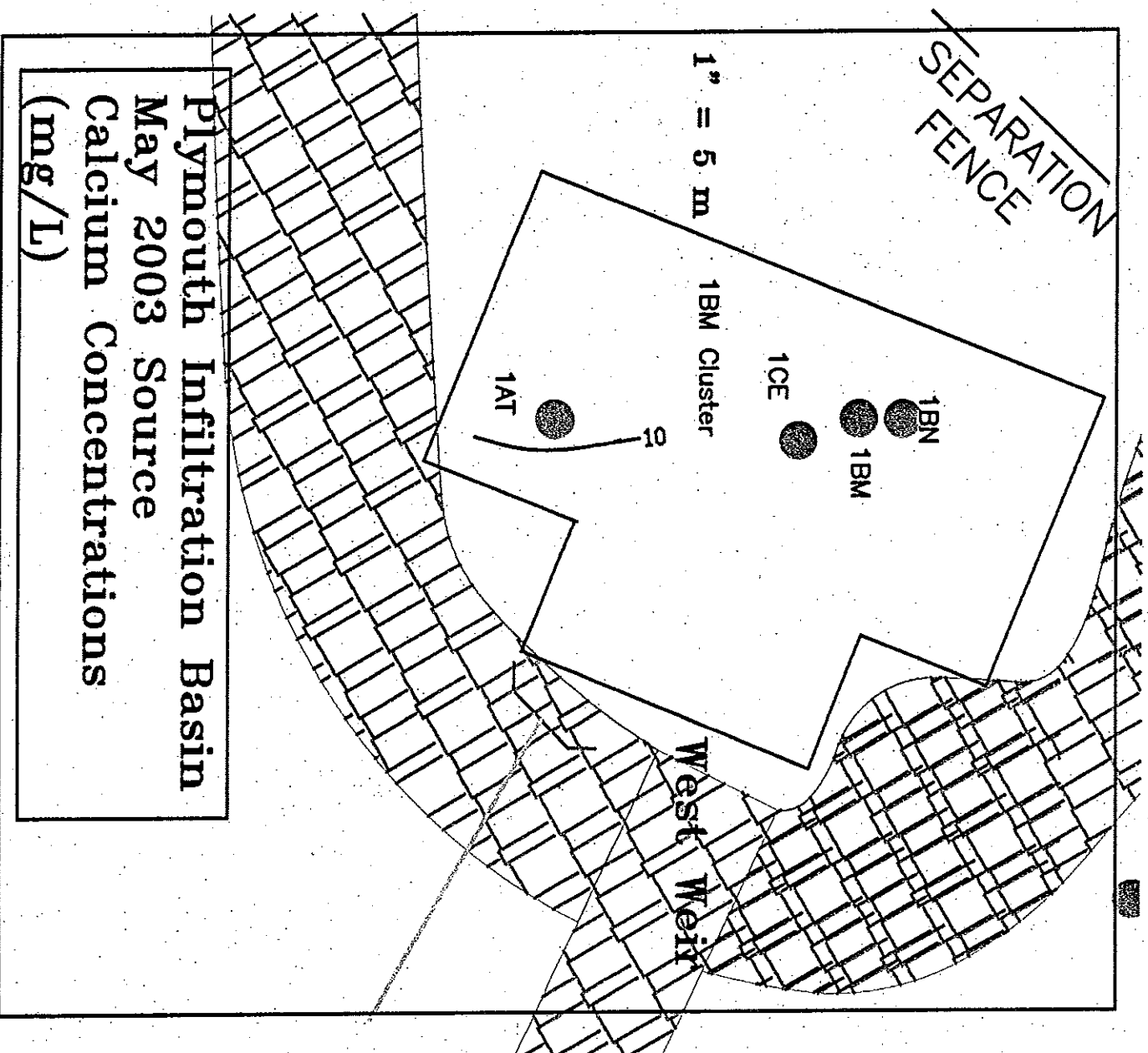




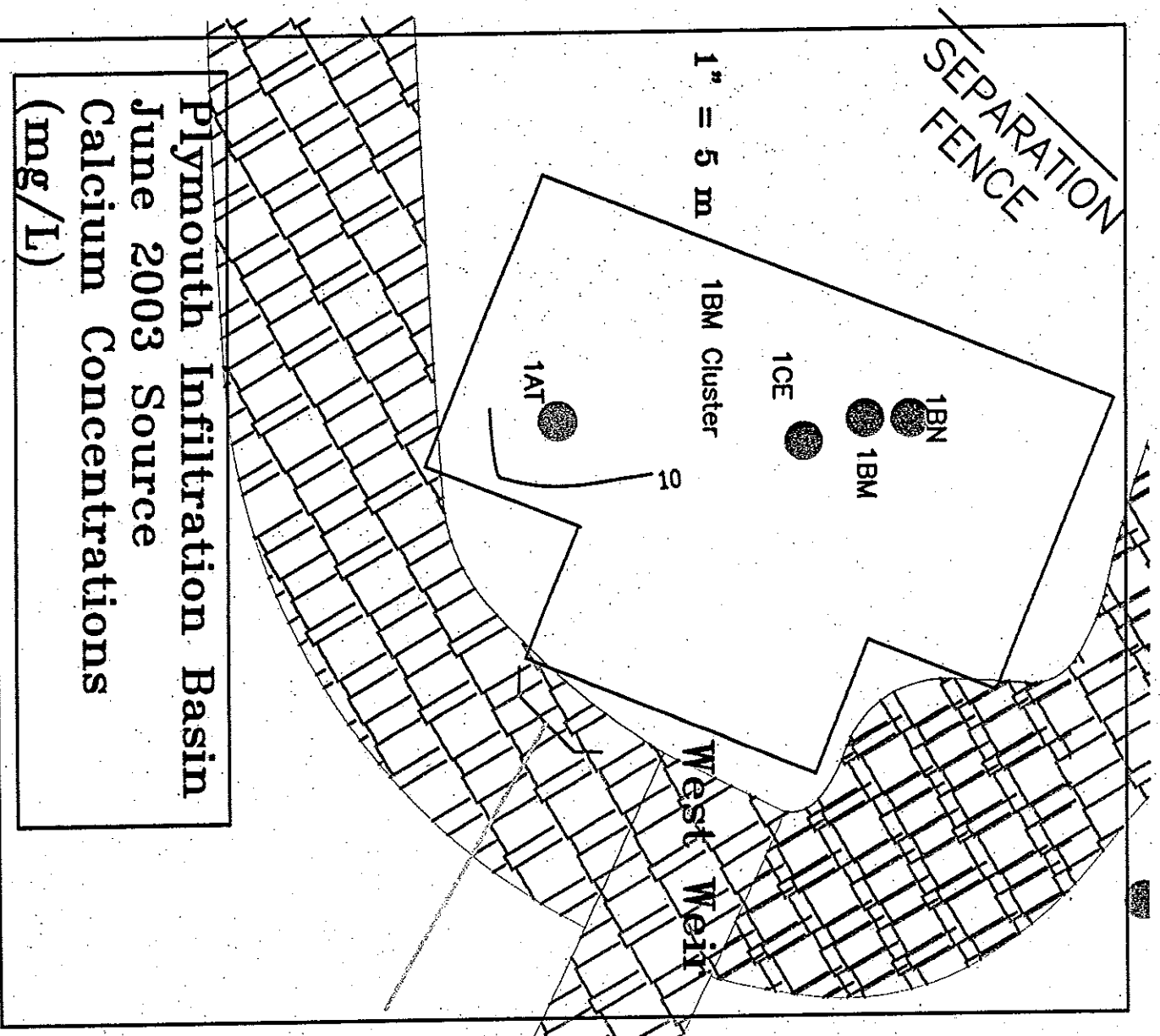


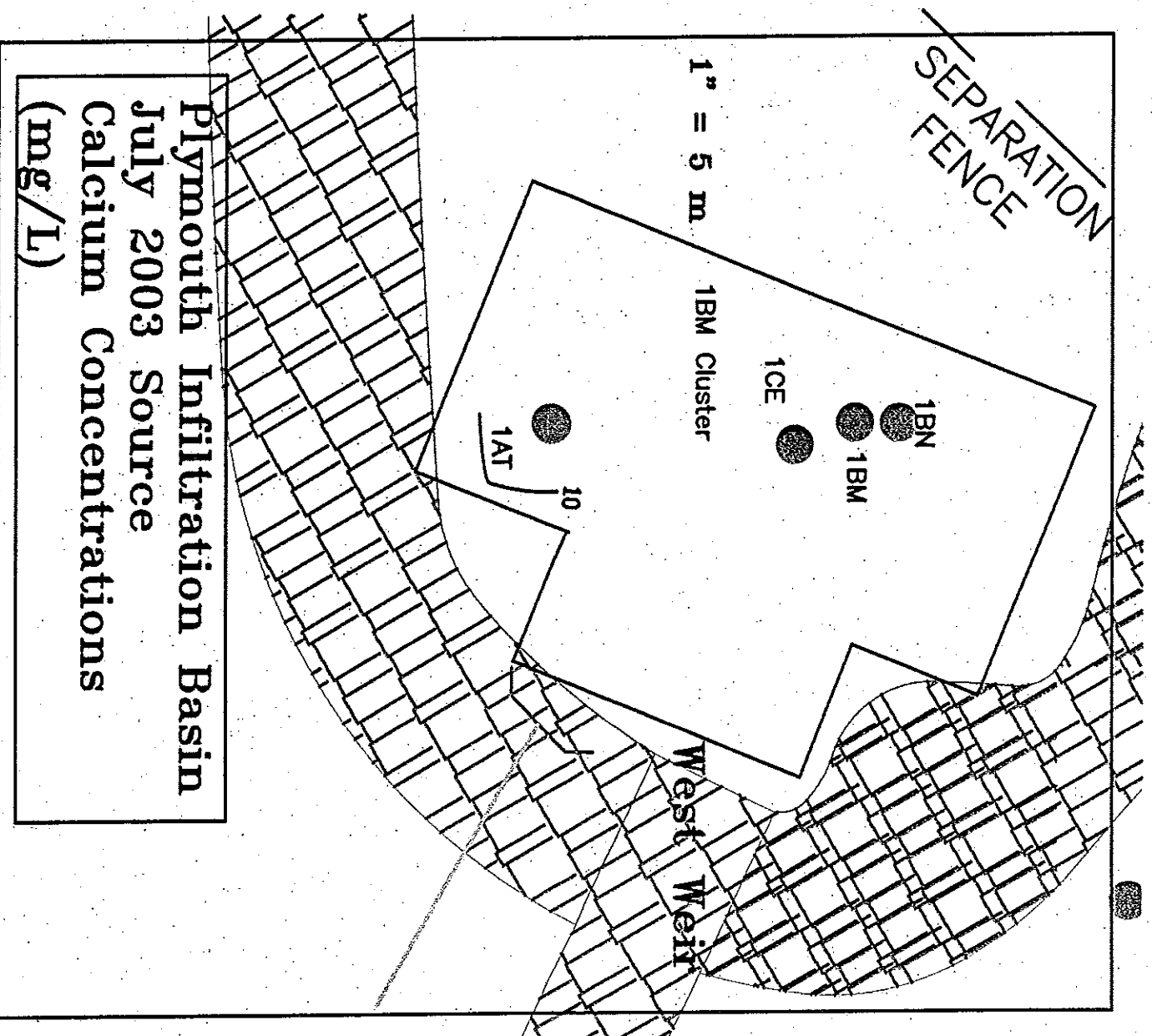


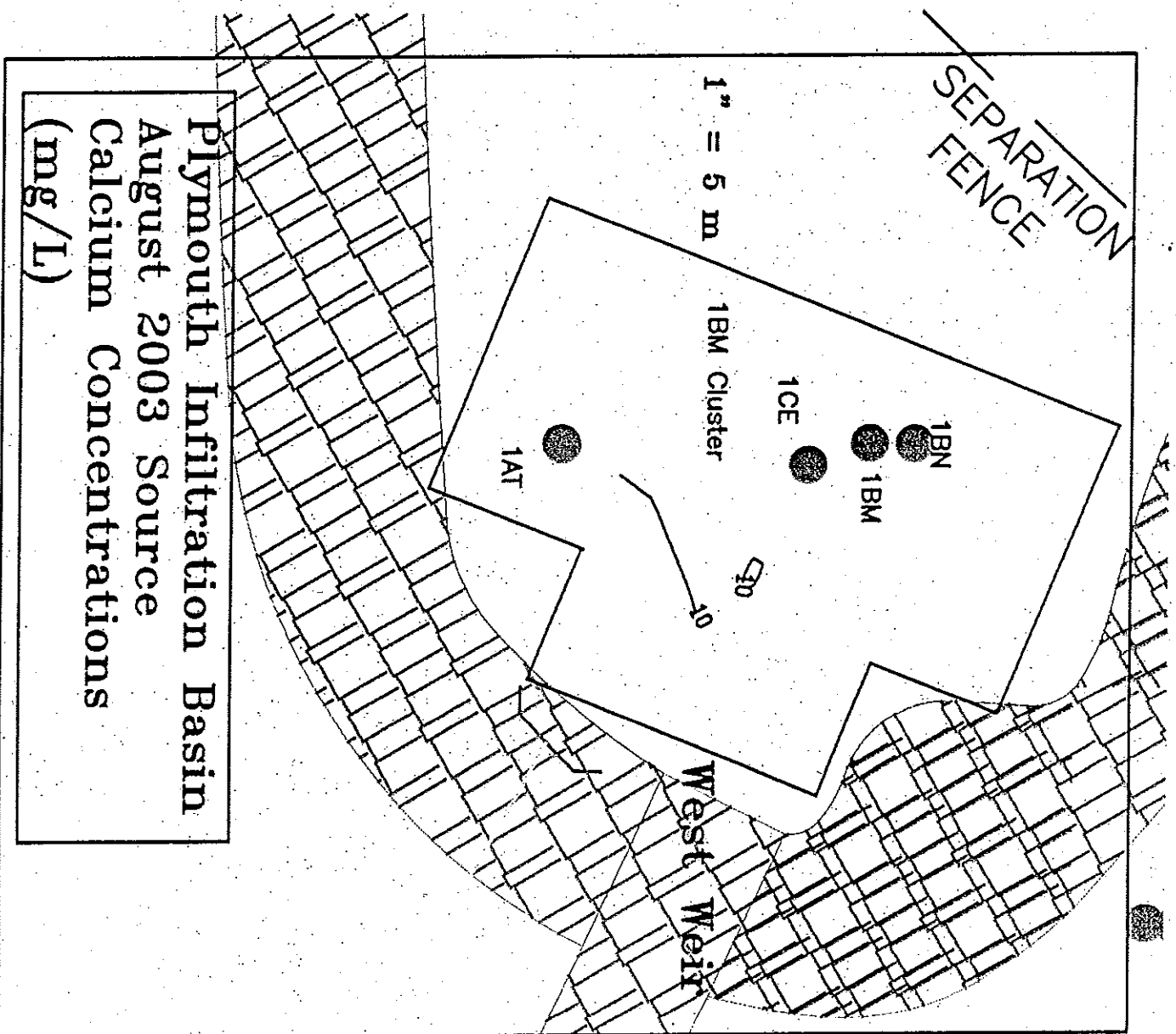


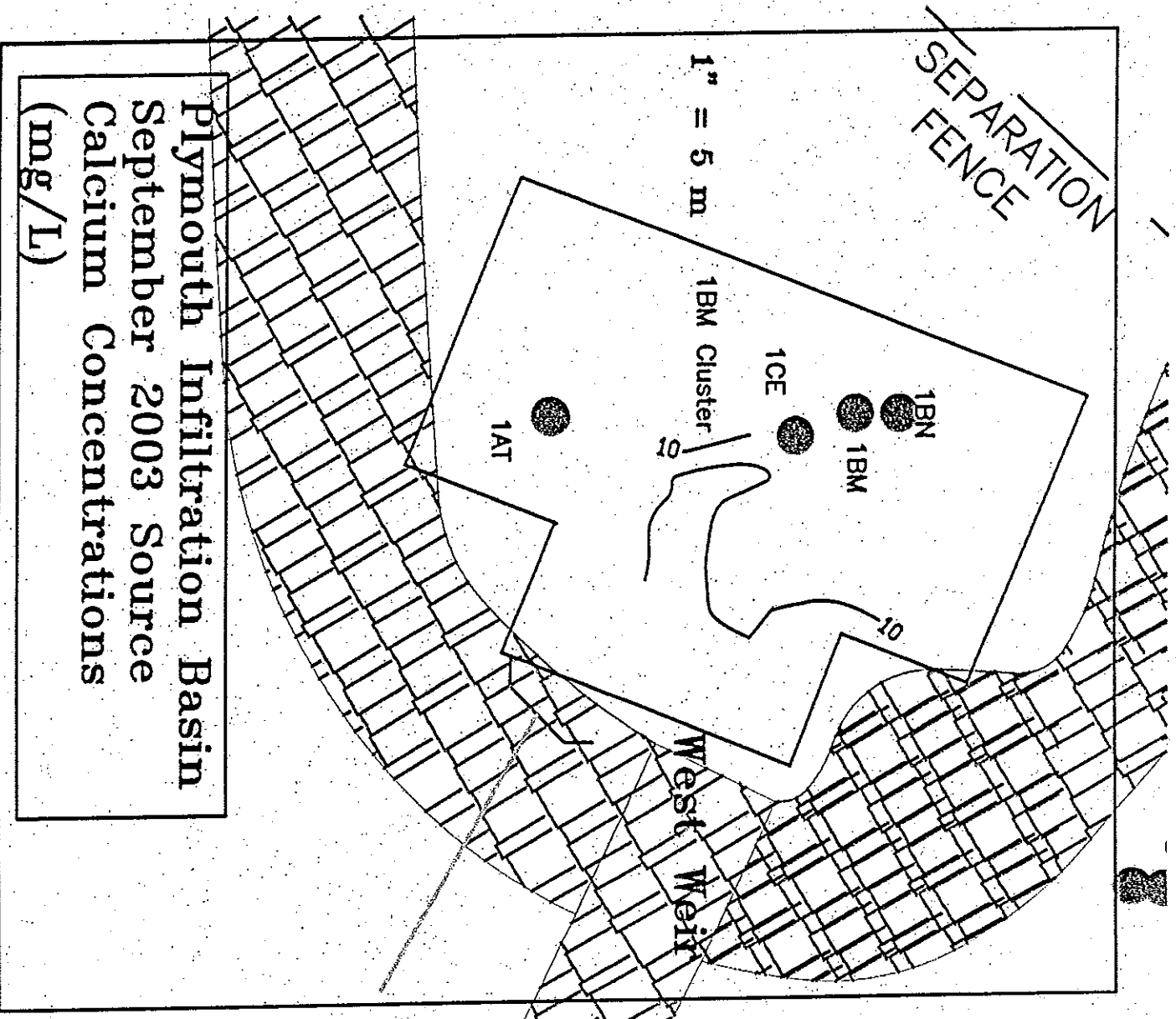


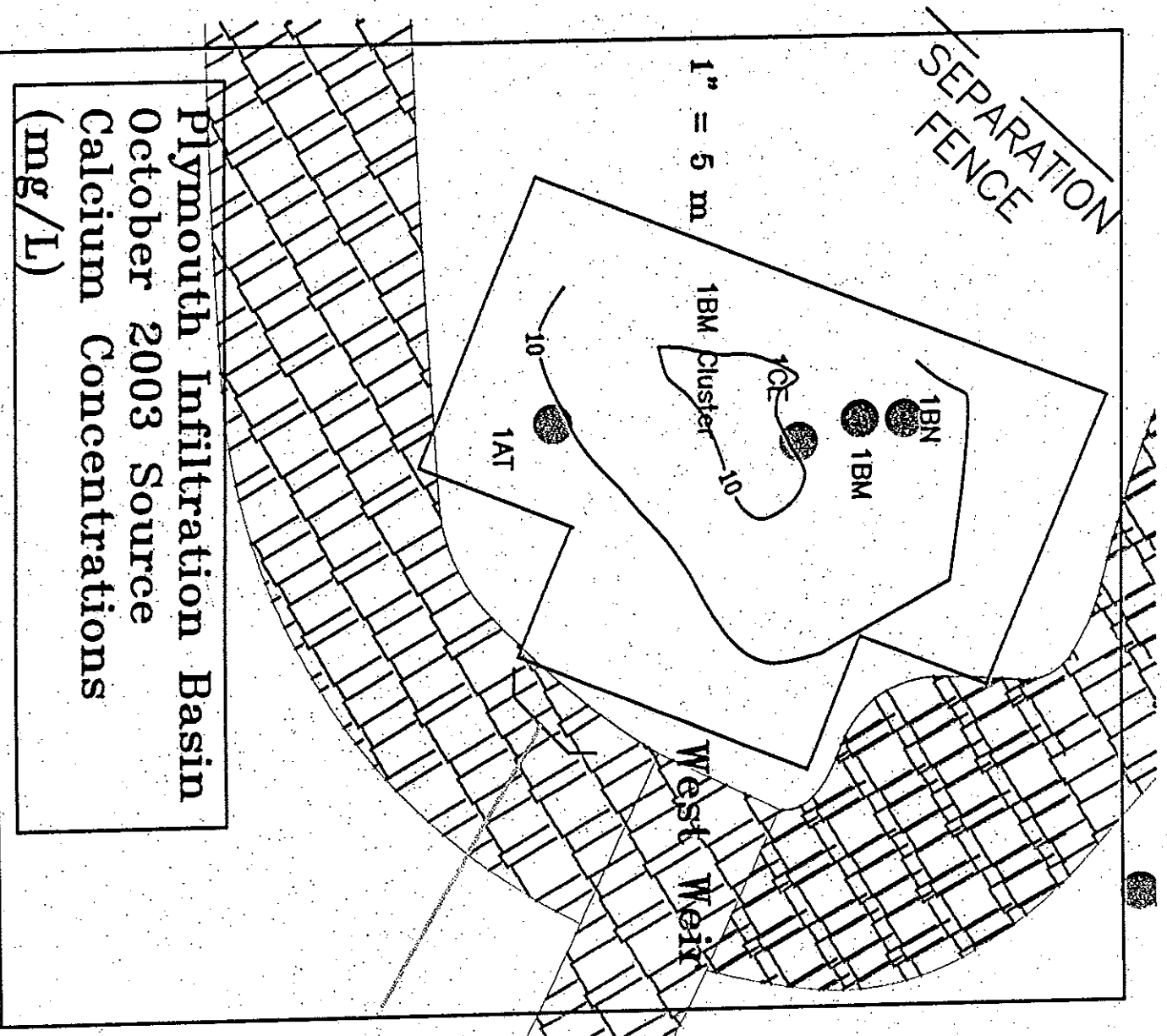
Plymouth Infiltration Basin
May 2003 Source
Calcium Concentrations
(mg/L)

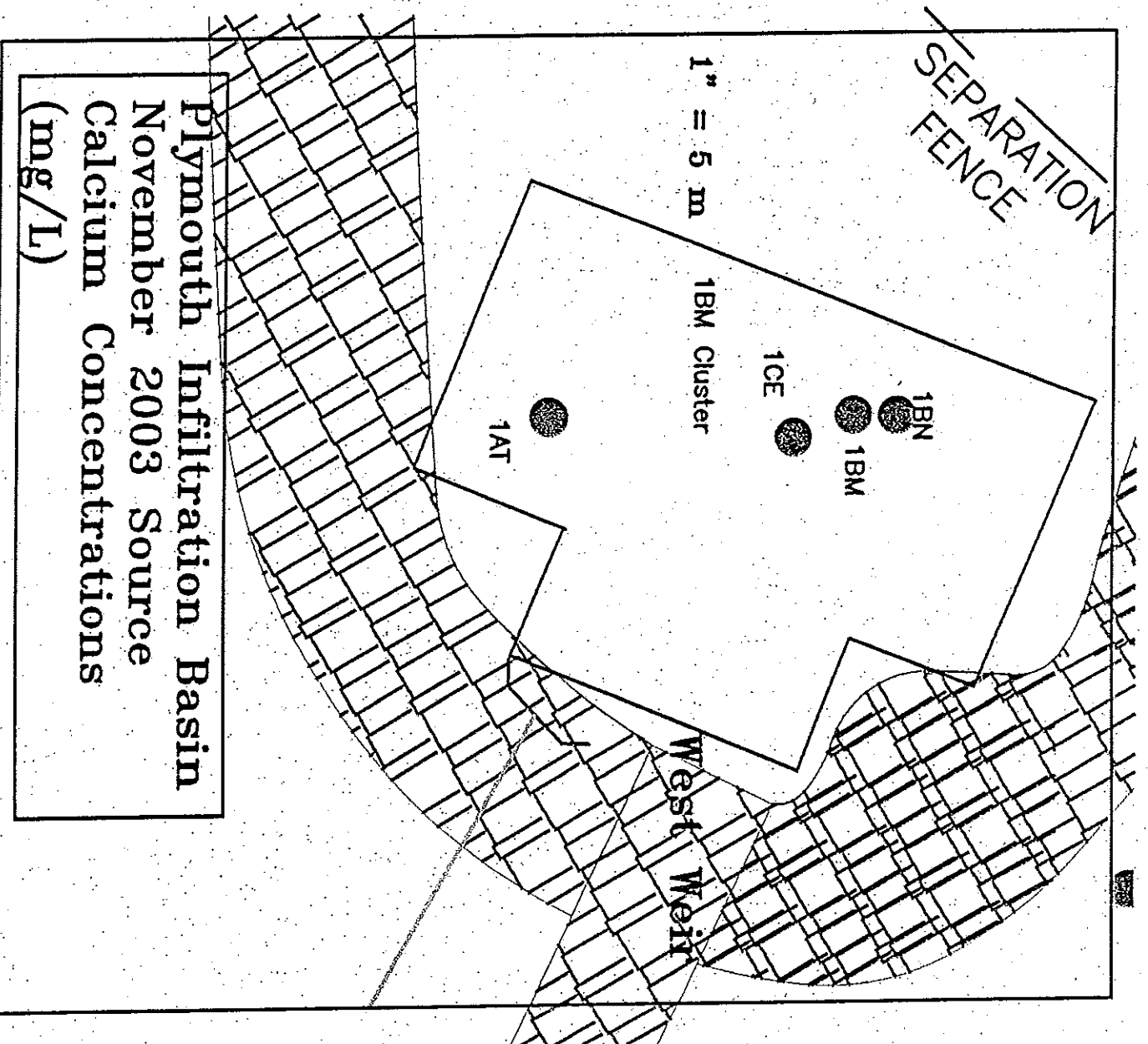


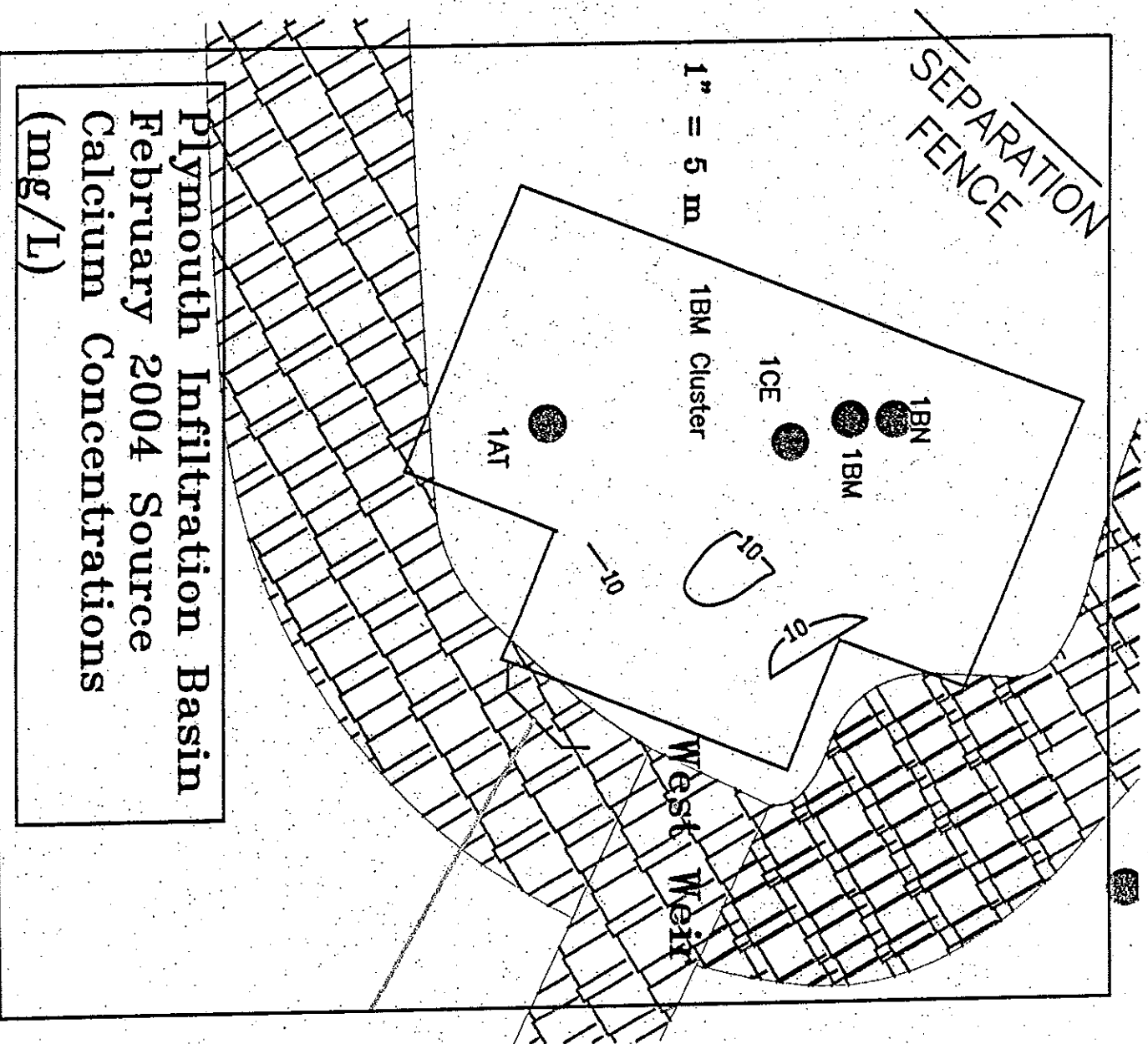


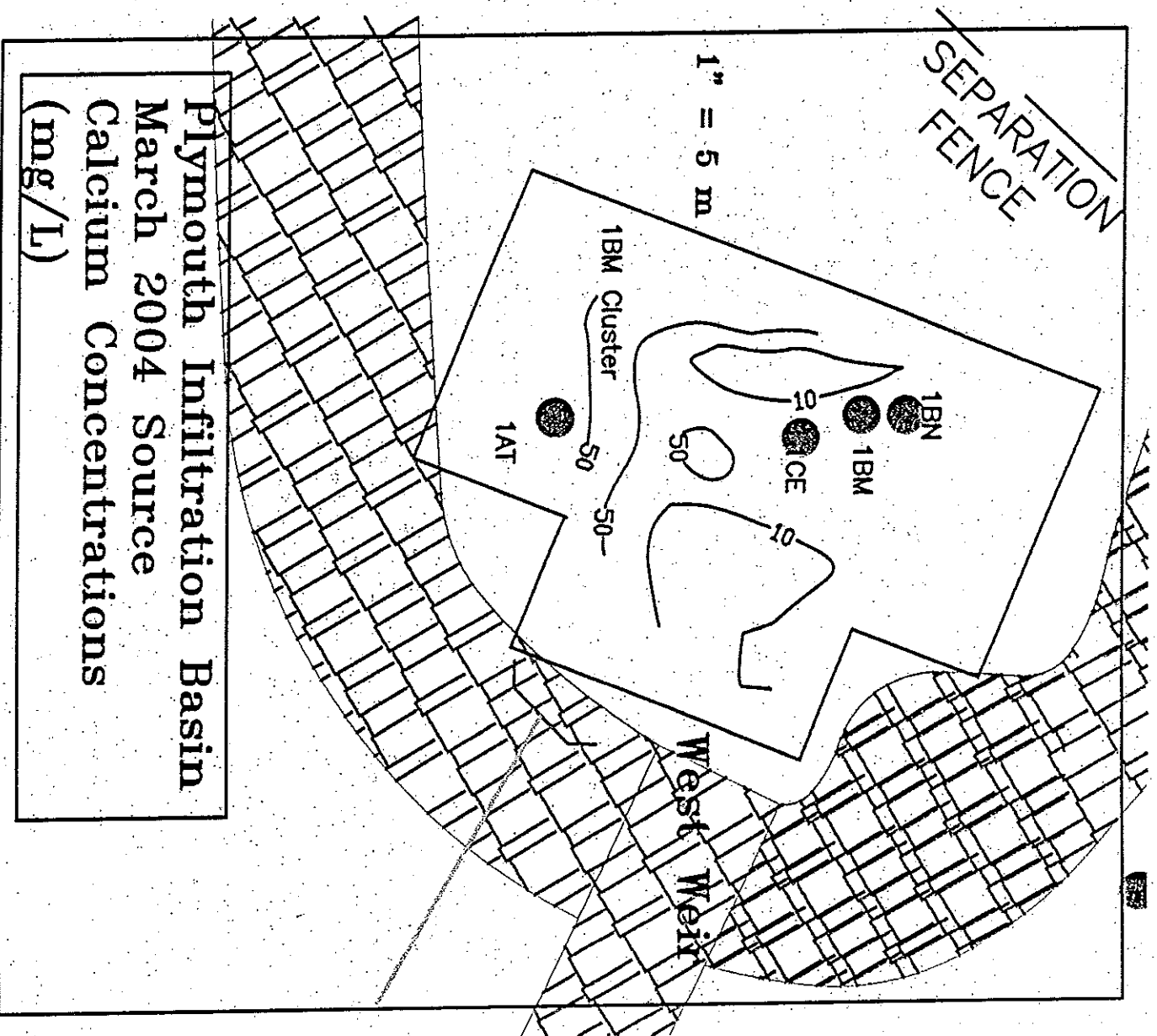


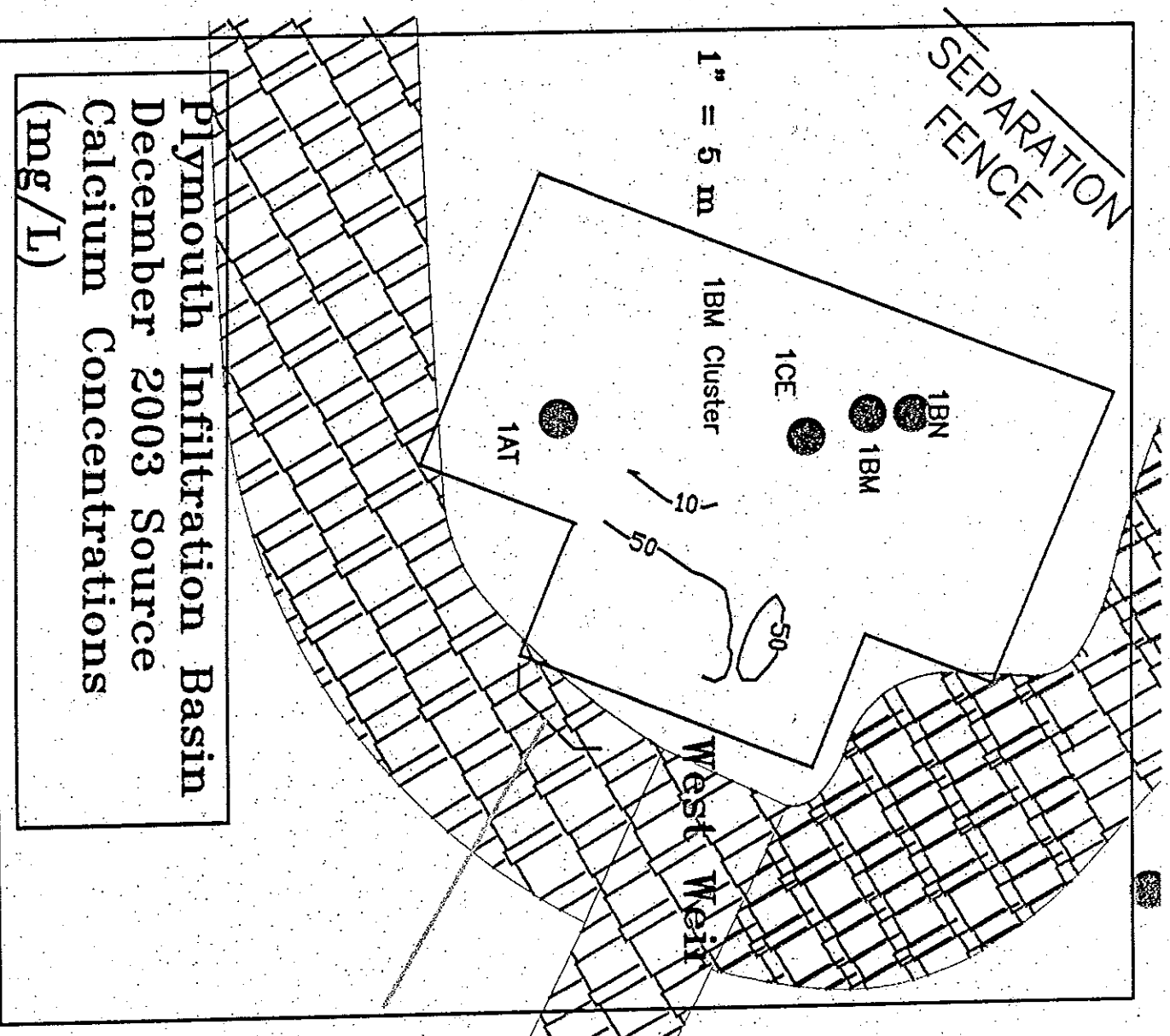


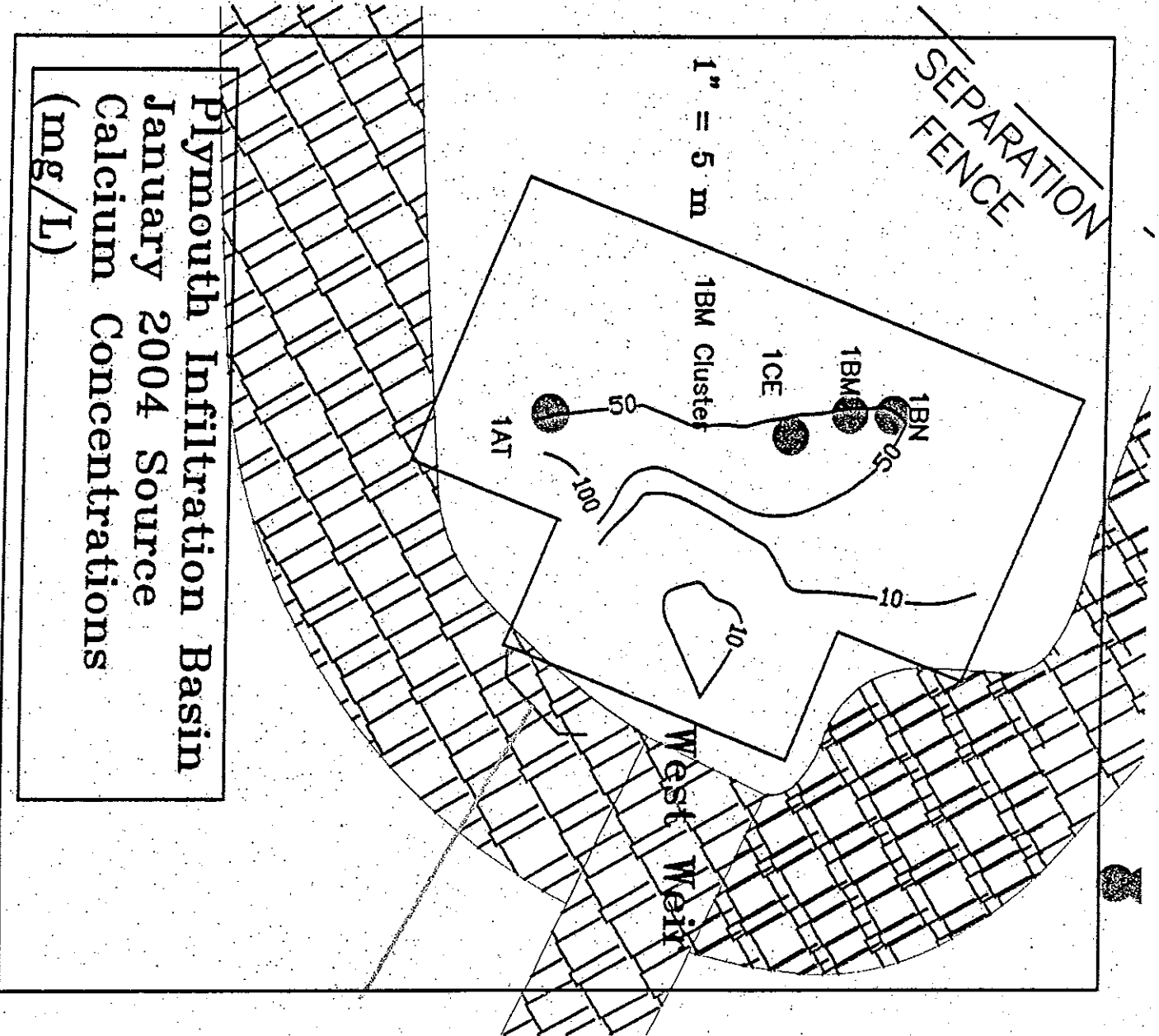


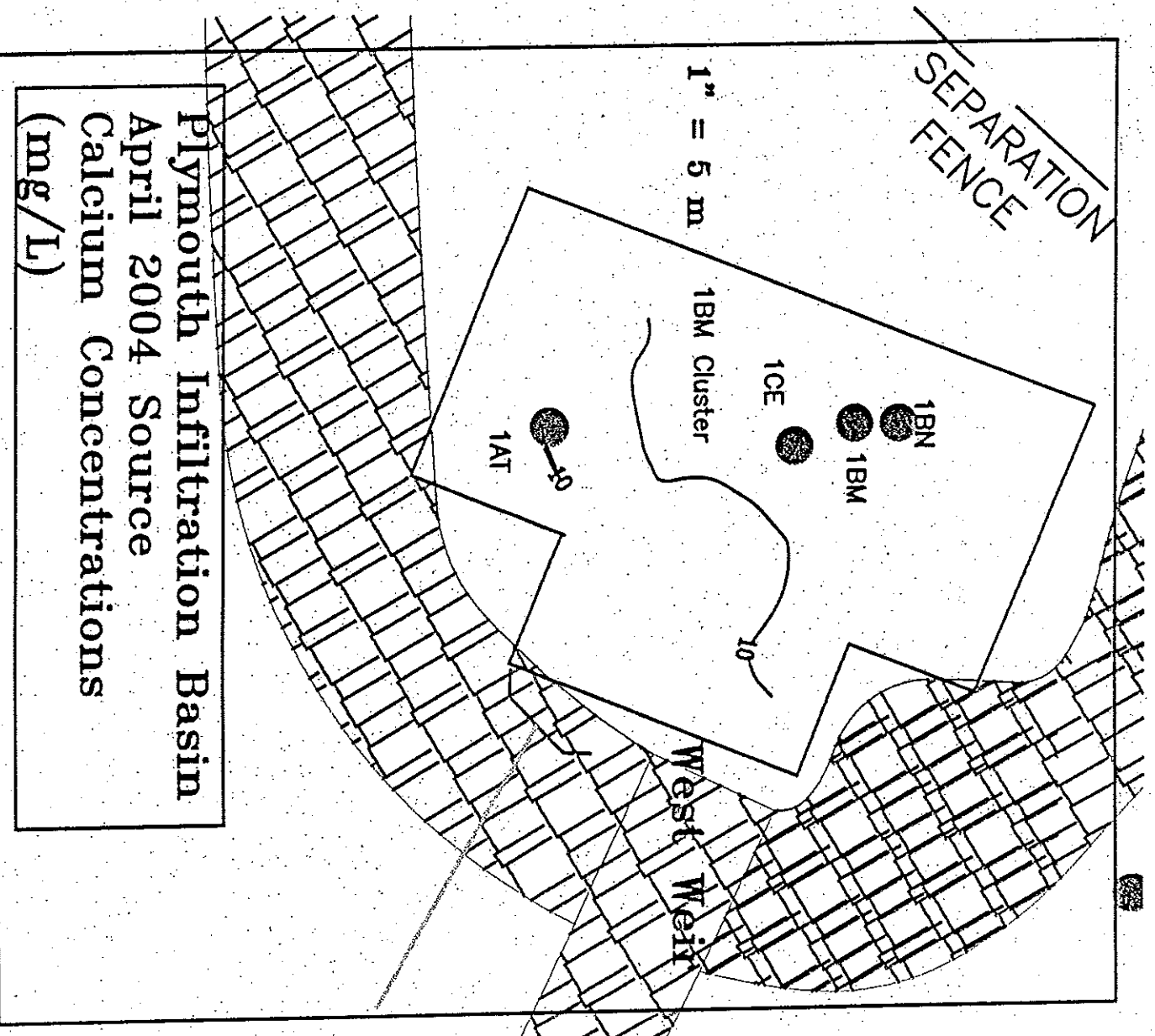


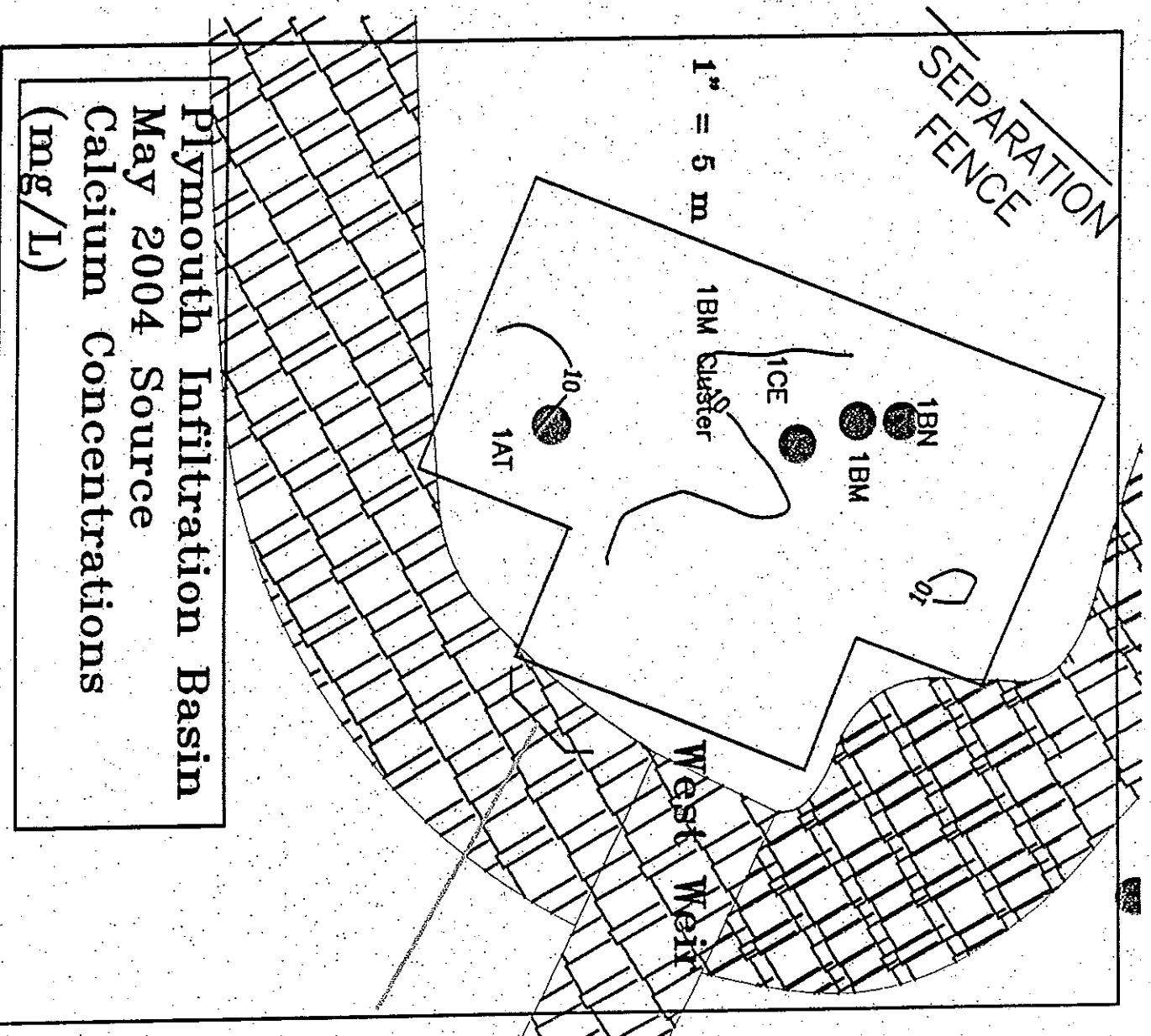




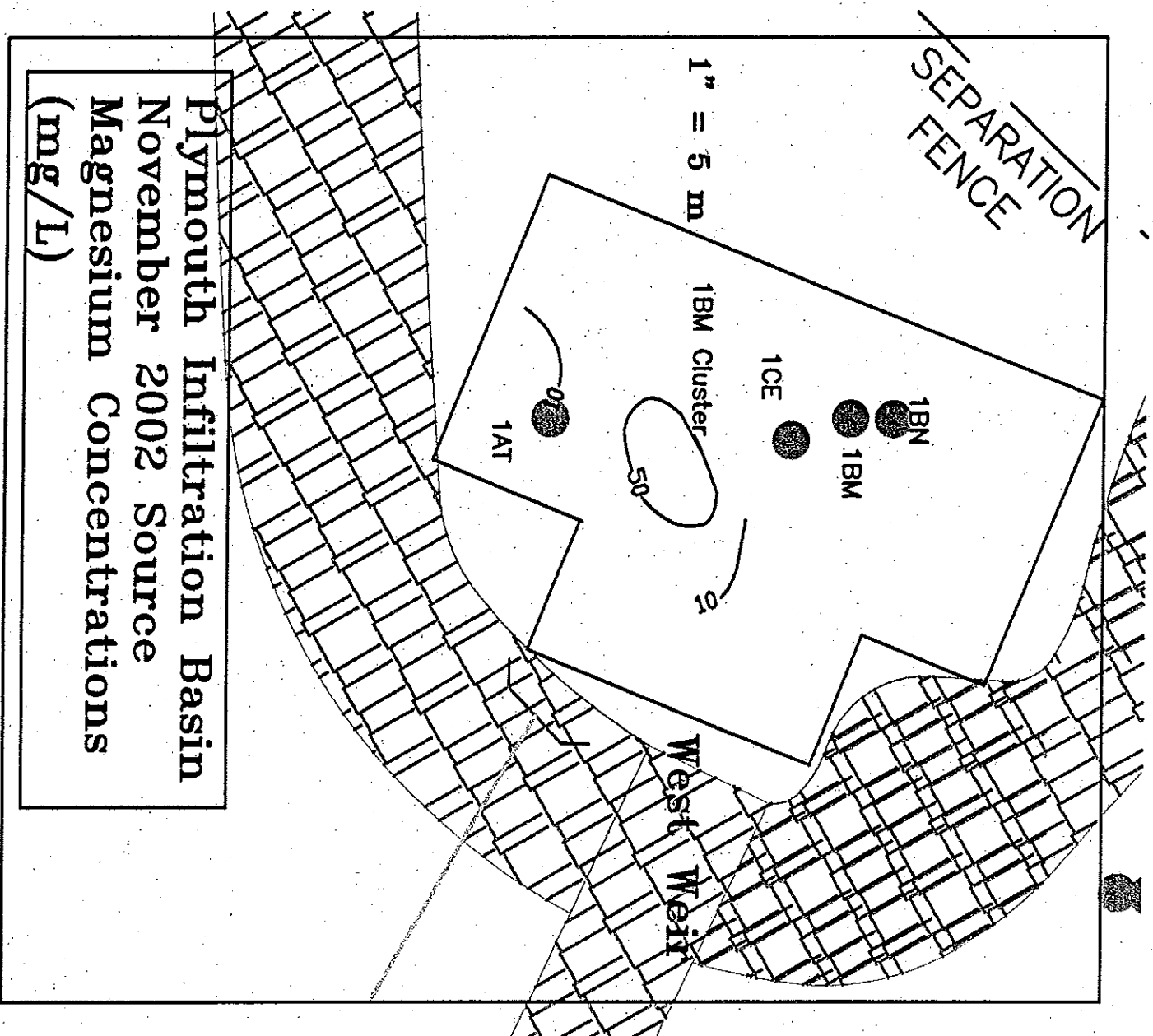


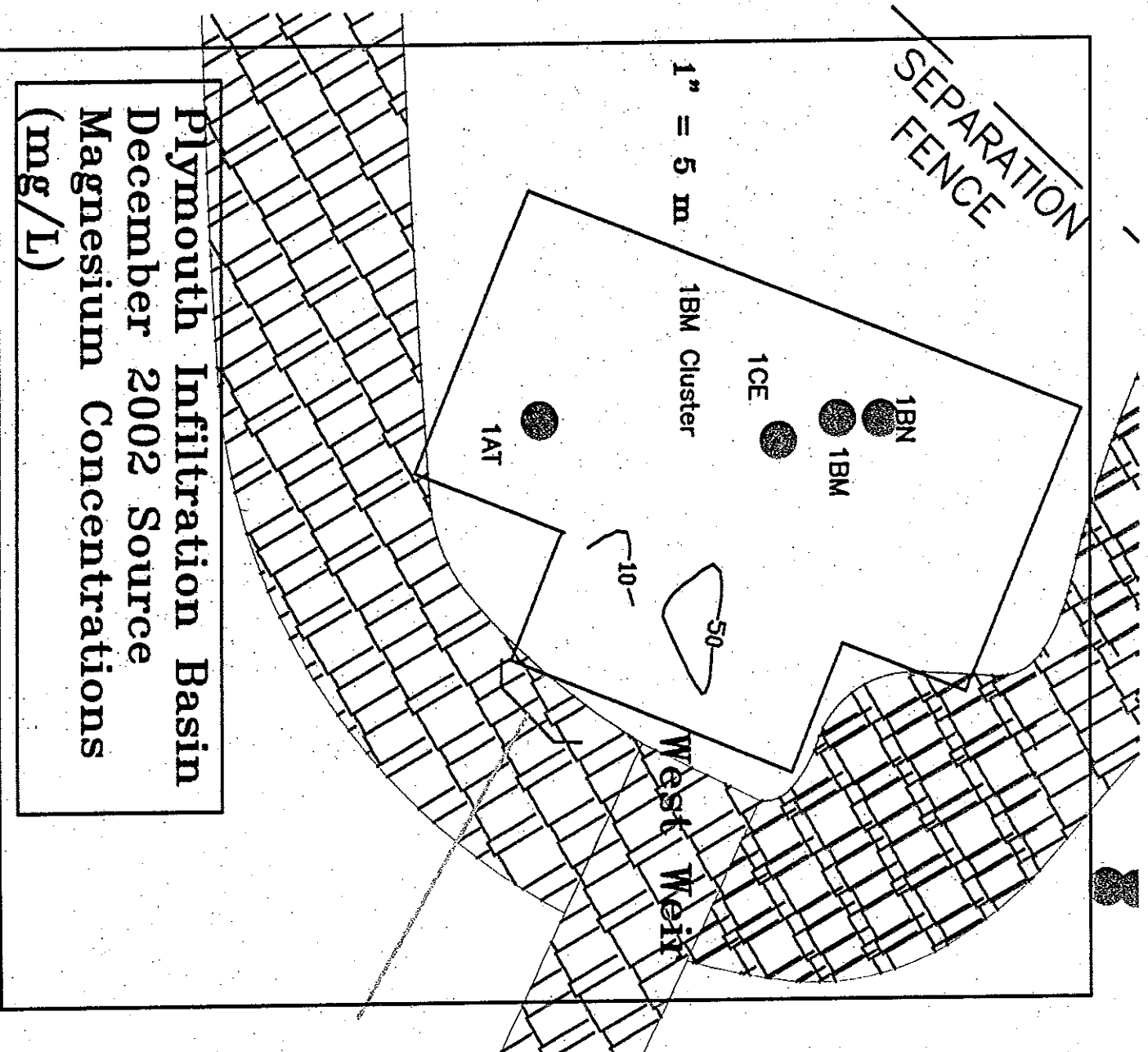


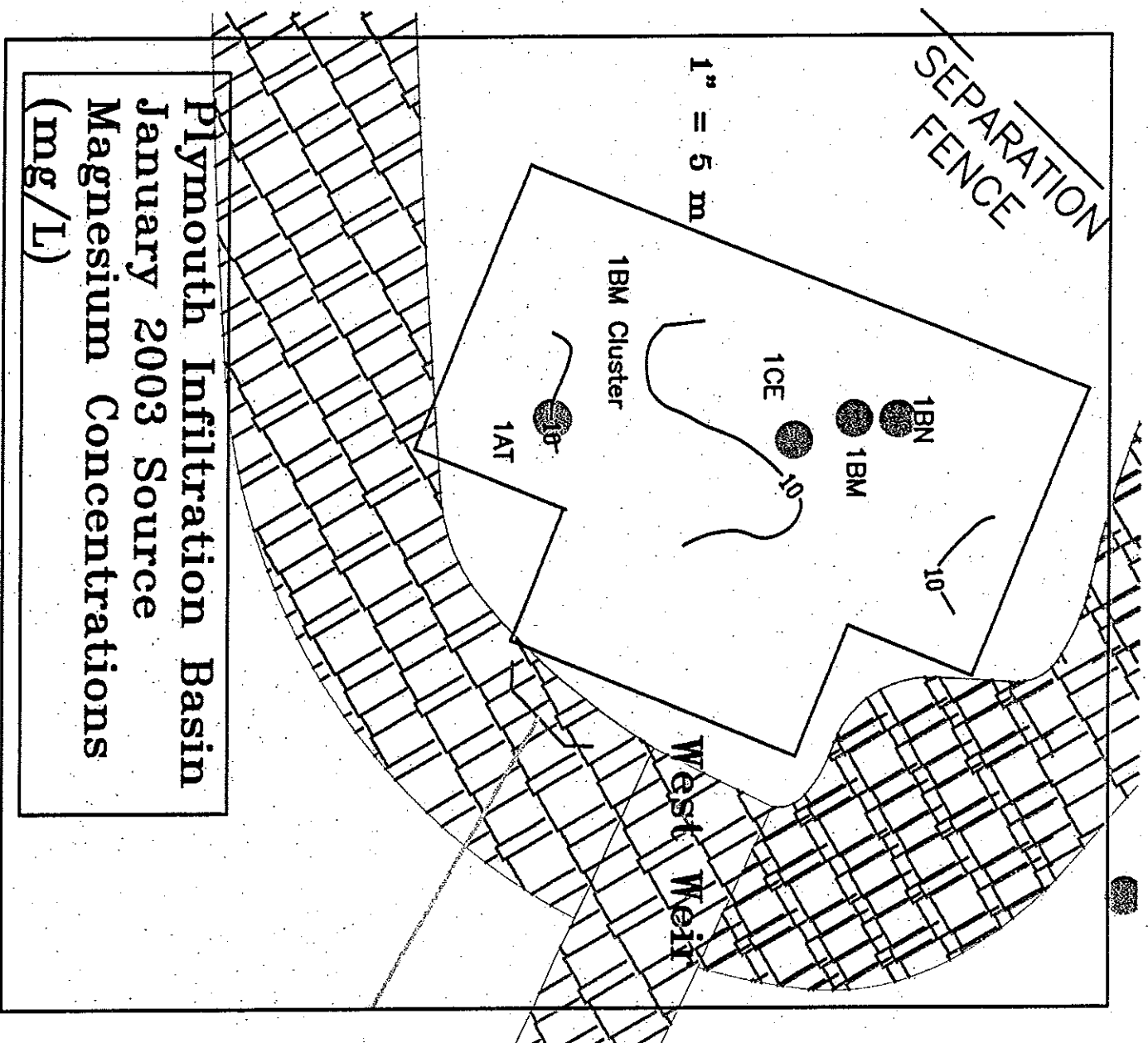


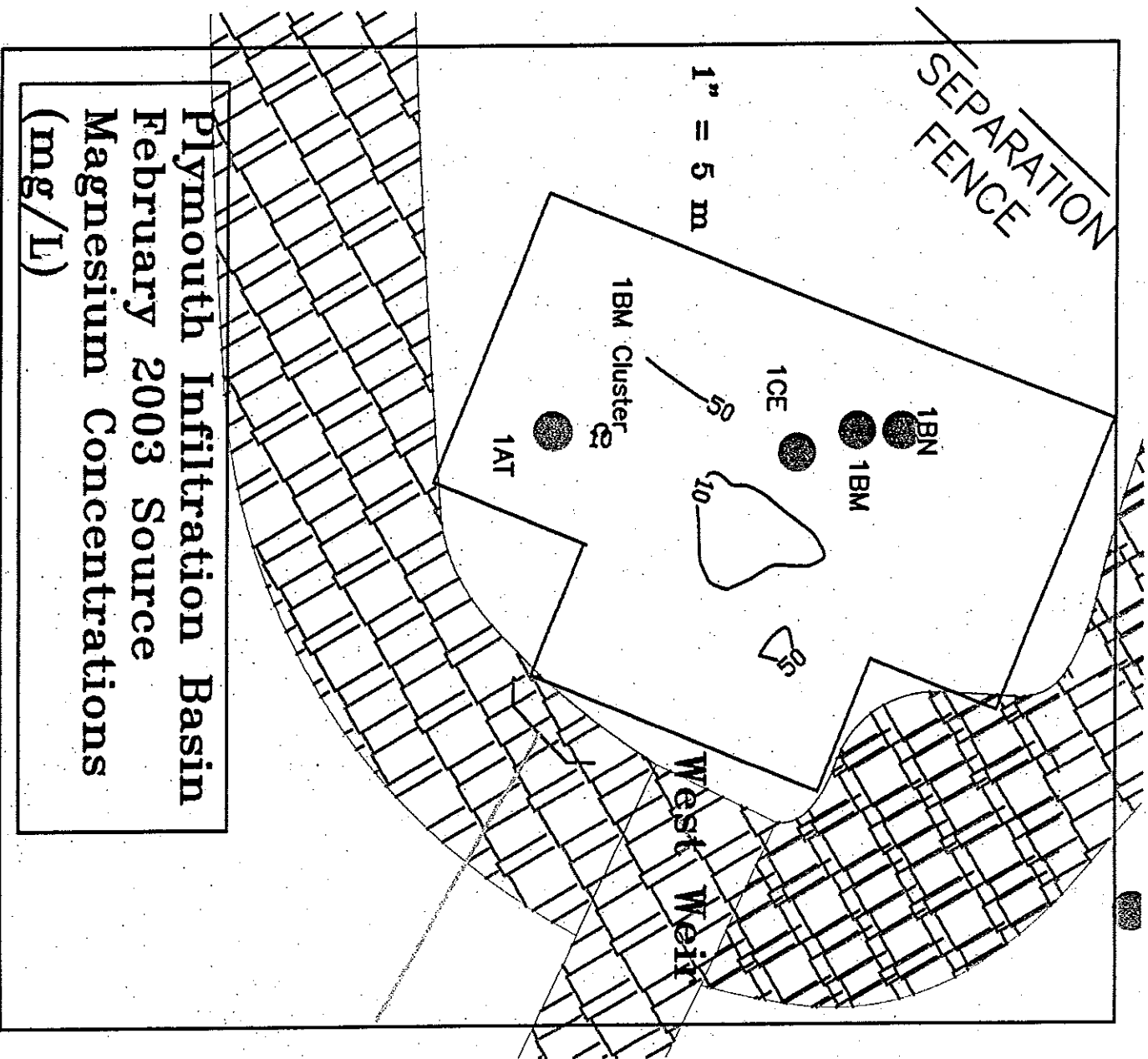


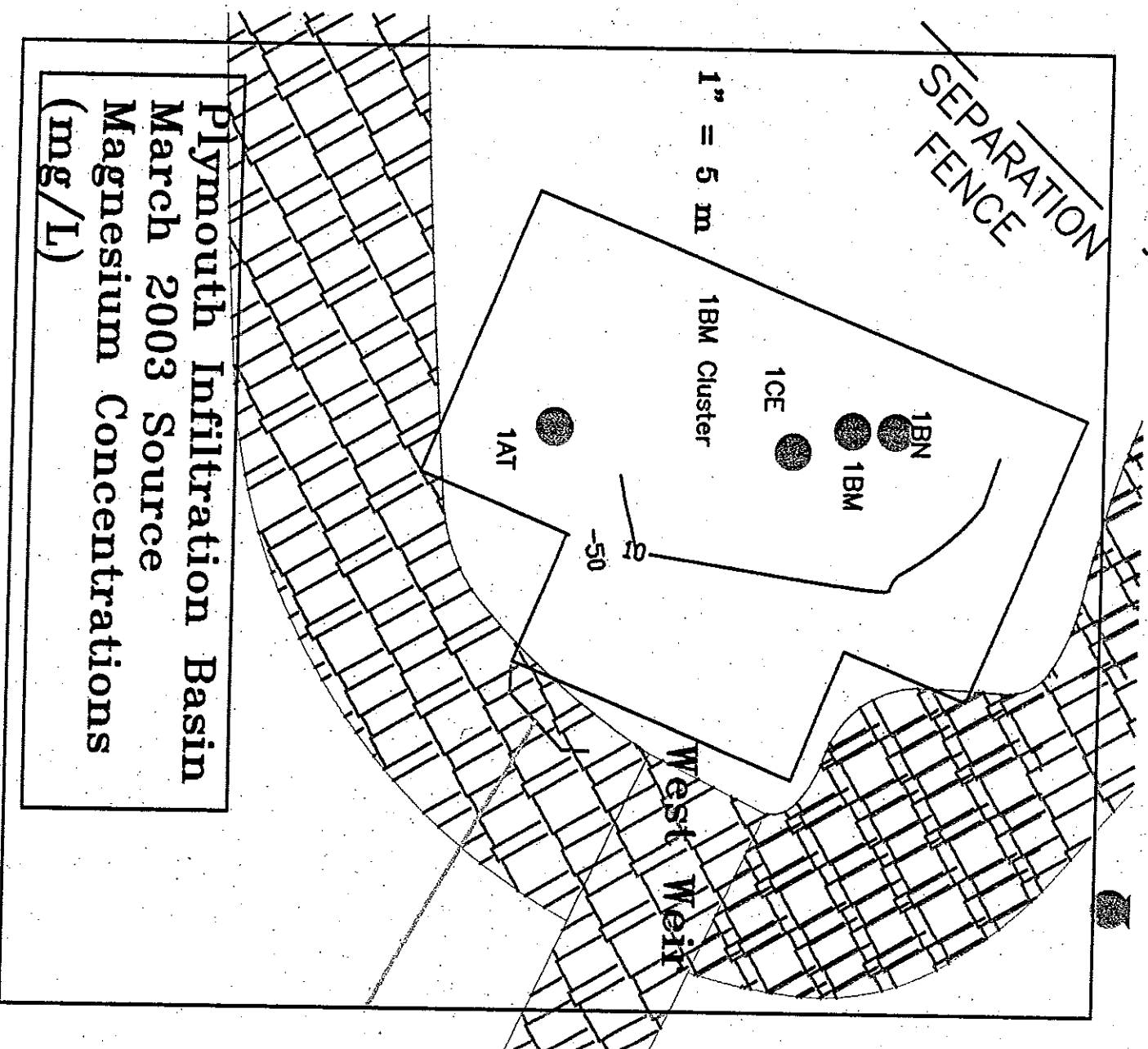
APPENDIX L
Magnesium Source Isopleths, November 2002 – May 2004

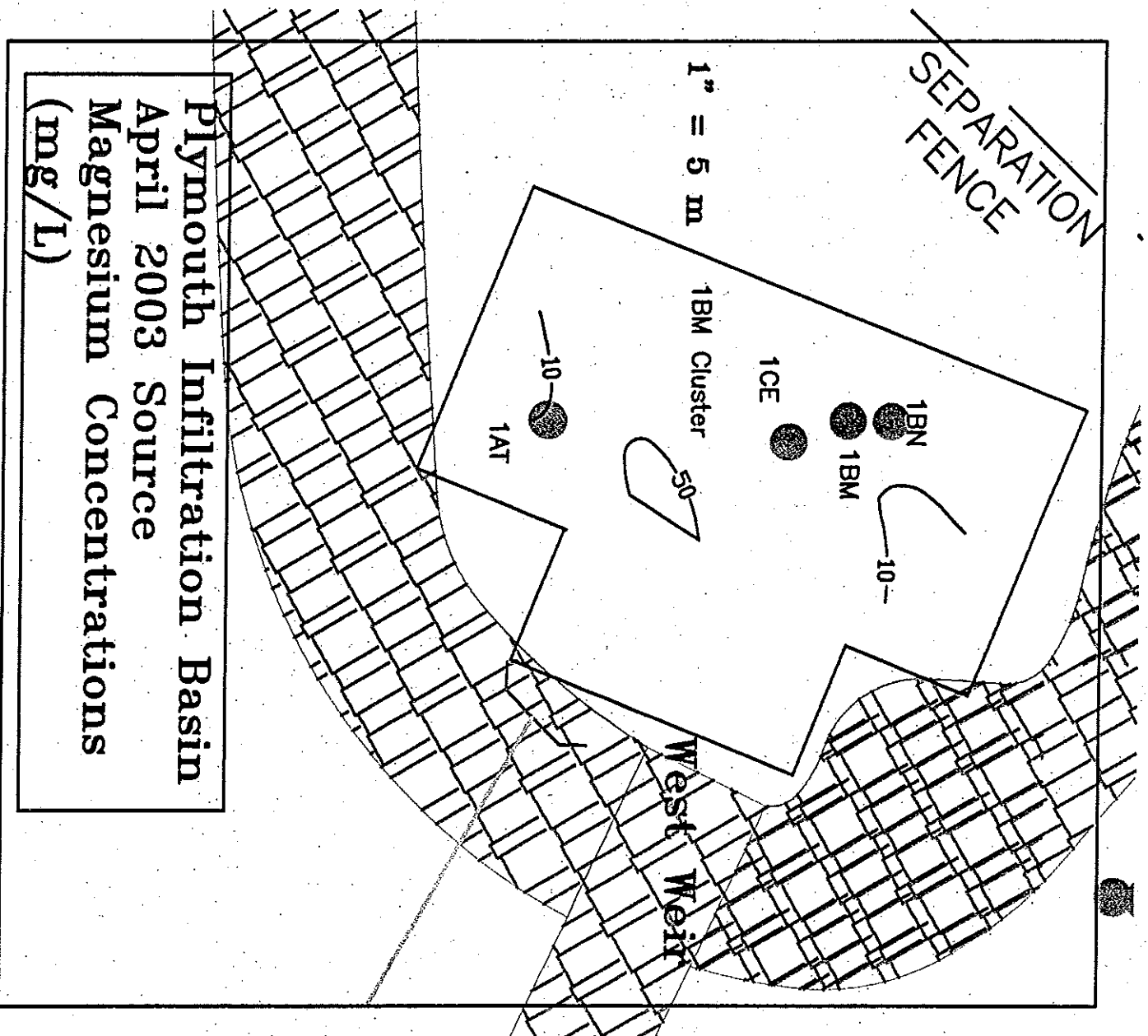


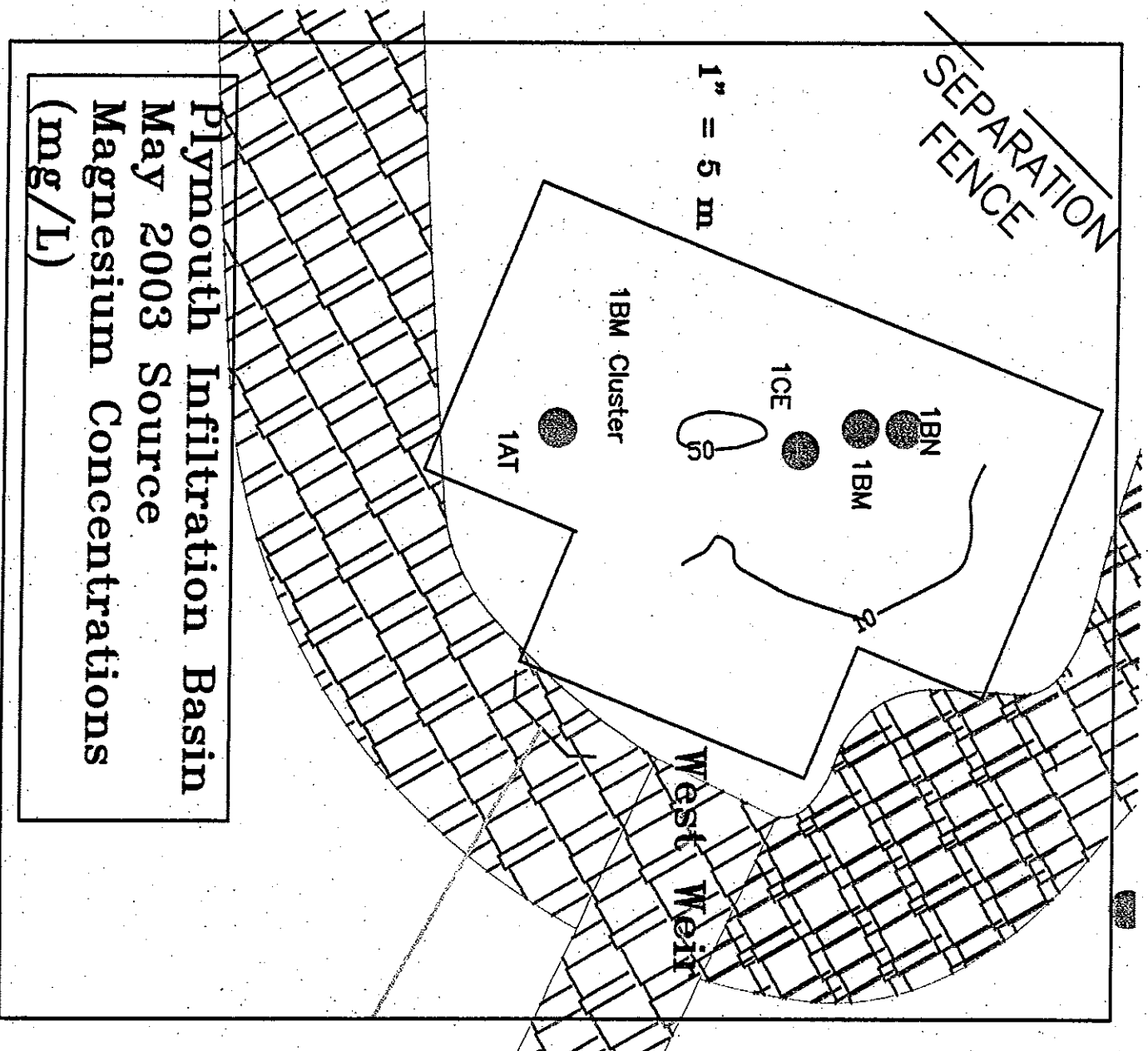


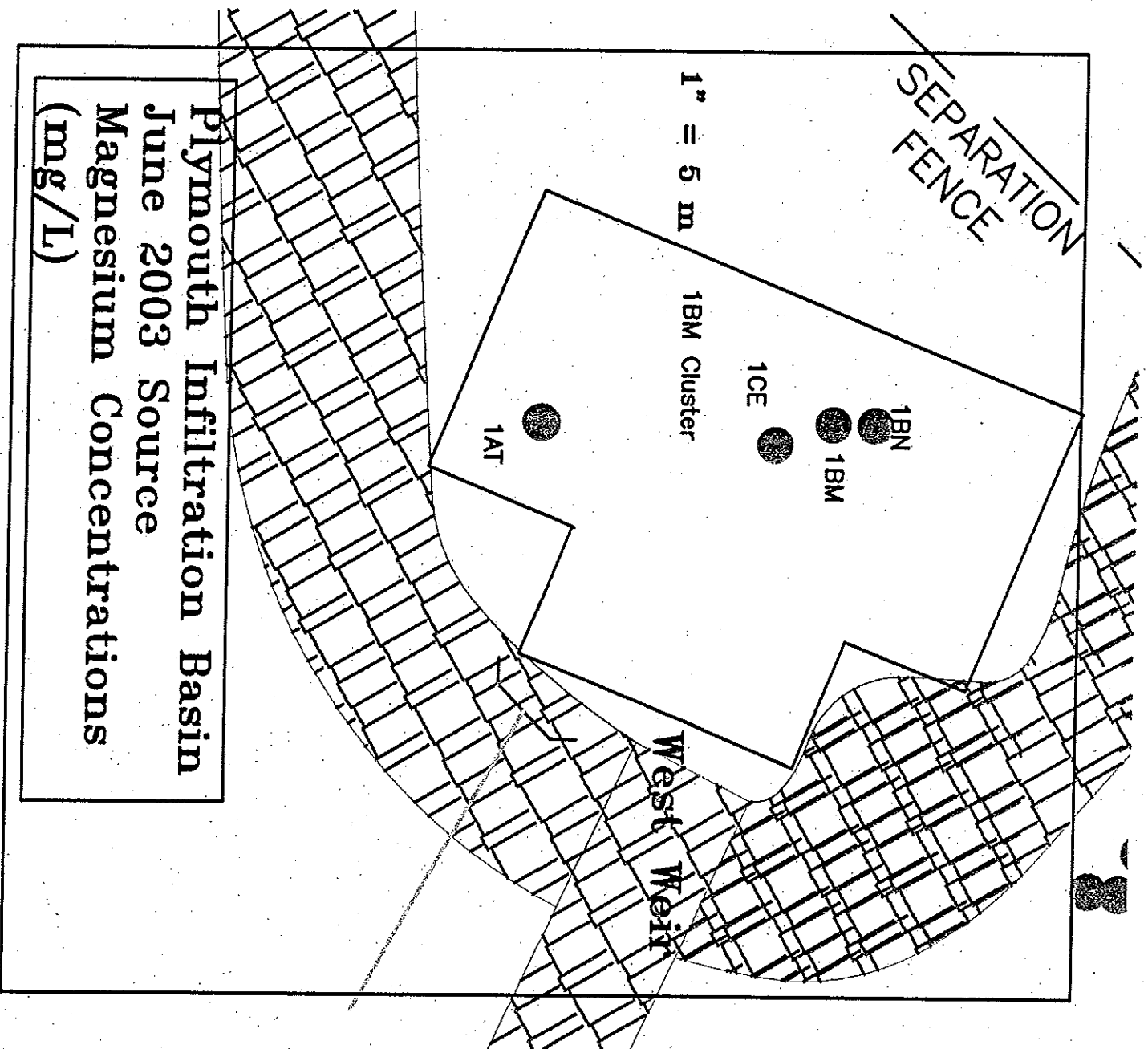


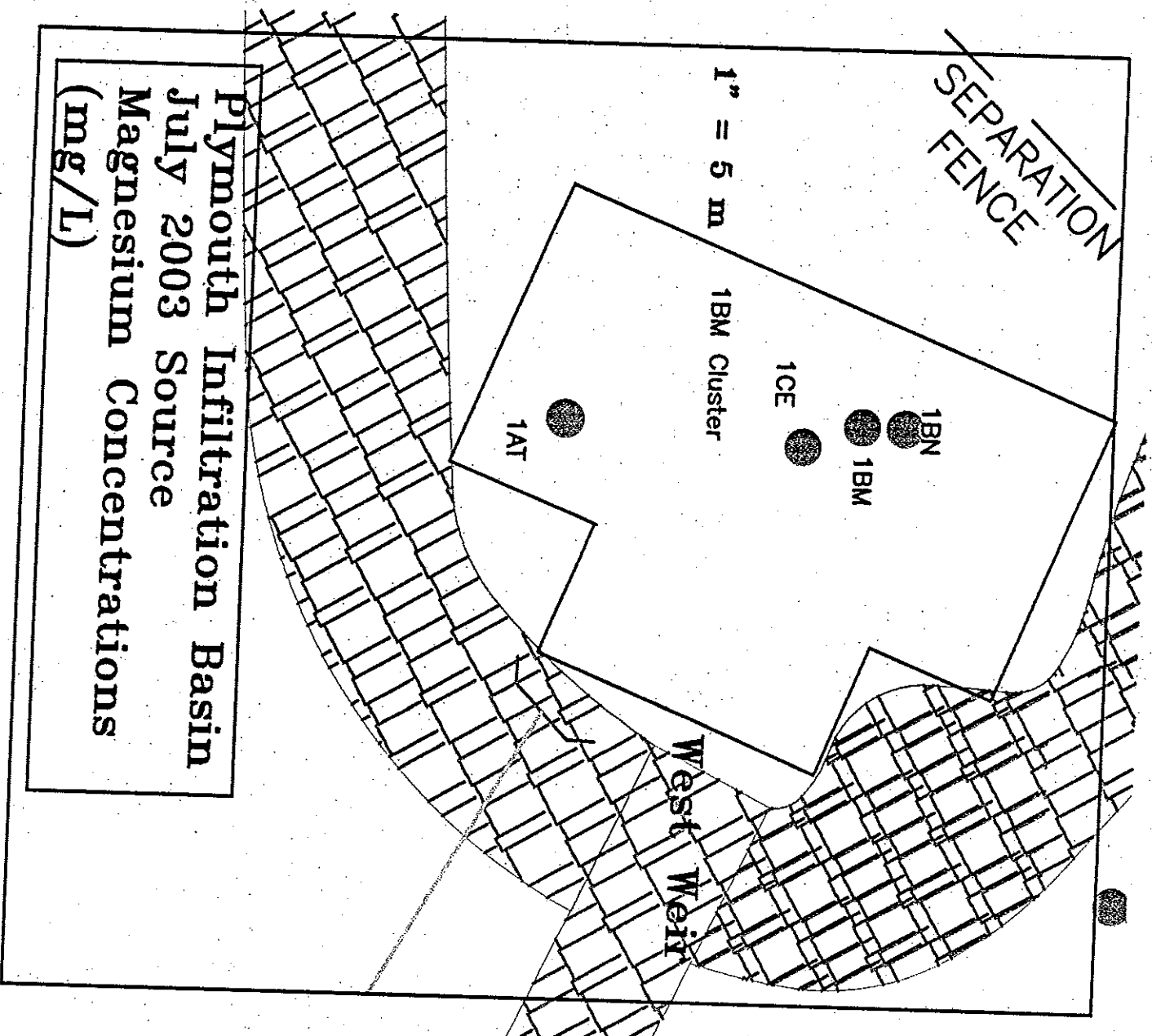


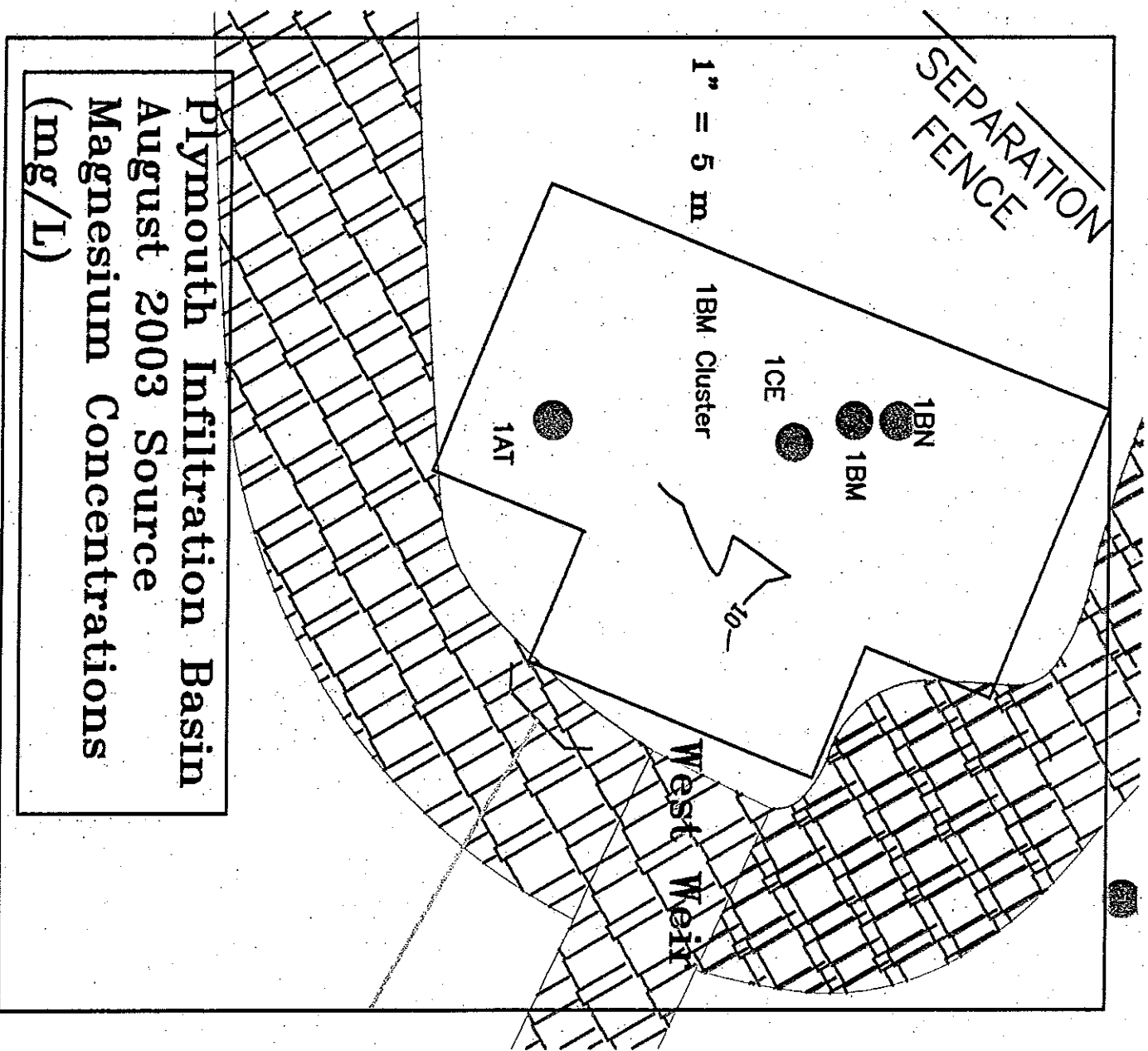




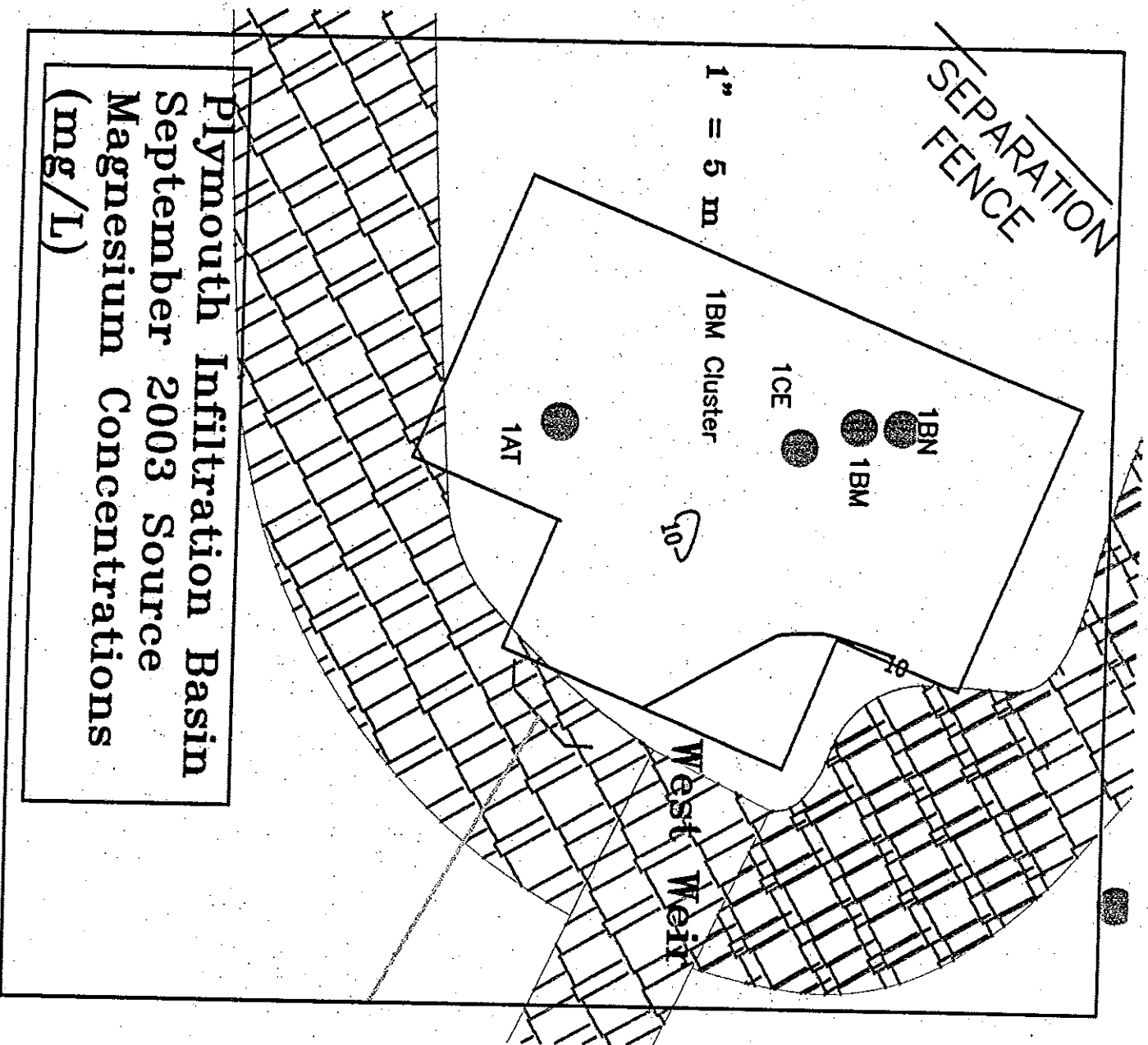


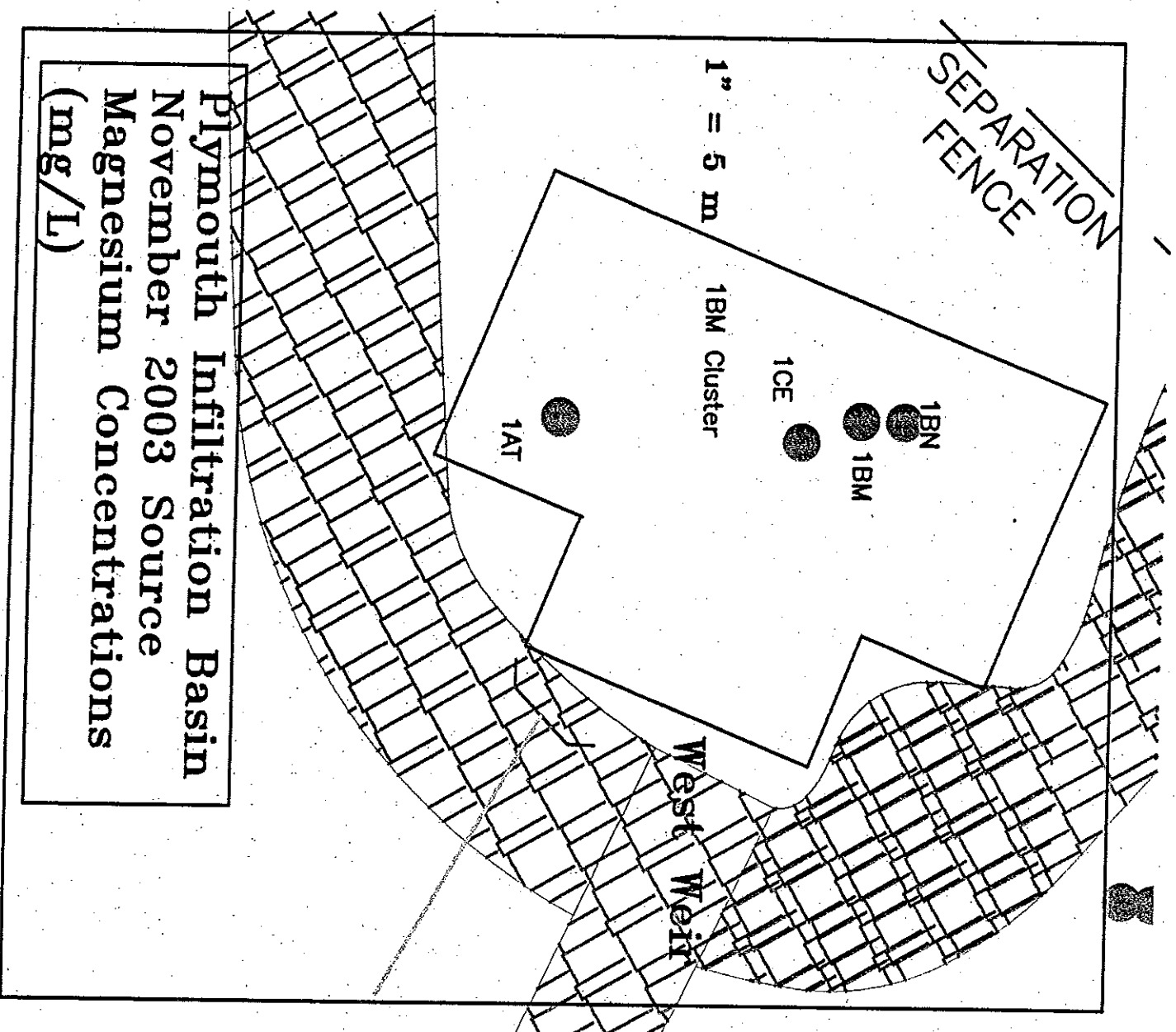


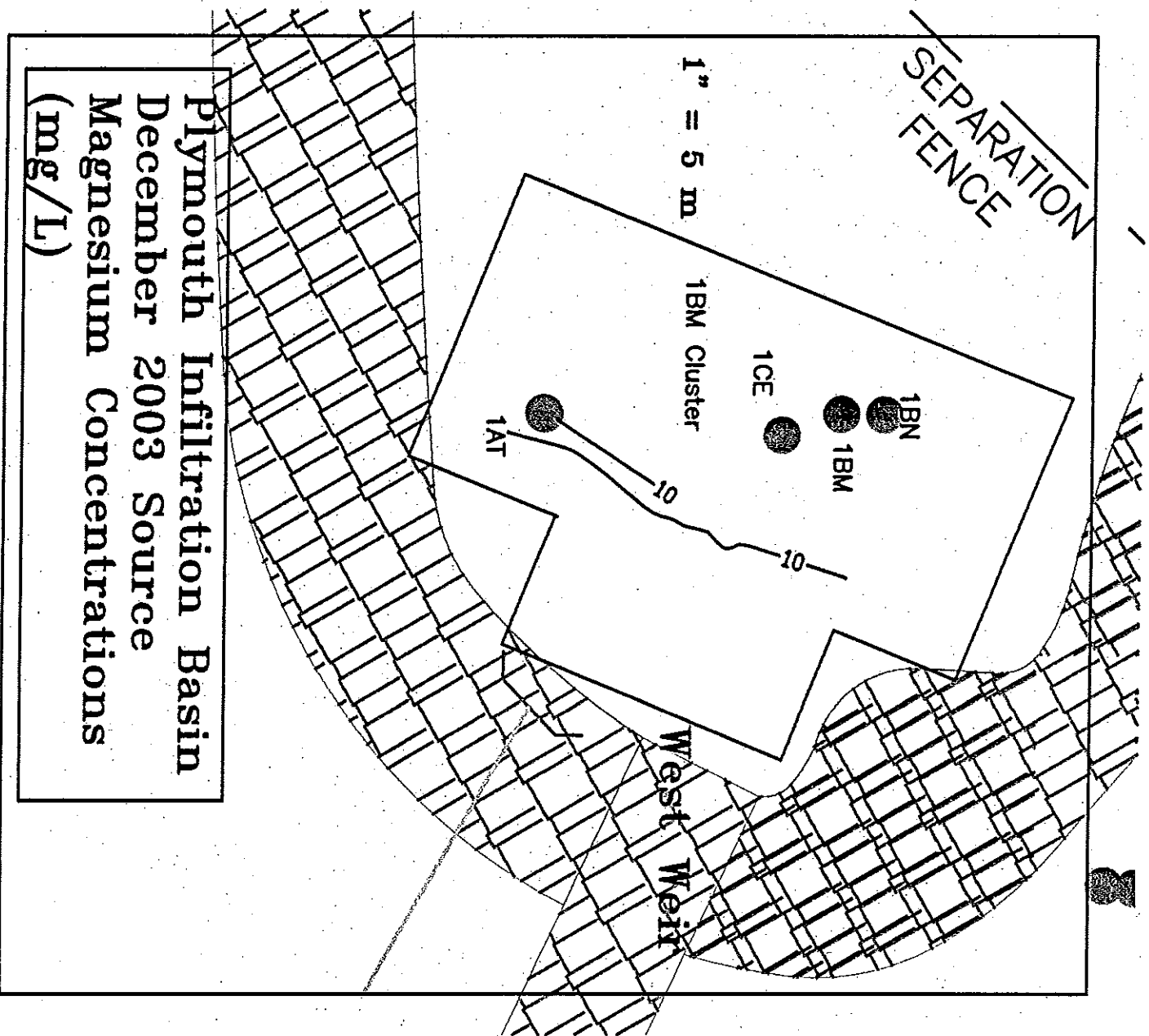


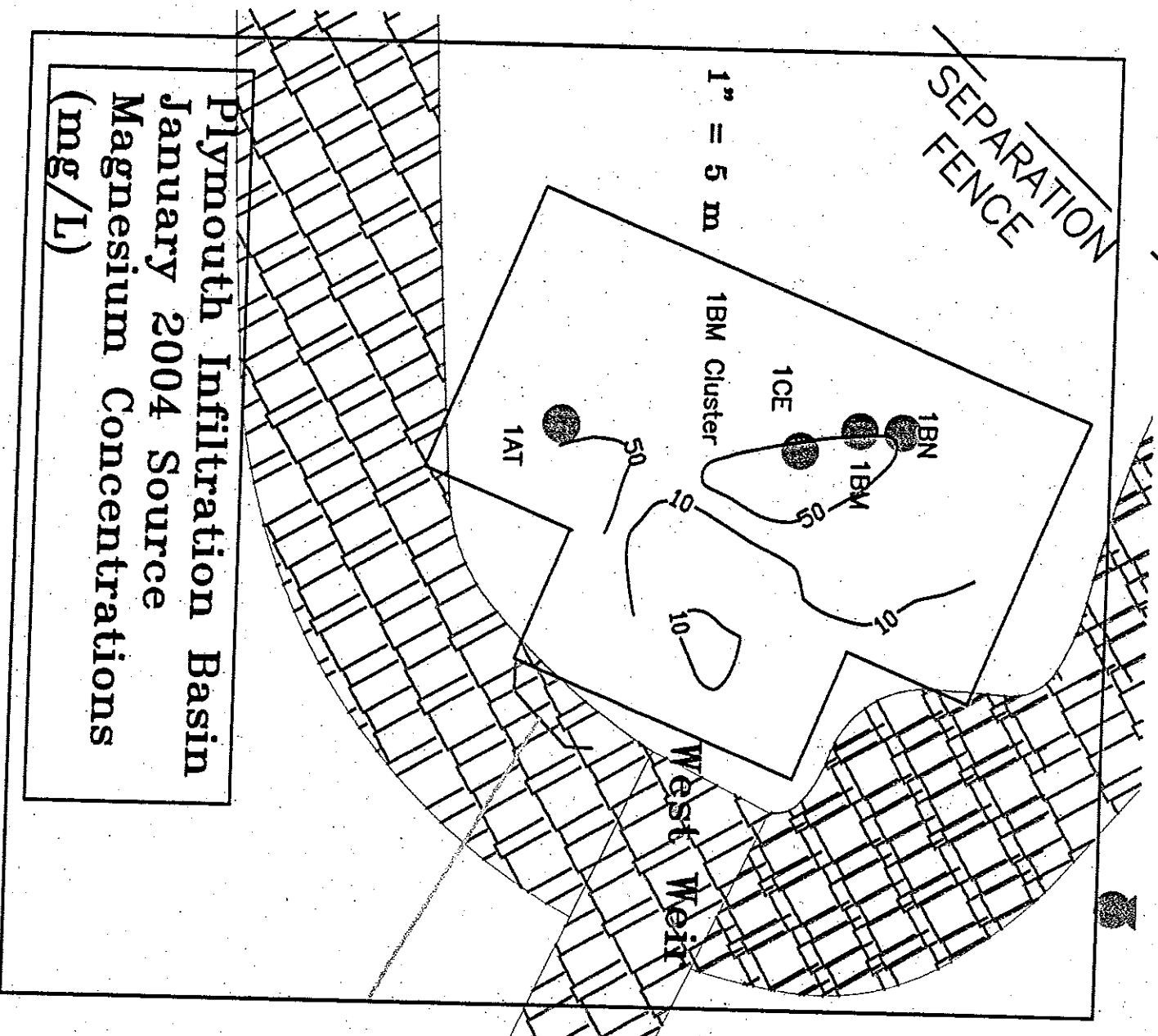


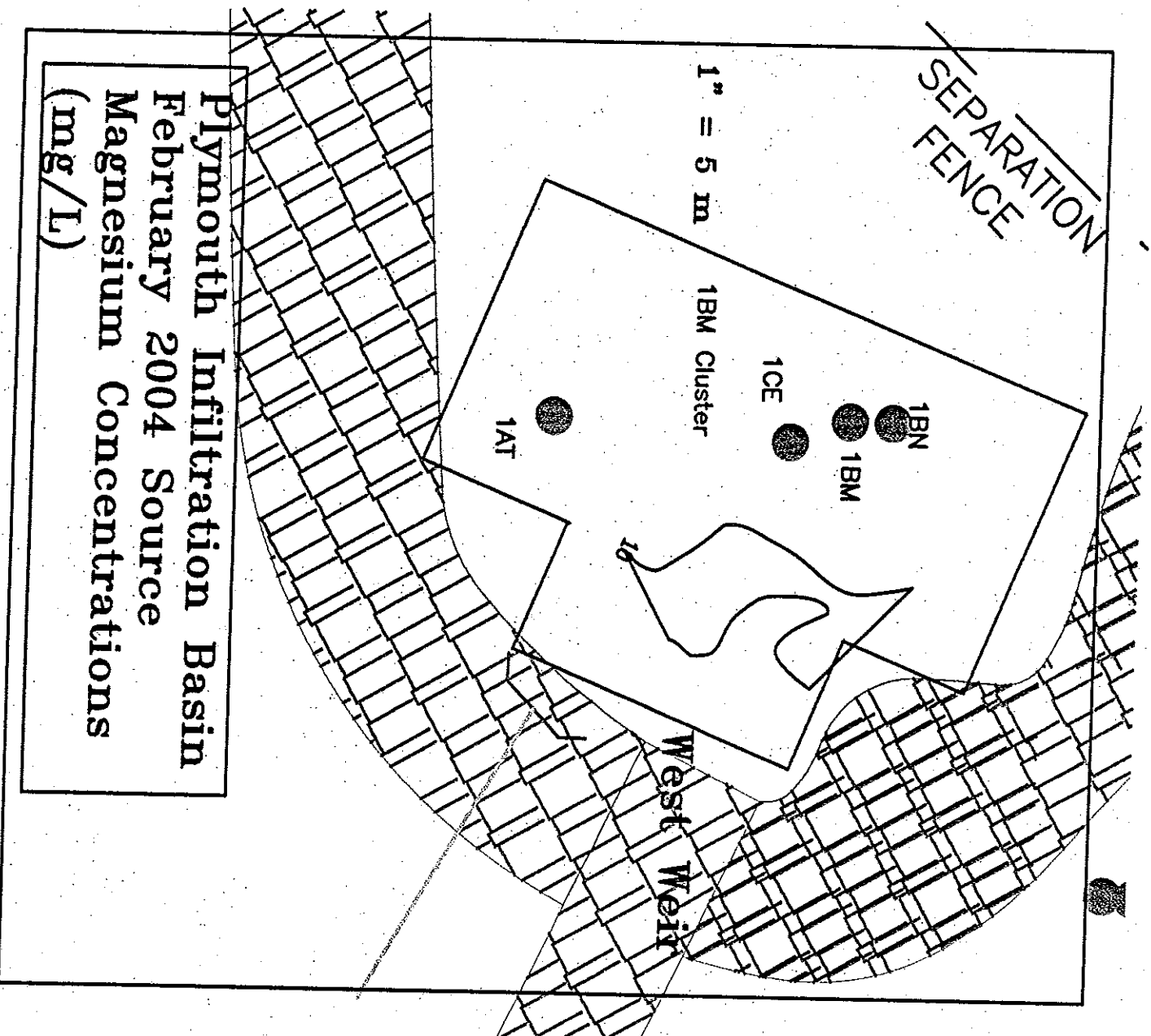
Plymouth Infiltration Basin
August 2003 Source
Magnesium Concentrations
(mg/L)

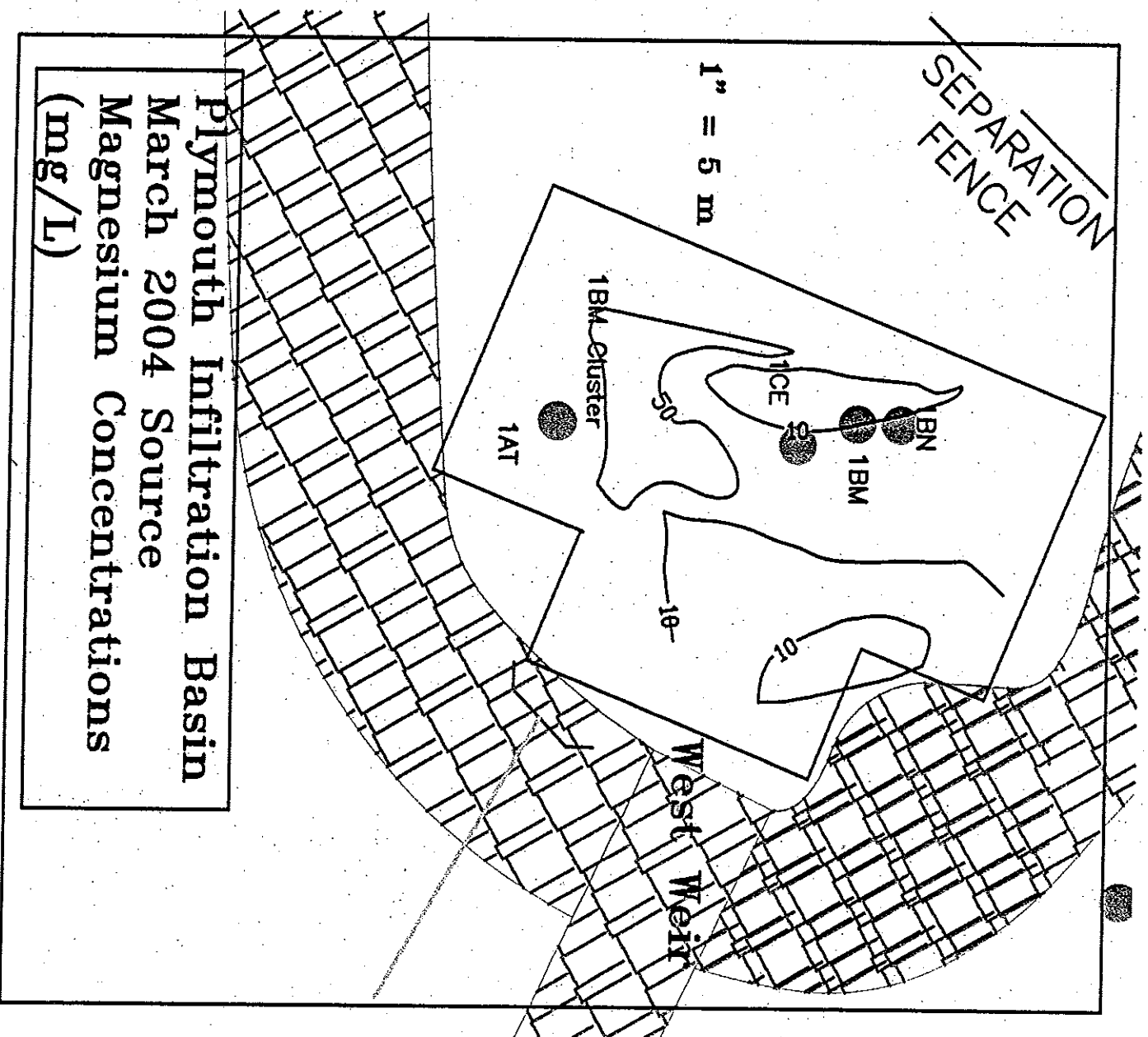


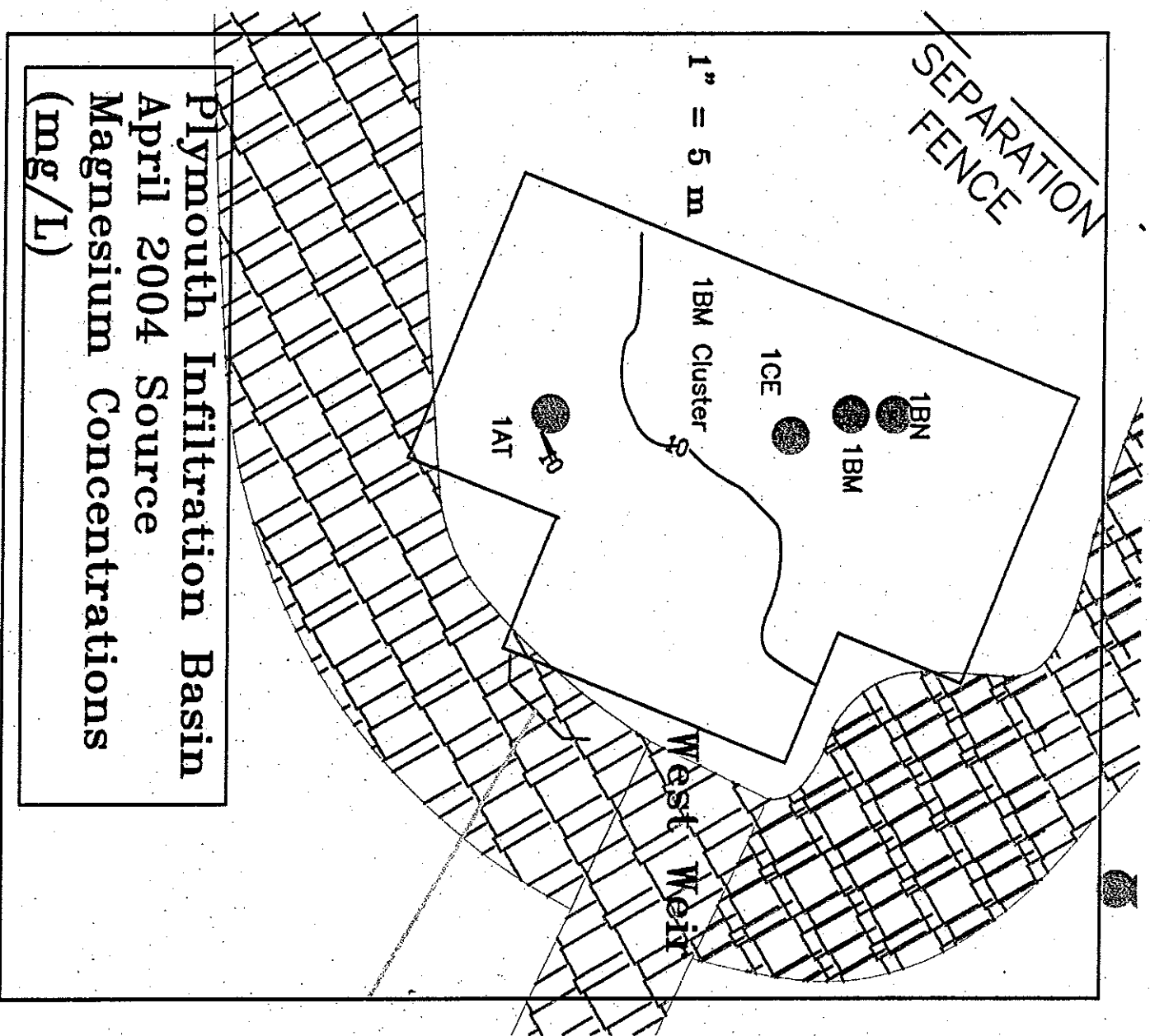


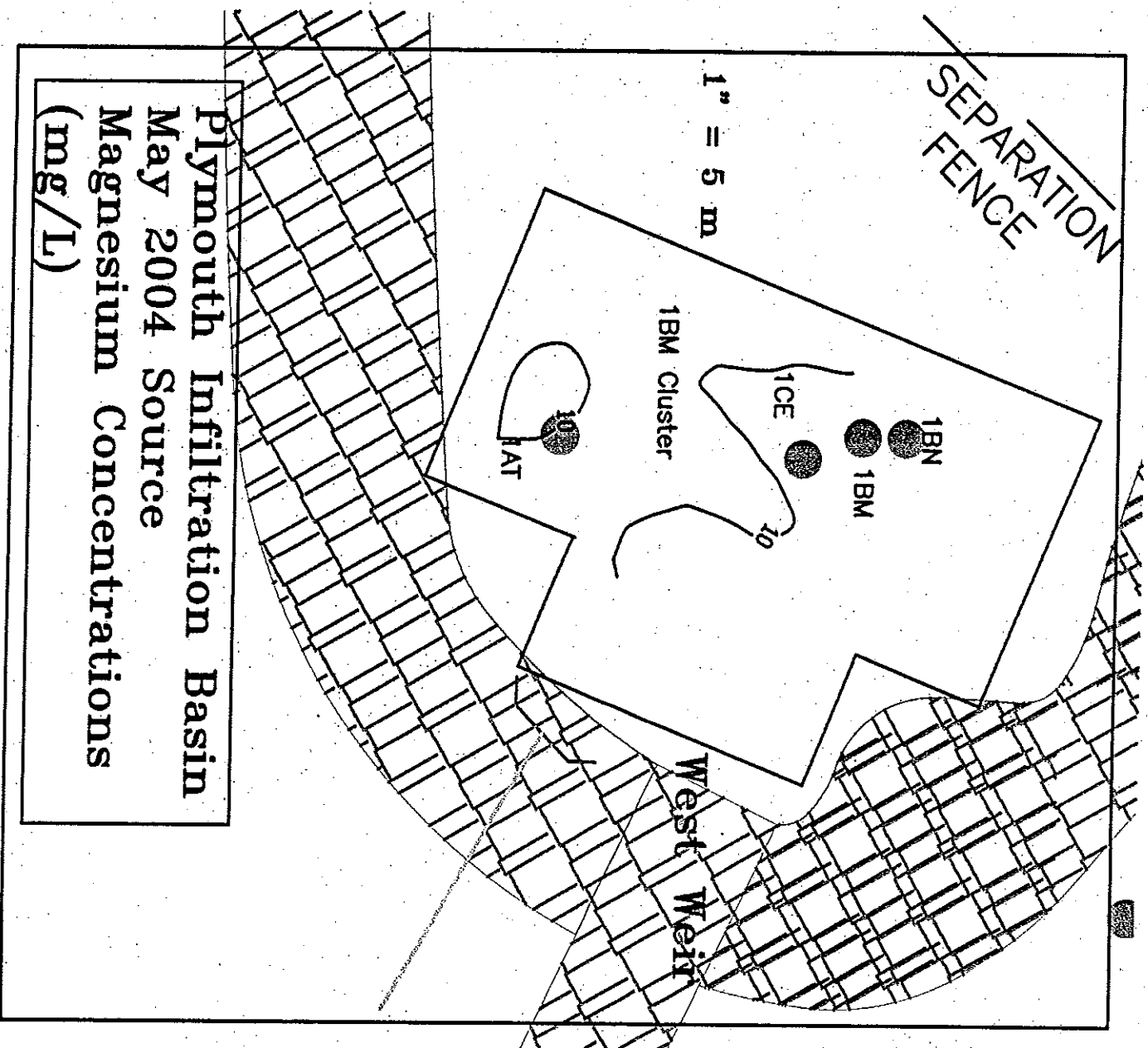












APPENDIX M
Hindcasted Flux Data, November 2002 – May 2004

DATE	Cl Flux		Na Flux		Ca Flux		Mg Flux	
	(mg/L * m3/mo)	(kg/mo)	(mg/L * m3/mo)	(kg/mo)	(mg/L * m3/mo)	(kg/mo)	(mg/L * m3/mo)	(kg/mo)
Nov-02	55207.9	55.2	17126.0	17.1	11205.1	11.2	18576.4	18.6
Dec-02	238749.2	238.7	134241.4	134.2	15834.7	15.8	12680.4	12.7
Jan-03	202287.1	202.3	137151.8	137.2	12756.5	12.8	13721.9	13.7
Feb-03	187519.2	187.5	111676.9	111.7	15971.2	16.0	14004.0	14.0
Mar-03	299572.2	299.6	177128.7	177.1	12775.6	12.8	12814.0	12.8
Apr-03	646378.8	646.4	371349.2	371.3	18595.8	18.6	27303.3	27.3
May-03	204960.8	205.0	131048.8	131.0	990.0	1.0	12269.0	12.3
Jun-03	86694.5	86.7	43000.9	43.0	663.8	0.7	6443.7	6.4
Jul-03	26463.9	26.5	29146.7	29.1	663.8	0.7	487.5	0.5
Aug-03	40715.9	40.7	22155.6	22.2	5292.1	5.3	3928.5	3.9
Sep-03	62085.6	62.1	47313.3	47.3	5033.2	5.0	3554.1	3.6
Oct-03	134868.9	134.9	77680.5	77.7	12776.3	12.8	9704.9	9.7
Nov-03	64034.3	64.0	31042.8	31.0	5981.5	6.0	5004.6	5.0
<hr/>								
	2249538.3	2249.5	1330062.7	1330.1	118539.6	118.5	140492.4	140.5
- ambient	201605.7		151086.6		16316.7		14904.7	
	2047932.6	2047.9	1178976.1	1179.0	102222.9	102.2	125587.7	125.6
		3454.7	total kg/mo					
unadjusted mass ratios		0.5928		0.3413		0.0296		0.0364
		0.819	mass ratio of ions studied (excluding acetate) compared to mass of all ions, used to correct					
			mass ratios					

	app mass ratio	inf mass ratio	error
Ca	0.026	0.024	5%
Na	0.299	0.280	7%
Cl	0.469	0.486	-4%
Mg	0.026	0.030	-16%

Ion	mg/L	
	Mean Concentration	Meyer, 1999
Ca ⁺²	1.0	1.4
Cl ⁻	12.9	10.3
Mg ⁺²	1.0	1.5
Na ⁺	9.6	6.7

	Start X	Y	End X	Y	average Cl- (mg/L)	Na+ (mg/L)	Ca+2 (mg/L)	Mg+2 (mg/L)
1	300	445	305	450	12.7	26.1	13.4	2.8
2	300	450	305	455	3.5	--	21.0	2.9
3	305	440	310	445				
4	305	445	310	450	161.6	50.0	52.5	44.2
5	305	450	310	455				
6	310	440	315	445	52.5	19.5	0.0	9.9
7	310	445	315	450	197.8	37.2	0.0	84.4
8	310	450	315	455				
9	315	445	320	450				
10	315	450	320	455				

	Area (m2)	Cl Flux (mg/L * m3/mo)	(kg/mo)	Na Flux (mg/L * m3/mo)	(kg/mo)	Ca Flux (mg/L * m3/mo)	(kg/mo)	Mg Flux (mg/L * m3/mo)	(kg/mo)
1	25	1.64E+03	1.64	3.37E+03	3.37	1.73E+03	1.73	3.57E+02	0.36
2	25	4.45E+02	0.44	--	--	2.71E+03	2.71	3.69E+02	0.37
3									
4	25	2.08E+04	20.84	6.45E+03	6.45	6.77E+03	6.77	5.69E+03	5.69
5									
6	25	6.77E+03	6.77	2.51E+03	2.51	0.00E+00	0.00	1.27E+03	1.27
7	25	2.55E+04	25.51	4.80E+03	4.80	0.00E+00	0.00	1.09E+04	10.88
8									
9									
10									
total	125	5.52E+04	55.21	1.71E+04	17.13	1.12E+04	11.21	1.86E+04	18.58

Monthly basin recharge rate = $\frac{30}{1.99E+06} \frac{m}{s}$
 $\frac{5.16E+00}{m/mo}$

Wells	X	Y	Cl- (mg/L)	Na+ (mg/L)	Ca+2 (mg/L)	Mg+2 (mg/L)	average Cl- (mg/L)	Na+ (mg/L)	Ca+2 (mg/L)	Mg+2 (mg/L)
BTj	302.767	447.697	27.9	26.1	2.3	1.3				
AT	304.034	447.735	7.3	--	24.3	6.1				
BMc	303.545	448.085	3.0	--	13.6	0.9	12.7	26.1	13.4	2.8
BMd	300.192	451.376	2.1	--	12.8	0.8				
BMa	304.614	451.451	4.8	--	28.8	4.9	3.5	--	21.0	2.9
BCe	306.19	447.614	7.4	12.1	--	--				
BCd	309.248	447.537	48.0	13.7	--	--				
BTg	309.324	446.859	429.3	124.2	52.5	44.2	161.6	50.0	52.5	44.2
BTe	311.776	443.016	55.9	19.1	0.0	11.3				
BTd	310.731	443.023	26.2	15.6	0.0	4.5				
BTa	313.463	443.199	10.5	12.9	0.0	4.0				
BTb	312.611	443.23	11.5	30.3	0.0	19.7	52.5	19.5	0.0	9.9
BTf	310.702	446.776	426.9	72.0	0.0	84.4				
BCi	310.74	447.497	163.1	31.9	--	--				
BCc	312.09	447.539	3.5	7.7	--	--	197.8	37.2	0.0	84.4

APPENDIX N
Summary of November 2002 – May 2004 West Weir Data

Note: When logger did not record data for extended time, estimate for entire month made based on precipitation.

Nov-02

Dec-02

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
1341000	55227.97451	823.3849948

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2664000	3991297.14	2287.72

avg cond 67.07430285 uS/cm

avg cond 1744.66 uS/cm

55227.97451 uS/cm * m3/mo
total monthly SC flux

3991297.14 uS/cm * m3/mo
total monthly SC flux

Jan-03

Feb-03

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
1339200	2589514.00	728.02

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2538000	35865433.44	39420.47

avg cond 3556.93 uS/cm

avg cond 909.82 uS/cm

2589514.00 uS/cm * m3/mo
total monthly SC flux

35865433.44 uS/cm * m3/mo
total monthly SC flux

Mar-03

Apr-03

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2678400	11898628.28	20417.83

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2588400	2659610.36	1346.74

avg cond 582.76 uS/cm

avg cond 1974.85 uS/cm

11898628.28 uS/cm * m3/mo
total monthly SC flux

2659610.36 uS/cm * m3/mo
total monthly SC flux

May-03

Jun-03

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2678400	221421.74	173.19

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2592000	9253.34	38.68

avg cond 1278.51 uS/cm

avg cond 239.21 uS/cm

221421.74 uS/cm * m3/mo
total monthly SC flux

9253.34 uS/cm * m3/mo
total monthly SC flux

Jul-03

Aug-03

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2673000	124621.36	229.48

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q * \text{delta t (m}^3)$
2449800	198316.65	667.51

avg cond 543.06 uS/cm

avg cond 297.10 uS/cm

124621.36 uS/cm * m3/mo
total monthly SC flux

198316.65 uS/cm * m3/mo
total monthly SC flux

Sep-03

$\Sigma\text{delta t (sec)}$	$\Sigma\text{Conductivity Flux}$	$\Sigma Q*\text{delta t (m}^3\text{)}$
1262700	0.00	0.00
avg cond	#DIV/0!	uS/cm
0.00	uS/cm * m3/mo	
	total monthly SC flux	

Oct-03

$\Sigma\text{delta t (sec)}$	$\Sigma\text{Conductivity Flux}$	$\Sigma Q*\text{delta t (m}^3\text{)}$
2679300	121548.72	1142.36
avg cond	106.40	uS/cm
121548.72	uS/cm * m3/mo	
	total monthly SC flux	

Nov-03

$\Sigma\text{delta t (sec)}$	$\Sigma\text{Conductivity Flux}$	$\Sigma Q*\text{delta t (m}^3\text{)}$
2592000	53944.90	530.79
avg cond	101.63	uS/cm
53944.90	uS/cm * m3/mo	
	total monthly SC flux	

Dec-03

$\Sigma\text{delta t (sec)}$	$\Sigma\text{Conductivity Flux}$	$\Sigma Q*\text{delta t (m}^3\text{)}$
1255500	5452800.28	1634.34
avg cond	3336.38	uS/cm
5.27	*flux based on half month =	5452800.28 uS/cm * m3/mo
0.62	in	fell from 12/1 to 12/15
5.89	in	fell from 12/16 to 12/31

estimate for whole month prorated based on precipitation that fell rest of month

6.09E+06 uS/cm * m3/mo
estimated monthly SC flux

Jan-04

$\Sigma\text{delta t (sec)}$	$\Sigma\text{Conductivity Flux}$	$\Sigma Q*\text{delta t (m}^3\text{)}$
2113800	9155587.27	209.90
avg cond	43618.48	uS/cm
0.94	*flux based on part of month =	9155587.27 uS/cm * m3/mo
0.69	in	fell from 1/1 to 1/7
1.63	in	fell from 1/7 to 1/31

estimate for whole month prorated based on precipitation that fell rest of month

1.59E+07 uS/cm * m3/mo
estimated monthly SC flux

Feb-04

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q^* \text{delta t}$ (m ³)
2010600	63206504	21663

avg cond

2917.76

uS/cm

63206504.00

uS/cm * m³/mo

monthly SC flux

Water backed up into weir 2/4/04 5:30 - 2/6/04 13:10 and 2/7/04 11:00 - 2/10/04 20:30. Data is excluded

Mar-04

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q^* \text{delta t}$ (m ³)
2678400	11898628.28	20417.83

avg cond

582.76

uS/cm

11898628.28

uS/cm * m³/mo

total monthly SC flux

Apr-04

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q^* \text{delta t}$ (m ³)
2677800	4077953	492

avg cond

8280.31

uS/cm

4077953.47

uS/cm * m³/mo

monthly SC flux

Cond Measurement on 3/12/04 13:45 wrong, value del.

May-04

Σ delta t (sec)	Σ Conductivity Flux	$\Sigma Q^* \text{delta t}$ (m ³)
2317800	328956.0254	570.2354939

avg cond

576.8774988

uS/cm

328956.0254

uS/cm * m³/mo

monthly SC flux

APPENDIX O
CMA Report Summaries, 2002 – 2003 Deicing Season

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # _____ ENDING 10/19/02

SECTION 5723 LOCATION _____ WAREHAM _____

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report								
Tons Delivered				SALT 590 543	SAND 300 251	PREMIX 23	CM4 90 92	
Total					300	23	90	
Tons Applied								
Tons On Hand				590	300	23	90	

Accumulation: Inches D - Drifting F - Frost 1- Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received
Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM		
ON HAND	1581	
DEL.		
APPL.		
TOT.	1581	

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Carlyle
Highway Repair Foreman
Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # #43-03 ENDING 10/26/02

SECTION 5723 LOCATION WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report				SALT 500	SAND 300	PREMIX 23		CMO 90
Tons Delivered				—	—	—		—
Total				500	300	23		90
Tons Applied				—	—	—		—
Tons On Hand				500	300	23		90

Accumulation: Inches D - Drifting.

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALC IUM		
ON HAND		1581
DEL.		
APPL.		
TOT.		1581

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

ENDING

11/2/02

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report				SALT 560	SAND 200	PREMIX 23		CMA 90
Tons Delivered				—	—	—		
Total				500	200	23		90
Tons Applied				—		—		
Tons On Hand				500	200	23		90

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level.

This report is to be submitted to the Snow and Ice Control Engineer

every Monday morning regardless of activity from the first Material Delivery to the

end of April. On back of sheet list P.O. numbers for sand and salt delivery received

Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	1581
DEL.	
APPL.	
TOT.	

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Collette
Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

#19

ENDING

11/9/02

SECTION

5723

LOCATION

WAREHAM

		SALT		SAND		PREMIX		
DATE	DAY	APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	ACCUM.
	Sunday							
	Monday							
	Tuesday	4						F
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report				SALT 500	SAND 200	PREMIX 23		CMA 90
Tons Delivered				—	—	—		—
Total				500	200	23		90
Tons Applied				4	—	—		—
Tons On Hand				496	200	23		90

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer

every Monday morning regardless of activity from the first Material Delivery to the

end of April. On back of sheet list P.O. numbers for sand and salt delivery received

Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM		
ON HAND		1581
DEL.		X
APPL.		
TOT.		1581

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

20

ENDING

11/16/02

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report				SALT 496	SAND 200	PREMIX 23		CMA 90
Tons Delivered				—	—	—		—
Total				496	200	23		90
Tons Applied				—	—	—		—
Tons On Hand				496	200	23		90

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer

every Monday morning regardless of activity from the first Material Delivery to the

end of April. On back of sheet list P.O. numbers for sand and salt delivery received

Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	1581
DEL.	
APPL.	
TOT.	1581

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Calder
Highway Repair Foreman

Highway Maintenance Foreman

#

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

22

ENDING

11/30/02

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
11/24	Sunday							
25	Monday							
26	Tuesday							
27	Wednesday	60		25				
28	Thursday							
29	Friday							
30	Saturday							
	TOTAL	60		25				
Tons On Hand Last Report				SALT 916	SAND 200	PREMIX 23		CMA 90
Tons Delivered				—	—	—		—
Total				916	200	23		90
Tons Applied				60	25	—		4
Tons On Hand				856	175	23		86

Accumulation: inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	1581
DEL.	
APPL.	
TOT.	1581

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Highway Maintenance Foreman

WALKER TOWNSHIP

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # #23 ENDING 12/7/02

SECTION 5723 LOCATION WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
<u>Dec 1</u>	Sunday							
<u>2</u>	Monday							
<u>3</u>	Tuesday	<u>200</u>	<u>(1756)</u>	<u>60</u>	<u>(145)</u>	<u>10</u>	<u>-</u>	<u>-</u>
<u>4</u>	Wednesday							
<u>5</u>	Thursday	<u>100</u>		<u>20</u>		<u>-</u>		
<u>6</u>	Friday	<u>150</u>		<u>30</u>		<u>-</u>		
<u>7</u>	Saturday							
	TOTAL	<u>350</u>		<u>100</u>	<u>(2145)</u>	<u>10</u>		
Tons On Hand Last Report				SALT	SAND	-PREMIX		<u>CMA</u>
Tons Delivered				<u>856</u>	<u>175</u>	<u>23</u>		<u>86</u>
Total				<u>856</u>	<u>175</u>	<u>23</u>		<u>86</u>
Tons Applied				<u>350</u>	<u>100</u>	<u>10</u>		<u>16</u>
Tons On Hand				<u>506</u>	<u>65</u>	<u>13</u>		<u>70</u>

Accumulation: Inches D - Drifting F - Frost I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' day at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM		
ON HAND		<u>1581</u>
DEL		
APPL		
TOT.		<u>1581</u>

CONVERSION FACTOR
 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Calder
 Highway Repair Foreman
 Highway Maintenance Foreman

CMA
6
5
7
18

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # # 24 ENDING 12/14/02

SECTION 5723 LOCATION WAREHAM

		SALT		SAND		PREMIX		
DATE	DAY	APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	ACCUM.
<u>Dec 8</u>	Sunday							
<u>9</u>	Monday							
<u>10</u>	Tuesday							
<u>11</u>	Wednesday					<u>491</u>		
<u>12</u>	Thursday	<u>30</u>		<u>10</u>		<u>298</u>		<u>Frost</u>
<u>13</u>	Friday	<u>10</u>		<u>—</u>				<u>Frost</u>
<u>14</u>	Saturday							
	TOTAL	<u>40</u>		<u>10</u>		<u>798</u>		
Tons On Hand Last Report				<u>SALT 506</u>	<u>SAND 175</u>	<u>PREMIX 23</u>		<u>CMA 70</u>
Tons Delivered				<u>—</u>	<u>798</u>	<u>—</u>		<u>—</u>
Total				<u>856</u>	<u>973</u>	<u>23</u>		<u>8670</u>
Tons Applied				<u>40</u>	<u>10</u>	<u>—</u>		<u>1</u>
Tons On Hand				<u>846</u>	<u>963</u>	<u>33</u>		<u>8569</u>

Accumulation: Inches 466 D-Drifting F-Frost I-Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P. O. numbers for sand and salt delivery received

Balance On Hand shown on this report should equal the amount of material you have

LIQ. CALCIUM	
ON HAND	<u>1581</u>
DEL.	
APPL.	
TOT.	<u>1581</u>

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

CDH

Highway Repair Foreman

Highway Maintenance Foreman

12/21/02

WAREHAM

03A

1-ICE

Liq. CALCIUM

end of April. On back of sheet list P.O. numbers for sand and salt delivery received

Balance On Hand shown on this report should equal the amount of material you have

Highway Repair Foreman

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Maintenance Foreman

WILLOW LAKE DISTRICT

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

26

ENDING

12/28/02

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
Dec 22	Sunday							
23	Monday							
24	Tuesday							
25	Wednesday	60		15				
26	Thursday	106		35		23		1 1/2"
27	Friday							
28	Saturday							
	TOTAL	166						
Tons On Hand Last Report				SALT	SAND	PREMIX		CMA
Tons Delivered				666	933	23		66
Total				666	933	23		66
Tons Applied				166	50	23		5
Tons On Hand				500	883	0		69

Accumulation: Inches D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received
Balance On Hand shown on this report should equal the amount of material you have

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

LIQ. CALCIUM		
ON HAND		2357
DEL.		X
APPL.		
TOT.		2357

Highway Repair Foreman

Highway Maintenance Foreman

#

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

428

ENDING

1/11/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday	20		10		10		5 CMA
	Monday	180		30		30		1.5 CMA
	Tuesday	135		20		-		2.5 CMA
	Wednesday	80		20		-		5
	Thursday							
	Friday							
	Saturday							
	TOTAL	355		80		40		6.5
Tons On Hand Last Report				SALT 976	SAND 818	PREMIX 44		CMA 56
Tons Delivered				976	818	44		56
Total				976	818	44		56
Tons Applied				355	80	40		6.5
Tons On Hand				621	738	4		49.5

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	2351
DEL.	
APPL.	
TOT.	2351

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

11/18/03

WAREHAM

Price

Highway Maintenance Foreman

WELLS RIVER TOWN

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # #30

ENDING 1/25/03

SECTION 5723

LOCATION WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
1/19	Sunday	30		15		15		
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday	2		20		30		
	Saturday							
	TOTAL	30		25		45		
Tons On Hand Last Report				SALT 991	SAND 698	PREMIX 143		CMA 45
Tons Delivered				—	—	—		—
Total				991	698	143		45
Tons Applied				30	25	45		1
Tons On Hand				961	673	98		44

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM		
ON HAND		2351
DEL		
APPL		
TOT.		2351

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Paul P. L. L.
Highway Repair Foreman

Highway Maintenance Foreman

ANNUAL MATERIALS EXPENDITURE REPORT

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

#31

ENDING

2/11/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
Jan 26	Sunday							
27	Monday							
	Tuesday	40		15		15		1/4"
	Wednesday	10		30				Forest
	Thursday	45		15		15		
	Friday							
Feb 1	Saturday	20		10		10		
	TOTAL	115		60		40		
Tons On Hand Last Report				SALT	SAND	PREMIX		CMA
Tons Delivered				961	673	98		44
Total				961	673	98		44
Tons Applied				115	60	40		8
Tons On Hand				846	613	58		42

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

LIQ. CALCIUM		
ON HAND		2351
DEL.		
APPL.		
TOT.		2351

Carls

Highway Repair Foreman

Highway Maintenance Foreman

WINTER MAINTENANCE LOG

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

#32

ENDING

2/8/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
2-2	Sunday	60		20		20		1/2
	Monday	80		10		10		1
	Tuesday							
	Wednesday							
	Thursday							
	Friday	400		60		20		9"
	Saturday	6		1				7
	TOTAL	546		90		50		8
Tons On Hand Last Report				SALT 846	SAND 613	PREMIX 58		CM1 42
Tons Delivered				—	—	—		—
Total				846	613	58		42
Tons Applied				546	90	50		7
Tons On Hand				300	523	8		35

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM		
ON HAND		2351
DEL.		✓
APPL.		
TOT.		2351

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Calder

Highway Maintenance Foreman

WINTER MAINTENANCE REPORT

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

33

ENDING

2/15/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday	190	X 78.88	40		8		1316 5
	Tuesday	404	376.77	10		—		1
	Wednesday	30		5		0		110 1
	Thursday							
	Friday		✓ 600.81					
	Saturday							
	TOTAL	260	1076.29	55				7
Tons On Hand Last Report				SALT 300	SAND 523	PREMIX 8		CMA 35
Tons Delivered				1076.0	—	—		—
Total				1376	523	8		35
Tons Applied				260	55	8		7
Tons On Hand				1146	468	0		28

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

LIQ. CALCIUM		
ON HAND		2351
DEL.		
APPL.		
TOT.		2351

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # # 34 ENDING 2/22/03

SECTION 5723 LOCATION WAREHAM

		SALT		SAND		PREMIX		
DATE	DAY	APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	ACCUM.
	Sunday							
	Monday	180		70				18 1/4
	Tuesday	180		60				18 1/4
	Wednesday							
	Thursday	40		10				Frost
	Friday							
	Saturday							
	TOTAL	400		140				
Tons On Hand Last Report				SALT 1116	SAND 468	PREMIX 0		CMA 28
Tons Delivered				—	—	—		—
Total				1116	468	0		28
Tons Applied				400	140	—		45
Tons On Hand				716	328	0		13

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

LIQ. CALCIUM		
ON HAND		2357
DEL.		
APPL.		
TOT.		2357

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

3/1/03

WAREHAM

C. M. H.

Highway Maintenance Foreman

LIQ. CALCIUM	
ON HAND	2351
DEL.	
APPL.	
TOT.	2351

MAINTENANCE LOG

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

#37

ENDING

3/15/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
3-9	Sunday							
10	Monday		406					
11	Tuesday							
12	Wednesday							
13	Thursday	200		40		0		34
14	Friday	50		10				
15	Saturday							
	TOTAL	250	406	50		0		
Tons On Hand Last Report				SALT 180	SAND 198	PREMIX 0		CMA 158
Tons Delivered				406	—	—		—
Total				586	198	0		138
Tons Applied				250	50	—		4
Tons On Hand				336	148	0		94

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

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CONVERSION FACTOR

- 1 Cubic Yard Sand = 1.5 ton(3000lbs.)
- 1 Cubic Yard Salt = 1.0 ton(2000lbs.)
- 1 Cubic Yard Premix = 1.0 ton(2000lbs.)

LIQ. CALCIUM	
ON HAND	2351
DEL	
APPL	
TOT.	2351

Highway Repair Foreman

Highway Maintenance Foreman

WARREHAU

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

439

ENDING

3/29/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCU.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
	Sunday							
	Monday							
	Tuesday							
	Wednesday							
	Thursday							
	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report								
				SALT	SAND	PREMIX		CMA
Tons Delivered				336	148	0		49
Total				336	148	0		49
Tons Applied				—	—	—		—
Tons On Hand				336	148	0		49

Accumulation: Inches D-Drifting

F-Frost

I-Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level.

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LIQ. CALCIUM		
ON HAND		2351
DEL.		
APPL.		
TOT.		2351

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Cal. J. J. J.
Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

40

ENDING

4/5/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
3-30	Sunday							
31	Monday	80		30		-		1"
4-1	Tuesday							
2	Wednesday							
3	Thursday							
4	Friday							
5	Saturday	50		-		-		1CE
	TOTAL	130		30		-		

CMA

2

1/5

		SALT	SAND	PREMIX	
Tons On Hand Last Report		336	148	0	CMA 49
Tons Delivered					
Total		336	148	0	49
Tons Applied		130	30	-	3
Tons On Hand		206	118	0	46

Accumulation: Inches

D - Drifting

F - Frost

I - Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	2351
DEL.	
APPL.	
TOT.	

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman

Highway Maintenance Foreman

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK # 41 SECTION 5723

ENDING 4/12/03 LOCATION WAREHAM

DATE	DAY	SALT			SAND			PREMIX		
		APPLIED	DELIVERED	ACCUM.	APPLIED	DELIVERED	ACCUM.	APPLIED	DELIVERED	ACCUM.
4-6	Sunday									
7	Monday	89	104							
8	Tuesday	90	20							
9	Wednesday									
10	Thursday	30	5							
11	Friday									
12	Saturday									
	TOTAL	200	104	45						
Tons On Hand Last Report				SALT	208	SAND	118	PREMIX	0	
Tons Delivered					104					
Total					310		118		0	
Tons Applied					800		48		—	
Tons On Hand					110		70		0	

Accumulation: Inches
D - Drifting
F - Frost
I - Ice

NOTE: To estimate materials on hand: 135 tons per 12" bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received Balance On Hand shown on this report should equal the amount of material you have.

CONVERSION FACTOR
1 Cubic Yard Sand = 1.5 ton(3000lbs.)
1 Cubic Yard Salt = 1.0 ton(2000lbs.)
1 Cubic Yard Premix = 1.0 ton(2000lbs.)

Highway Repair Foreman E. J. J. J.
Highway Maintenance Foreman

LIQ. CALCIUM
ON HAND 2351
DEL. 2351
APPL. 2351
TOT. 2351

DISTRICT FIVE MATERIALS EXPENDITURE REPORT

WEEK #

#40

ENDING

4/19/03

SECTION

5723

LOCATION

WAREHAM

DATE	DAY	SALT		SAND		PREMIX		ACCUM.
		APPLIED	DELIVERED	APPLIED	DELIVERED	APPLIED	DELIVERED	
13	Sunday							
14	Monday							
15	Tuesday							
16	Wednesday							
17	Thursday		530.90					
18	Friday							
	Saturday							
	TOTAL							
Tons On Hand Last Report				SALT 110	SAND 70	PREMIX 0		CMA 40
Tons Delivered				531	—	—		—
Total				641	70	0		40
Tons Applied				—	—	—		—
Tons On Hand				641	70	0		40

Accumulation: Inches

D - Drifting

F- Frost

I- Ice

NOTE: To estimate materials on hand: 135 tons per 12' bay at water level

This report is to be submitted to the Snow and Ice Control Engineer every Monday morning regardless of activity from the first Material Delivery to the end of April. On back of sheet list P.O. numbers for sand and salt delivery received. Balance On Hand shown on this report should equal the amount of material you have.

LIQ. CALCIUM	
ON HAND	2351
DEL.	
APPL.	
TOT.	2351

CONVERSION FACTOR

1 Cubic Yard Sand = 1.5 ton(3000lbs.)

1 Cubic Yard Salt = 1.0 ton(2000lbs.)

1 Cubic Yard Premix = 1.0 ton(2000lbs.)


 Highway Repair Foreman

Highway Maintenance Foreman